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BACHELOR'S THESIS

**PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT
USING AVIARY**

By

Samuel Theofilus Tamonob

11202101008

Presented to the Faculty of Engineering and Life Sciences
In Partial Fulfillment Of the Requirements for the Degree of

BACHELOR'S DEGREE

In

AVIATION ENGINEERING

FACULTY OF ENGINEERING AND LIFE SCIENCES

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APPROVAL PAGE

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STATEMENT BY THE AUTHOR

I hereby declare that this submission is my own work and to the best of my knowledge, it contains no material previously published or written by another person, nor material which to a substantial extent has been accepted for the award of any other degree or diploma at any educational institution, except where due acknowledgment is made in the thesis.

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ABSTRACT

Preliminary Sizing of Homeland Defense Interceptor Aircraft using Aviary

by

Samuel Theofilus Tamonob

Triwanto Simanjuntak, PhD, Advisor

Dr. Eng. Ressa Octavianty, Co-Advisor

The increasing threat from aerial incursions such as cruise missiles, stealth aircraft, and unmanned systems demands interceptor specifically designed for homeland defense. This study presents the preliminary sizing of an unmanned Homeland Defense Interceptor (HDI) using the open-source AVIARY framework, which integrates parametric design and mission analysis within OpenMDAO. Based on the 2025 AIAA Undergraduate Design RFP, the HDI is evaluated across three mission profiles: Defensive Counter-Air Patrol, Point Defense Interception, and Intercept/Escort, using benchmarking data from the F-22 Raptor, Saab JAS 39C Gripen, MiG-29 Fulcrum, and Bayraktar Kzlelma. Through iterative simulation and constraint analysis, the HDI has a Gross Takeoff Weight ($GTOW$) of 36,066 lb (16,359 Kg), fuel weight of 14,683 lb (6660.1 Kg), a wing area of 486.61 ft² (45.17 m²), Aspect Ratio of 3.98, Horizontal Tail Area of 154.73 ft² (14.37 m²), Vertical Tail Area of 53.98 ft² (5.01 m²), Wing Loading of 72.04 lb/ft² (351.73 kg/m²) and a Thrust-to-Weight ratio of 0.98, while meeting key loiter, dash, and interception requirements. The results demonstrate AVIARYs effectiveness as a multidisciplinary conceptual design tool and confirm the feasibility of a tailored unmanned interceptor within defined performance.

Keyword: *Conceptual Design, Aircraft sizing, AVIARY, Interceptor, Homeland Defense, OpenMDAO*

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Special appreciation goes to AVIARY development communities. Their open-source contributions, documentation, and collaborative spirit have played a crucial role in the progress of this project. I am grateful for the opportunity to learn from such a dedicated and innovative group of professionals.

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Finally, to my friends and peers, thank you for the camaraderie, shared struggles, and words of encouragement that made this journey not only possible but also meaningful and fulfilling. Your presence has been a source of both strength and joy.

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List of Abbreviations

AIAA	American Institute of Aeronautics and Astronautics
NASA	National Aeronautics and Space Administration
HDI	Homeland Defense Interceptor
RFP	Request For Proposal
UCAV	Unmanned Combat Aerial Vehicle
NGAD	Next Generation Air Dominance
IADS	Integrated Air Defense System
SAMs	Surface to Air Missiles
GTOW	Gross Takeoff Weight
CG	Central of Gravity
EOM	Equation Of Motion
SFC	Specific Fuel Consumption
AR	Aspect Ratio
nmi	nautical miles
APU	Auxiliary Power Unit
RCS	Radar Cross Section
ICNIA	Integrated Communications Navigation and Identification Avionics
MFDs	Multi Function Displays
OBOGS	On Board Oxygen Generating System
OBIGGS	On Board Inert Gas Generating System
AIM	Aeronautical Information Manual
FAA	Federal Aviation Administration
EASA	European Union Aviation Safety Agency
FLOPS	Flight Optimization System
GASP	General Aviation Synthesis Program
OpenMDAO	Open Source Multidisciplinary Design Analysis and Optimization
MDO	Multidisciplinary Design Optimization

IPOPT	I nterior P oint O ptimizer
SNOPT	S parse N onlinear O ptimizer
SLSQP	S equential L east S quares P rogramming
CFD	C omputational F luid D ynamics
DATCOM	D ata C omendium
DCAP	D efense C ombat A ir P atrol
PDI	P oint D efense I ntercept

Dedicated to my parents

CHAPTER 1

INTRODUCTION

1.1 Background

The increasing instability of world political and military developments points to the necessity of securing national airspace. The United States today could be targeted with a variety of airborne weapons including hijacked commercial jets or cruise missiles or drones that are difficult to stop. This requires a quick-reaction air defense system that can identify, intercept and negate such threats before they strike critical infrastructure or civilian targets.

Current air superiority fighters such as the *F-22 Raptor* and *F-35 Lightning II*, while technologically advanced, were primarily developed for high-end conflict scenarios and are associated with high operational costs and limited production quantities. These characteristics make them less ideal for widespread deployment in a homeland defense role where affordability, operational simplicity, and high sortie rates are crucial.



(A) F-22 Raptor LockheedMartinF222025



(B) F-35 Lightning II
LockheedMartinF352025

To address this capability gap, the AIAA Undergraduate Aircraft Design Team RFP 2025 calls for the development of a new class of interceptor aircraft which

is the *Homeland Defense Interceptor (HDI)*. The HDI must be unmanned, highly maneuverable, and optimized for three specific mission profiles:

1. Defensive Counter-Air (DCA) Patrol, involving loitering near high-value assets to intercept threats.
2. Point Defense Interception, for rapid engagement of local airborne threats.
3. Intercept/Escort, entailing high-speed pursuit or protection of allied aircraft.

This research utilizes AVIARY, an open-source tool developed by NASA on the OpenMDAO framework. AVIARY supports multidisciplinary aircraft sizing through parametric inputs and integrated mission analysis capabilities, making it highly suitable for early-phase design studies like this one.

1.2 Problem Statement

The conceptual design of modern military aircraft faces increasing complexity, driven by the demanding interplay of advanced performance metrics and stringent operational effectiveness requirements. Traditional sizing methods are often insufficient in this environment due to:

- Siloed by discipline, requiring manual coordination of aerodynamic, propulsion, and weight estimates.
- Time-consuming and inefficient for rapid design iterations.
- Difficulties in adapting swiftly to evolving mission constraints or integrating technological updates.

This research aims to address these challenges by applying AVIARY as a design tool for preliminary sizing. The tool's integration of weight, performance, mission, and geometry estimation enables a more streamlined and data-driven approach to concept development for the HDI.

1.3 Research Objectives

The primary objectives of this research are as follows:

1. To interpret the mission profiles and technical constraints defined in the AIAA 2025 RFP.
2. To use the AVIARY framework to develop a preliminary aircraft sizing model that meets those mission requirements.
3. To evaluate aircraft performance across three mission types: DCA patrol, point defense, and intercept/escort.
4. To determine key design parameters such as takeoff weight, wing area, thrust requirement, and fuel load.
5. To benchmark the HDI design against existing aircraft, including both manned and unmanned interceptors.

1.4 Research Scope and Limitation

1.4.1 Scope

This research focuses exclusively on the preliminary sizing of a homeland defense interceptor aircraft. The specific areas of focus include:

- Development of a parametric sizing model using AVIARY.
- Inclusion of three distinct mission profiles with performance constraints.
- Estimation of key design parameters: gross weight, wing area, aspect ratio, thrust-to-weight ratio, and fuel capacity.
- Use of empirical models from Raymer and benchmark aircraft data to provide sizing inputs.
- Iterative mission-constrained design refinement using AVIARY's optimization tools.

1.4.2 Limitations

Despite the comprehensive approach, this study is limited by several factors:

- AVIARY does not currently support supersonic aerodynamic modeling; thus, any supersonic effects are excluded.
- No structural modeling or stress analysis is performed at this stage.

- The study does not account for stealth characteristics, radar cross-section, or ECM systems integration.
- Engine modeling is simplified to thrust and fuel flow estimates without full cycle thermodynamics.

1.5 Significance of the Study

This study contributes to the field of preliminary aircraft design in the following ways:

- Demonstrates AVIARY, the application of a modern, open-source, multidisciplinary tool for aircraft conceptual sizing.
- The findings can inform future research and development efforts in aircraft design and aerospace engineering, particularly in the context of homeland security.

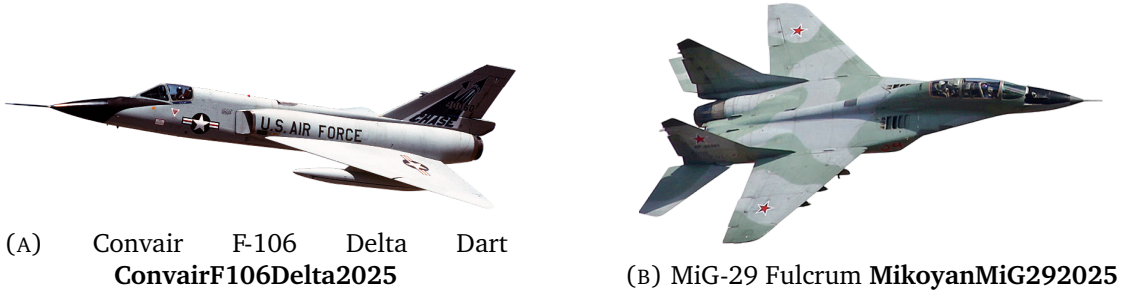
CHAPTER 2

LITERATURE REVIEW

2.1 Interceptor Aircraft Concept

2.1.1 Development of Interceptor Aircraft

The development of interceptors aircraft have been a subject of ongoing research for decades. Since the Cold War era, aircraft interception has evolved with technological advancements in aerodynamics, propulsion systems, avionics, and missile technology **InterceptorAircraft2025**. Earlier interceptor designs, such as the MiG-21 and the F-106 Delta Dart as shown in Figure 2.1a, were focused on high-speed interception, relying heavily on supersonic performance and missile armament. Over the years, newer designs have incorporated advanced stealth technologies, agility, and multi-role capabilities, exemplified by modern aircraft such as the F-22 Raptor 1.1a and Mikoyan MiG-29 Fulcrum 2.1b.



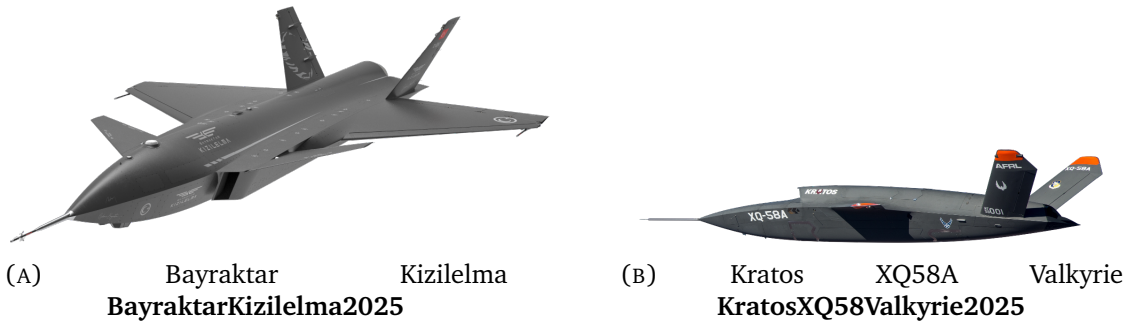
Homeland aircraft interceptors are specialized military aircraft designed to respond rapidly to aerial threats within a nation’s airspace. The primary mission of an interceptor is to engage and neutralize incoming aircraft or missiles, often before they can reach critical targets. To meet these operational needs, interceptors must excel in high-speed flight, fast climb rates, and superior maneuverability.

These requirements present unique challenges for aircraft designers, who must also balance the interceptors range, payload capacity, and fuel efficiency.

2.1.2 Future Interceptor Aircraft

The pursuit of advanced interceptor aircraft has become a major focus in modern aerospace defense discussions. Initiatives such as the U.S. Next Generation Air Dominance (NGAD) and Russias MiG-41 project reflect a growing trend toward aircraft capable of hypersonic flight, enhanced stealth, and sophisticated electronic warfare capabilities. These platforms are being designed to counter both conventional aerial threatslike fighter jets and bombersand newer challenges such as hypersonic missile systems.

At the same time, the role of Unmanned Combat Aerial Vehicles (UCAVs) in air defense is gaining prominence. UCAVs present several advantages over manned aircraft, including reduced operational risk, enhanced agility, and lower life-cycle costs. Modern demonstrators such as the Kratos XQ-58A Valkyrie shown in Figure 2.2b, Northrop Grumman X-47B, and Bayraktar Kzlelma shown in Figure 2.2a exemplify the growing feasibility of unmanned interceptors capable of fulfilling high-speed, high-threat missions. Furthermore, with the integration of artificial intelligence and real-time data processing, UCAVs are increasingly capable of operating autonomously in dynamic combat environments. These trends suggest that future interceptor aircraft will likely be unmanned, highly networked, and optimized using multidisciplinary design frameworks to meet evolving defense needs with greater speed, efficiency, and adaptability.



2.2 Homeland Defense and Air Threats

2.2.1 Overview of Homeland Defense Systems

Homeland defense systems are developed to safeguard a nation's airspace against a wide range of aerial threats, including hostile aircraft, unmanned aerial vehicles (UAVs), and missiles. These systems operate as part of a comprehensive Integrated Air Defense System (IADS), which merges early warning mechanisms, ground-launched missile systems, and interceptor aircraft.

A key feature of homeland defense is the implementation of a multi-layered protection strategy, which utilizes a combination of airborne and ground-based sensors, command and control infrastructure, and interceptor platforms. This layered approach allows threats to be detected and neutralized at various distances and altitudes. Components of this system typically include:

- Long-range surveillance system, such as over-the-horizon radar systems.
- Medium-range protection via surface-to-air missile (SAM) systems shown in Figure 2.3 like the Patriot or S-400.
- Short-range, rapid-response interceptors to engage threats that manage to breach the outer layers of defense.

Command and Control (C2) systems are vital to ensuring effective coordination within homeland defense operations. These systems support quick decision-making and seamless integration across different defensive layers. By leveraging data fusion technologies, C2 systems can combine inputs from multiple sources including ground radar stations, satellites, and airborne early warning platforms like AWACS to deliver real-time situational awareness and guide response actions effectively.

2.2.2 Emerging Aerial Threats

The nature of aerial threats is changing rapidly, prompting the need for homeland defense strategies to evolve accordingly. Today's threats are more varied and sophisticated, necessitating that interceptor technologies advance to meet these new challenges. Key emerging threats include:



FIGURE 2.3: surface-to-air missiles (SAMs)
SurfacetoairMissile2025

- **Hypersonic Missiles:**

Missiles like Russias Avangard and Chinas DF-ZF shown in Figure 2.4 can exceed Mach 5 and are capable of executing unpredictable maneuvers. Their extreme velocity and agility make them exceptionally hard to detect and intercept using conventional air defense systems.



FIGURE 2.4: China Hypersonic Missile DF-ZF **DFZF2025**

- **Stealth Aircraft:**

Aircraft such as the Chengdu J-20 and Sukhoi Su-57 shown in Figure 2.5a and 1.1b are designed with stealth technologies that reduce radar visibility, making them difficult to detect and target. As stealth capabilities continue to improve, interceptors will require enhanced sensor fusion, as well as integration into network-centric warfare systems, to successfully engage these aircraft.

- **Unmanned Aerial Vehicles (UAVs):**

Both reconnaissance and armed UAVs, including Turkeys Bayraktar TB2 and the U.S. MQ-9 Reaper shown in Figure 2.6, are being increasingly utilized



(A) Sukhoi Su-57 **SukhoiSu572025**



(B) Chengdu J-20 **ChengduJ202025**

in modern combat. These drones often fly at low altitudes and may operate in large groups, potentially overwhelming traditional defense systems. Swarm tactics where multiple UAVs coordinate attacks simultaneously pose a particularly complex challenge.



FIGURE 2.6: MQ-9 Reaper **GeneralAtomicsMQ92025**

- **Cruise Missiles:**

Weapons such as the U.S. Tomahawk shown in Figure 2.7 and Russias Kalibr remain serious threats due to their low-altitude flight paths and ability to avoid radar through terrain-following methods. Their precision over long distances demands that interceptor systems be equipped with advanced guidance and long-range engagement capabilities.

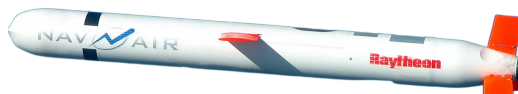


FIGURE 2.7: U.S. Tomahawk **TomahawkMissileFamily2025**

2.3 Design Requirements for Homeland Defense Interceptor Aircraft

The Homeland Defense Interceptor (HDI) is being developed in response to the design goals outlined in the 2024-2025 AIAA Undergraduate Design Team Project Request for Proposal **aiaaRFPHDIAircraft**. This document lays out the key missions, performance expectations, and operational requirements that shape the foundation of the HDIs design. At its core, the RFP emphasizes the need for a mission-tailored aircraft that meets strict operational standards while filling a critical gap in the U.S. homeland air defense system.

Theres a clear demand for a new kind of interceptorne thats affordable, yet capable of responding to a wide variety of aerial threats, from hijacked passenger planes to autonomous cruise missiles. Current high-end fighters like the F-22 and F-35, while powerful, are simply too expensive and not well-suited for mass production or large-scale homeland defense missions.

1. Mission Requirement

The RFP specifies two primary design missions: Defensive Counter-Air (DCA) Patrol and Point Defense Interception. Additionally, an Intercept/Escort mission is considered **aiaaRFPHDIAircraft**. The mission profiles are as follows:

- Defensive Counter-Air (DCA) Patrol Mission

This mission is designed to safeguard friendly airspace by keeping a watchful presence over a designated area and staying ready to respond to any potential threats in the sky. The aircraft essentially acts as both a deterrent and a first line of defense against any unauthorized intrusions.

To effectively carry out this role, the aircraft needs to remain on station for up to four hours during a combat air patrol. This requirement pushes the endurance well beyond what most modern supersonic fighters are typically built to handle as shown im Figure [2.8](#).

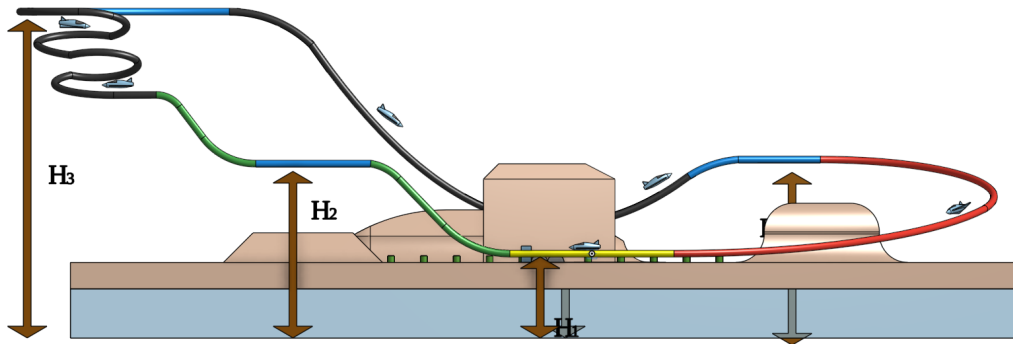


FIGURE 2.8: Mission Profile: Defensive Counter-Air Patrol Mission

TABLE 2.1: DCAP - Mission Segments Description

Phase	Description
1	Take-off and acceleration
2	Climb from sea level to optimum cruise altitude
3	Cruise out 300 nm at optimum speed and altitude
4	Combat air patrol for 4 hours at best loiter speed at 35,000 ft
5	Dash 100 nm at maximum speed at 35,000 ft
6	Combat maneuvers at 35,000 ft, maximum thrust and fuel flow. Fire all missiles and retain gun ammunition
7	Climb/accelerate to optimum speed and altitude
8	Cruise back 400 nm at optimum speed and altitude
9	Descend to sea level
10	Reserves: Fuel for 30 minutes at sea level at maximum endurance speed

- Point Defense Interception Mission

This mission focuses on delivering a rapid response to urgent, localized aerial threats such as incoming missiles or enemy aircraft targeting key infrastructure or high-value assets.

Unlike the extended patrol mission, this operation does not involve loitering. Instead, it emphasizes quick reaction times and longer dash segments to reach the threat area as fast as possible. Despite these differences in timing and distance, the aircraft still performs similar combat maneuvers and carries the same weapon load. Because the mission profile closely mirrors that of a Defensive Counter-Air (DCA)

mission, performance parameters like speed (Mach number) and altitude remain largely unchanged as shown in Figure 2.9.

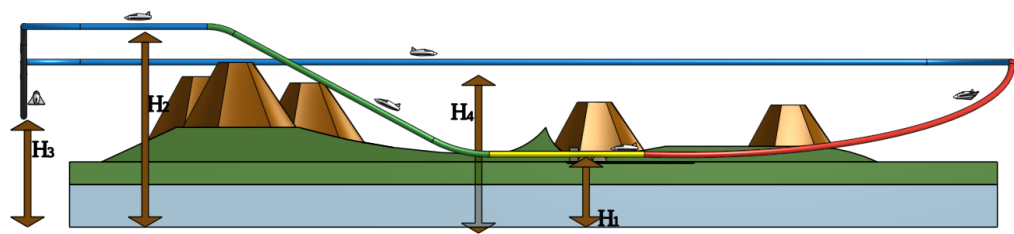


FIGURE 2.9: Mission Profile: Point Defense Intercept Mission

TABLE 2.2: PDI - Mission Segments Description

Phase	Description
1	Take-off and acceleration
2	Climb from sea level to 35,000 ft and accelerate to maximum speed
3	Dash 200 nm at maximum speed at 35,000 ft
4	Combat maneuvers at 35,000 ft, maximum thrust and fuel flow. Fire all missiles and retain gun ammunition.
5	Climb/accelerate to optimum speed and altitude
6	Cruise back 200 nm at optimum speed and altitude
7	Descend to sea level
8	Reserves: Fuel for 30 minutes at sea level at maximum endurance speed

- Intercept/Escort Mission
This mission involves escorting friendly aircraft such as bombers or reconnaissance platforms through contested or potentially hostile airspace to ensure they can complete their objectives and return safely. Unlike the previous missions, this one is not bound by the strict performance criteria outlined in the original request for proposal. Instead, it was designed to evaluate the interceptors combat radius and its ability to operate effectively at lower speeds an important factor when supporting slower-moving or civilian aircraft during escort operations as shown in Figure 2.10.

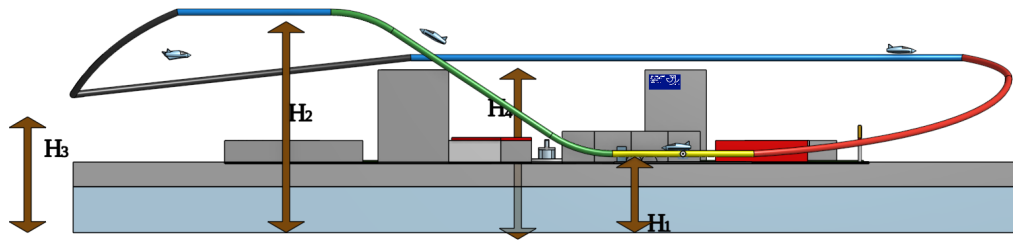


FIGURE 2.10: Mission Profile: Escort Mission

TABLE 2.3: Escort - Mission Segments Description

Phase	Description
1	Take-off and acceleration
2	Climb from sea level to 35,000 ft and accelerate to maximum speed
3	Dash out at maximum speed at 35,000 ft
4	Escort for 300 nm at minimum practical airspeed while retaining all weapons
5	Climb/accelerate to optimum speed and altitude
6	Cruise back at optimum speed and altitude
7	Descend to sea level
8	Reserves: Fuel for 30 minutes at sea level at maximum endurance speed

2. Design Constraints

3. Component List

The total payload of a homeland defense interceptor aircraft plays a crucial role in determining the operational capabilities and mission flexibility. Payload refers to the combined weight of all mission-specific equipment and systems carried on board, excluding the basic aircraft structure, fuel, and propulsion systems. For a homeland defense interceptor, the payload is typically composed of weapons, sensors, communication systems, and additional mission-related equipment as shown in Table 2.5. The payload that consist of air-to-air weapons have the total weight of 802 lbm.

4. Other Requirements

- Standard day conditions with no wind.
- Fuel type: JP-8 or Jet-A, with self-sealing fuel tanks.

TABLE 2.4: List of Design Constraints

Mission Performance		Performance Requirement
Intercept Radius		200 nm
DCA Mission CAP endurance		At 300 nm, duration = 4 Hours radius
Maximum Mach Number		At 35,000 ft: M = 1.6
Maneuver Weight (50% Internal Fuel)		
1-g Specific Excess Power	Military Thrust	0.9M/Sea Level = 200 ft/s, 0.9M/15,000 ft = 50 ft/s
1-g Specific Excess Power	Maximum Thrust	0.9M/Sea Level = 700 ft/s, 0.9M/15,000 ft = 400 ft/s
5-g Specific Excess Power	Maximum Thrust	0.9M/Sea Level = 300 ft/s, 0.9M/15,000 ft = 50 ft/s
Sustained Load Factor	Maximum Thrust	0.9M/15,000 ft
Maximum Instantaneous Turn Rate	Turn	At 35,000 ft = 18.0 deg/s

- Operation from NATO-standard runways (8,000 ft) and austere bases.

2.4 Aircraft Design

2.4.1 Aircraft Design Process

The development of an aircraft is a structured process that evolves through several critical stages to ensure the final product meets performance, safety, and mission requirements. The general sequence of the aircraft design process are illustrated in Raymer's book **raymerAircraftDesignConceptual2006a** that consists of the following phases:

1. Design and Mission Requirement

The first step involves defining the mission profile and operational roles of the aircraft. These requirements are established based on military or commercial needs and include parameters such as range, payload, speed,

TABLE 2.5: Weight Payload Component List

No.	Items	Weight (lb / kg)	Volume (ft ³ / m ³)
Avionics			
1	ICNIA	100 / 45.36	3 / 0.085
2	3 X MFDs	20 / 9.07	1.5 / 0.042
3	Head-up Display	35 / 15.88	1.6 / 0.045
4	Data Bus	10 / 4.54	0.5 / 0.014
5	INEWS	100 / 45.36	3 / 0.085
Flight and Propulsion Control System			
6	Vehicle Management System	50 / 22.68	1 / 0.028
Fire Control Systems			
7	IRSTS	50 / 22.68	1 / 0.028
8	Active Array Radar	450 / 204.12	6 / 0.170
System and Equipment			
9	Electrical Systems (2 Engines)	300 / 136.08	4 / 0.113
10	Auxiliary Power Unit (APU)	100 / 45.36	1 / 0.028
11	Ejection Seat	160 / 72.57	2 / 0.057
12	OBOGS	35 / 15.88	1 / 0.028
13	OBIGGS	35 / 15.88	1 / 0.028
Air-to-Air Weapons			
14	AIM - 120 AMRAAM	327 / 148.32	
15	M61A1 20 MM Cannon	275 / 124.74	
16	Ammunition feed system (500 rounds)	200 / 90.72	
Total Weight:		2,347 / 1,064.96	

altitude, maneuverability, and endurance. This phase sets the foundation for all subsequent design decisions by identifying the critical design drivers.

2. Conceptual Design

In this phase, various design concepts are explored and evaluated. Designers develop multiple configurations and perform preliminary sizing calculations to determine approximate weight, wing area, thrust requirements, and fuel capacity. Analytical tools and historical data are often used to evaluate the feasibility of different design options. The goal is to identify the most promising configuration that satisfies the mission requirements.

3. Preliminary Design

The selected concept is further refined in this phase. Detailed analyses are conducted in aerodynamics, propulsion, structures, flight mechanics, and systems integration. At this stage, design trade-offs are performed to optimize the aircraft performance, and more accurate estimations of weight, balance, and system layout are developed. Computational tools such as OpenMDAO and AVIARY may be employed to simulate and analyze mission performance and subsystem interactions.

4. Detail Design

This phase involves finalizing the design for production. Every aircraft component is fully defined, including dimensions, materials, and manufacturing processes. Engineering drawings, system schematics, and structural details are produced. The integration of all subsystems such as avionics, hydraulics, and landing gear is completed to ensure compatibility and functionality.

5. Prototype, Testing, and Certification

A prototype of the aircraft is constructed and subjected to a series of ground and flight tests to verify design performance and safety compliance. These tests are essential for validating the design assumptions and identifying potential issues. Following successful testing, the aircraft undergoes a certification process to ensure it meets regulatory and safety standards set by aviation authorities such as the FAA or EASA.

This systematic process as shown in Figure 2.11 ensures that the final aircraft design is not only capable of meeting the specified mission objectives but also safe, efficient, and economically viable.

2.4.2 Preliminary Sizing Methodologies

Preliminary aircraft sizing is a critical phase in the design process that establishes the basic parameters of an aircraft to meet specified performance requirements. Initial estimates from empirical methods inform analytical calculations, which in turn reveal inconsistencies or areas for optimization. This necessitates revisiting initial assumptions and refining design parameters until a consistent and feasible

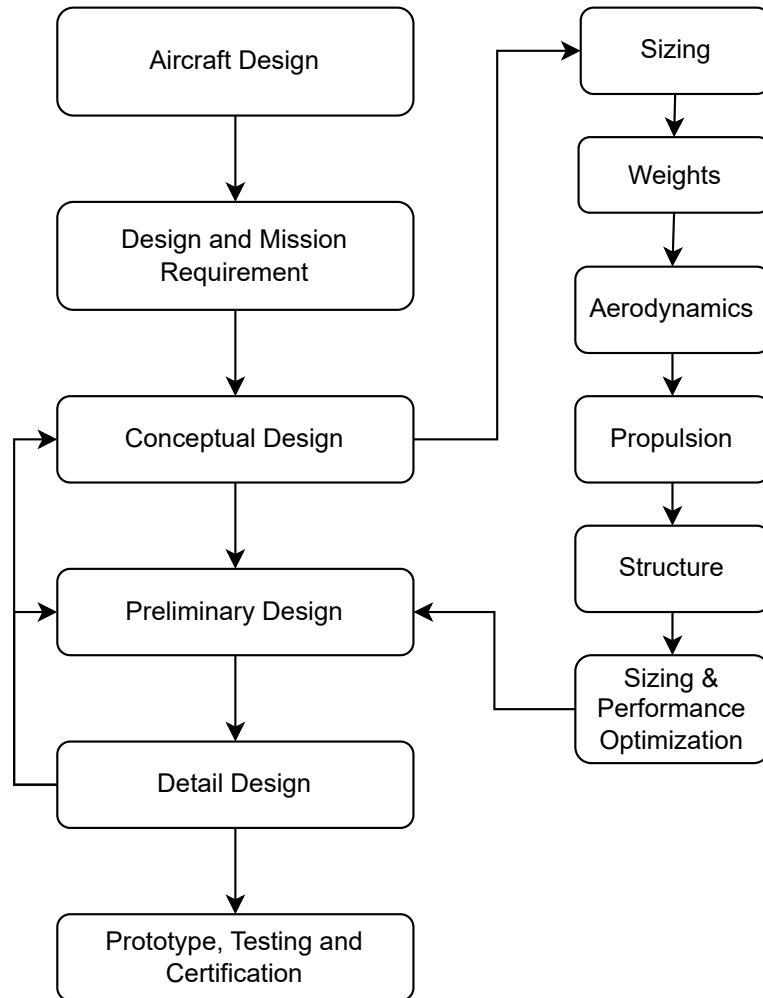


FIGURE 2.11: Aircraft Design Phases

solution that satisfies all requirements is achieved. The interplay between various disciplines aerodynamics, propulsion, structures, and performance means that changes in one area invariably affect others, demanding a continuous feedback loop. This iterative and interconnected nature of aircraft design, spanning from initial requirements through detailed design and into operations, is famously visualized by the design spiral, as illustrated in Figure 2.12. This model emphasizes how each stage of design feeds back into and refines earlier stages, underscoring the necessity for a holistic approach.

1. Mission Definition and Requirements

The first step in any sizing methodology is defining the mission profile of the aircraft. For an interceptor, the mission typically includes:

- Scramble and intercept: The ability to quickly launch and climb to a high altitude to engage a hostile aircraft.
- High-speed engagement: The capacity to reach and sustain supersonic speeds during combat.
- Endurance and loiter: The ability to loiter for extended periods, especially for homeland defense missions where constant patrol may be required.
- Return to base: After mission completion, sufficient fuel for safe return.

2. Initial Weight Estimation

A commonly used method for estimating aircraft weight is Raymers approach **raymerAircraftDesignConceptual2006a**, which divides weight estimation into statistical regression models based on historical data for similar aircraft. This method provides initial guesses for empty weight fractions, which are iteratively refined during the design process. The fuel fraction for military aircraft like interceptors is typically higher due to the need for high thrust and supersonic flight.

(a) Takeoff Gross Weight

The design process starts by calculating to estimate the Take-off Weight W_0 aircraft. The W_0 is a very important design parameter as it sizes the takeoff weight. The W_0 equation used in their analysis, based on input geometry and mission data, provides a starting point for estimating fuel and engine requirements.

$$\begin{aligned} W_0 &= W_{\text{crew}} + W_{\text{payload}} + W_{\text{empty}} + W_{\text{fuel}} \\ &= \frac{W_{\text{crew}} + W_{\text{payload}}}{1 - \left(\frac{W_{\text{empty}}}{W_0} + \frac{W_{\text{fuel}}}{W_0} \right)} \end{aligned} \quad (2.1)$$

where:

- W_{fuel} : Fuel weight.

- W_{payload} : Weight of passengers or equipment.
- W_{empty} : Empty weight of the aircraft.

(b) Fuel weight fraction

$$\frac{W_f}{W_i} = 1.06 \times \left(1 - \frac{W_x}{W_i}\right) \quad (2.2)$$

where:

- $\frac{W_f}{W_i}$: Fuel Fraction for each mission.
- $\frac{W_x}{W_i}$: Weight fraction for each mission.

This equation provides a baseline for sizing interceptors, where the objective is to minimize the *GTOW* while ensuring sufficient fuel for rapid response is crucial.

3. Wing Loading and Thrust-to-weight Ratio

An essential factor in the performance of supersonic aircraft is achieving an optimal balance between wing loading (W/S) and thrust-to-weight ratio (T/W). For supersonic interceptors designed for rapid response and high-speed agility these parameters must be carefully optimized. Lower wing loading contributes to better lift characteristics at lower speeds, whereas a higher thrust-to-weight ratio enables fast acceleration and the ability to sustain supersonic speeds. The following equation of wing loading (W/S) and thrust-to-weight ratio (T/W):

(a) Wing Loading:

$$\frac{W}{S} \quad (2.3)$$

where:

- W : Weight of the wing.
- S : Area of the wing.

(b) Thrust-to-weight-Ratio:

$$\frac{T}{W} = \frac{qC_D}{W/S} \quad (2.4)$$

where:

- $\frac{T}{W}$: Total thrust of the engines.
- $\frac{W}{S}$: Required Wing Loading.
- q : Dynamic pressure
- C_D : Drag coefficient
- n : Load factor

4. Lift-to-Drag ratio

In high-speed flight conditions, a strong thrust-to-weight ratio is vital for countering aerodynamic drag and enabling quick speed changes. Additionally, the lift-to-drag ratio (L/D) significantly influences cruise performance, as it reflects the aircraft's aerodynamic efficiency. This efficiency is governed by the drag equation in combination with the lift characteristics. The drag equation, used in conjunction with lift, defines the overall aerodynamic efficiency:

- Lift-to-Drag ratio:

$$\frac{L}{D} = \frac{C_L}{C_D} \quad (2.5)$$

where:

- C_L : Coefficient of lift .
- C_D : Coefficient of drag.

For interceptors, optimizing the L/D ratio is key to ensuring the aircraft can sustain supersonic speeds while conserving fuel for long-range missions.

5. Required Thrust

The required thrust is estimated using the thrust-to-weight ratio, which is a critical parameter in assessing aircraft performance, particularly for fighters and interceptors. It is calculated using:

$$T = W_0 \times T/W \quad (2.6)$$

where:

- W_0 : Takeoff gross weight
- T/W : Required thrust-to-weight ratio

Raymer **raymerAircraftDesignConceptual2006a** notes that values for T/W typically range between 0.3 to 0.6 for subsonic aircraft and up to 1.2 or higher for highly agile supersonic fighters, depending on mission roles.

6. Wing Area

Wing area is determined based on the wing loading W/S , which relates the aircrafts weight to the surface area of the wing:

$$S = \frac{W_0}{W/S} \quad (2.7)$$

where:

- W_0 : Takeoff gross weight
- $\frac{W}{S}$: Required Wing Loading

This parameter plays a key role in determining takeoff and landing performance, stall speed, and maneuverability. According to Raymer **raymerAircraftDesignConceptual2006a** and Nikolai **nicolaiFundamentalsAircraftAirship2010** theories, wing loading values are selected based on a trade-off between aerodynamic efficiency and operational performance such as field length and rate of climb.

7. Wing Span

Given the wing area and desired aspect ratio AR , the wingspan b is calculated using the inverse form of the aspect ratio equation

$$AR = \frac{b^2}{S} \quad (2.8)$$

where:

- AR : Aspect ratio
- S : Wing Area
- b : Wing Span

Solving for b , the designer can define the span based on aerodynamic efficiency needs. As it stated by Raymer **raymerAircraftDesignConceptual2006a**

and Nikolai **nicolaiFundamentalsAircraftAirship2010**, a higher aspect ratio generally reduces induced drag and is preferred for long-endurance or high-altitude missions.

8. Horizontal and Vertical Tail

Stability and control surfaces are sized using tail volume coefficients. These are empirical values based on historical aircraft data and are defined separately for horizontal and vertical stabilizers.

(a) Horizontal Tail Area

$$S_h = \frac{V_h \times S \times c}{l_h} \quad (2.9)$$

where:

- V_h : Horizontal tail volume coefficient
- S : Wing Area
- c : Mean Aerodynamic Chord
- l_h : Distance from the aircraft CG to the horizontal tails aerodynamic center

Using Raymer's typical values of V_h range from 0.7 to 1.1 for fighters. This ensures adequate pitch stability and control authority.

(b) Vertical Tail Area

$$S_v = \frac{V_v \times S \times b}{l_v} \quad (2.10)$$

where:

- V_v : Vertical tail volume coefficient
- S : Wing Area
- b : Wing Span
- l_v : Distance from the aircraft CG to the vertical tails aerodynamic center

Raymer and Nikolai suggest that values of V_v generally range from 0.02 to 0.07 for military aircraft, depending on mission requirements and whether the aircraft carries external stores or operates at high yaw rates.

9. Fuel Sizing and Endurance

Accurate fuel sizing plays a vital role in defining the interceptor's range and endurance capabilities, particularly during prolonged loitering missions typical of homeland defense operations. To estimate the aircraft's range, the Breguet Range and Endurance equation from Raymer's approach is commonly applied, incorporating key parameters such as lift-to-drag ratio, flight speed, and Specific Fuel Consumption (SFC).

- Range:

$$R = \frac{v}{c} \cdot \frac{L}{D} \cdot \ln \left(\frac{W_i}{W_f} \right) \quad (2.11)$$

- Endurance:

$$E = \frac{\frac{L}{D}}{C} \ln \left(\frac{W_{i-1}}{W_f} \right) \quad (2.12)$$

where:

- R is the range of the aircraft.
- E is the endurance of the aircraft.
- v is the velocity.
- c is the specific fuel consumption (fuel burn per unit thrust per unit time)
- $\frac{L}{D}$ is the Lift-to-Drag ratio
- W_f is the final weight of the aircraft.
- W_i is the initial weight of the aircraft.

2.5 Optimization in Interceptor Aircraft Design

Designing interceptor aircraft involves distinct challenges stemming from their critical role in national defense missions. These aircraft must be capable of rapid deployment, combining high speed, maneuverability, and endurance, all while maintaining low structural weight and cost-effectiveness. The integration of advanced computational tools and multidisciplinary design optimization (MDO) platforms such as AVIARY and OpenMDAO, they have significantly advanced this design process, allowing engineers to analyze complex trade-offs and develop optimized, mission-tailored configurations.

2.5.1 Objectives in Interceptor Optimization

The primary goal of optimization in interceptor design is to ensure the aircraft meets stringent operational requirements while adhering to technical and economic constraints. Key objectives include:

1. Maximizing Agility and Maneuverability:

Interceptors often engage in high-speed aerial combat, requiring tight turn radii, rapid climb rates, and effective evasion capabilities. Achieving superior agility involves optimizing the thrust-to-weight ratio (T/W) and minimizing moment of inertia **satheConceptualDesignStudies2010**.

2. Sustaining Supercruise Performance:

Supercruise capability sustained supersonic flight without afterburners is critical for interceptors to reach targets quickly and efficiently. This requires precise optimization of aerodynamic efficiency (L/D), propulsion system performance, and overall weight **joinerConceptualSizingNext2018**.

3. Maximizing Operational Range:

Although interceptors prioritize speed, they must also have sufficient range to engage targets at significant distances or conduct patrol missions. This involves a delicate balance between fuel capacity, structural weight, and aerodynamic design **takasuPreliminarySizingSupersonic1996a**.

4. Minimizing Radar Cross-Section (RCS):

In modern air combat, stealth capabilities are indispensable. Optimizing the shape and materials of the airframe reduces the RCS, enhancing survivability against advanced detection systems **satheConceptualDesignStudies2010**.

5. Ensuring Mission Effectiveness:

Optimization ensures the aircraft meets specific mission profiles, including rapid climb to engagement altitude, high-speed interception, and safe return to base, while carrying adequate payloads **satheConceptualDesignStudies2010**.

2.5.2 Design Variables in Interceptor Optimization

The optimization process relies on key design variables that significantly impact aircraft performance. These include:

- **Thrust-to-Weight Ratio (T/W):**
A higher T/W ratio ensures rapid acceleration, shorter take-off distances, and superior climb performance. Typical interceptors achieve T/W values greater than 1, enabling sustained vertical climbs **satheConceptualDesignStudies2010**.
- **Wing Loading (W/S):**
Wing loading affects both lift generation and maneuverability. Lower W/S values enhance agility but may reduce structural efficiency and aerodynamic performance at higher speeds **takasuPreliminarySizingSupersonic1996a**.
- **Fuel Fraction:**
Fuel weight as a fraction of total take-off weight is a critical parameter for determining range and endurance. For interceptors, fuel fractions typically range between 25-40% of the total take-off weight **joinerConceptualSizingNext2018**.
- **Aerodynamic Parameters:**
Variables such as wing sweep angle, aspect ratio, and airfoil profile determine the drag characteristics at various speeds. For supercruise, optimizing these parameters minimizes wave drag at transonic and supersonic velocities **satheConceptualDesignStudies2010**.
- **Propulsion Parameters:**
Engine thrust, bypass ratio, and specific fuel consumption (SFC) are optimized to balance high-speed performance with fuel efficiency **satheConceptualDesignStudies2010**.

2.5.3 Multidisciplinary Design Optimization (MDO)

The development of modern interceptor aircraft demands a holistic approach, utilizing multidisciplinary design optimization (MDO) to address the complex interactions among aerodynamic performance, propulsion, structural integrity, and mission-specific requirements. Tools like OpenMDAO and AVIARY streamline this process by automating the interrelated analyses and enabling iterative design improvements.

1. Aerodynamic Optimization:

Aerodynamic efficiency is paramount for interceptors. Using advanced computational fluid dynamics (CFD) and low-fidelity methods for early-stage design, designers optimize L/D for both subsonic maneuverability and

supersonic cruise **takasuPreliminarySizingSupersonic1996a**. Reducing wave drag is critical at supersonic speeds, achieved through optimized wing sweep angles, slender fuselages, and area-ruling principles **satheConceptualDesignStudies**.

2. Propulsion System Optimization:

Interceptors depend on propulsion systems that deliver high thrust-to-weight ratios while maintaining fuel efficiency during super-cruise. Enhancements in engine materials and thermal management systems support performance during prolonged high-speed missions **satheConceptualDesignStudies2010**. Optimizing specific fuel consumption (SFC) across various mission phases such as steep climbs and long-duration patrols is key to improving operational range **satheConceptualDesignStudies2010**.

3. Structural Weight Optimization:

A critical aspect of design is minimizing structural weight without compromising strength. Techniques like topology optimization help eliminate excess material while ensuring structural resilience against aerodynamic and inertial stresses **satheConceptualDesignStudies2010**. High-performance materials such as titanium alloys and carbon fiber composites are favored for their excellent strength-to-weight characteristics **takasuPreliminarySizingSupersonic19**.

4. Stealth Integration:

Reducing radar detectability requires thoughtful design of the aircraft's shape and material selection. Smooth surface transitions and the application of radar-absorbent materials are essential in decreasing the radar cross-section (RCS), thus improving survivability in contested environments **satheConceptualDesignStudies**.

2.5.4 Trade Studies in Optimization

Trade studies are essential for evaluating competing design priorities and achieving an optimal balance between conflicting performance objectives in interceptor aircraft. Several critical trade-offs commonly assessed during the design process include:

- Weight vs. Agility:

Lowering structural weight can improve maneuverability, but excessive weight reduction may negatively impact payload capabilities and structural integrity **joinerConceptualSizingNext2018**.

- Fuel Capacity vs. Range and Weight:

While larger fuel reserves increase operational range, they also add to the aircraft's weight, potentially diminishing its agility. Trade studies help identify the ideal fuel fraction suited to different mission scenarios. **takasuPreliminarySizingSup**

- Supercruise vs. Subsonic Handling:

Designs tailored for efficient supercruise such as specific wing and fuselage configurations can hinder handling at lower speeds. Designers use trade analyses to fine-tune parameters like wing aspect ratio and control surface geometry **satheConceptualDesignStudies2010**.

- Stealth vs. Aerodynamic Efficiency:

Enhancing stealth through features like internal weapon bays and blended surfaces often results in increased drag. Careful trade-off evaluations are necessary to balance reduced radar visibility with acceptable aerodynamic efficiency **joinerConceptualSizingNext2018**.

2.5.5 Case Studies in Optimization

- Supersonic Fighter Jets:

Optimization analyses of lightweight interceptors exemplified by the F-22 Raptor underscore the necessity of harmonizing structural mass, aerodynamic performance, and propulsion efficiency to maintain sustained supercruise capability **joinerConceptualSizingNext2018**.

- UCAV Optimization:

Research on unmanned combat aerial vehicles (UCAVs) frequently employs genetic algorithms to find optimal trade-offs among stealth characteristics, payload capacity, and mission endurance. These findings offer valuable guidance applicable to interceptor aircraft development **satheConceptualDesignStudies20**

2.6 Overview of OpenMDAO and AVIARY

2.6.1 OpenMDAO

OpenMDAO (Open-Source Multidisciplinary Design Analysis and Optimization) developed by NASA, is a powerful open-source computational framework designed to solve complex multidisciplinary optimization challenges. It serves as a valuable platform for integrating various engineering domains, making it especially useful in contemporary aircraft design processes **grayOpenMDAOOpenframework2**

OpenMDAO's modular and flexible architecture supports iterative workflows and promotes collaboration across different technical disciplines. OpenMDAO is particularly effective in implementing Multidisciplinary Design Optimization (MDO), a crucial approach for resolving trade-offs between competing design goals such as minimizing weight, enhancing aerodynamic performance, and improving fuel efficiency.

2.6.2 Workflow and Architecture of OpenMDAO

OpenMDAO is developed to efficiently manage interactions between models, solvers, and optimization routines through a unified interface, making it highly suitable for multidisciplinary design applications in aerospace engineering. Its modular structure promotes scalability, re-usability, and clarity in complex system-level analyses. The key components of OpenMDAO are described as follows:

- **Problem:**
This serves as the top-level entity that governs the overall optimization process. It defines the design variables, objectives, and constraints, and acts as the central interface for running analyses and optimizations.
- **Components:** These are discrete computational units responsible for specific tasks, such as thrust estimation or aerodynamic drag prediction. Each component is designed with explicit input and output definitions, enabling modular and independent operation.
- **Groups:**

Components are organized into hierarchical groups representing major subsystems or disciplinary models (e.g., aerodynamics, propulsion). Grouping allows for structured model development, easier maintenance, and enhanced modularity.

- **Solvers:**

OpenMDAO integrates both nonlinear and linear solvers to address the coupling between different components. Nonlinear solvers, such as Newton-based methods, are used for converging system-level interactions, while linear solvers like Krylov methods handle subproblem linearizations.

- **Driver:**

The driver controls the optimization algorithm, iteratively modifying design variables to optimize the specified objective function under defined constraints. Common drivers include:

- `ScipyOptimizeDriver`: Performs gradient-based optimization using methods from the SciPy library.
- `GeneticAlgorithmDriver`: Used for global search in non-convex problems.

- **Data Connections:** OpenMDAO utilizes explicit and implicit connections to manage data exchange between components and subsystems. These connections ensure data consistency and facilitate the propagation of design sensitivities, which is essential for accurate multidisciplinary optimization.

2.6.3 Benefits of OpenMDAO in Aircraft Sizing Design

The adoption of OpenMDAO in aircraft design offers several key benefits that significantly enhance the design process:

- **Enhanced Design Precision:**

OpenMDAO effectively reduces design inaccuracies by capturing the interdependencies between engineering disciplines for instance, accounting for how structural deflections influence aerodynamic behavior.

- **Accelerated Prototyping:**

The framework's modular structure allows engineers to rapidly construct and evaluate conceptual models, thereby shortening the design iteration cycle and facilitating early-stage decision-making.

- **Resource Efficiency:**

By automating repetitive and complex computational tasks, OpenMDAO minimizes the need for manual calculations, leading to substantial savings in both time and computational effort for multidisciplinary projects.

- **Versatile Optimization Capability Optimization:**

OpenMDAO supports both local and global optimization strategies, enabling the exploration of nonlinear and non-convex design landscapes to identify optimal solutions across a wide range of design scenarios.

2.6.4 AVIARY

AVIARY is a sophisticated multidisciplinary optimization framework developed within the OpenMDAO ecosystem, specifically designed to streamline aircraft design and analysis. It allows the users to design aircraft, and optimize trajectories simultaneously, add their own subsystem and use gradient-based optimization effectively. By integrating key disciplines such as aerodynamics, propulsion, and structural analysis into a unified workflow, AVIARY supports both conceptual and detailed design studies with high efficiency **AviaryDocumentation**.

Leveraging advanced methodologies inspired by NASA's FLOPS (Flight Optimization System) and GASP (General Aviation Synthesis Program), AVIARY enhances model integration and optimization capabilities. Its modular architecture allows for the construction of highly customizable aircraft models, accommodating diverse configurations and mission profiles.

With its flexibility and robust features, AVIARY empowers users at all levels enabling beginners to create foundational models, intermediate users to develop sophisticated designs, and advanced practitioners to tackle complex and innovative projects.

2.6.5 Tools that build within Aviary

AVIARY integrates a suite of computational tools, including OpenMDAO, Dymos, and several legacy NASA-developed systems that have been adapted for its architecture, such as FLOPS and GASP. At its core, AVIARY is built entirely within the OpenMDAO framework, an open-source, Python-based platform for multidisciplinary modeling and optimization. As a result, OpenMDAO handles much of the underlying computational infrastructure, including numerical solving, derivative propagation, and parallel execution. This tight integration also enables seamless compatibility with other models or tools developed within the OpenMDAO environment, enhancing modularity and extensibility across design applications.

AVIARY incorporates foundational methodologies and equations from earlier NASA-developed aircraft design tools, most notably FLOPS and GASP. These legacy tools, which were originally created for designing conventional, particularly commercial, aircraft, have had their computational methods systematically ported into AVIARY, ensuring continuity and reliability in performance prediction. Structurally, AVIARY is entirely developed within the OpenMDAO framework, which serves as the backbone of its architecture. Many of its discipline-specific models, such as aerodynamics, weight estimation, and propulsion, are implemented as individual OpenMDAO systems. In contrast, the framework responsible for integrating these models and conducting mission-level simulations, including time integration and trajectory optimization, is developed using Dymos, which builds upon OpenMDAO's core capabilities.

1. **Dymos:**

Dymos is an open-source library tailored for optimizing dynamic systems, with a primary focus on trajectory optimization. Built within the OpenMDAO framework, it offers advanced time integration schemes, support for transcription methods, and automated results post-processing. Dymos enables AVIARY to perform coupled mission-level design and optimization by simulating time-dependent flight paths under a wide range of operational scenarios.

2. **OpenMDAO:**

OpenMDAO serves as the core computational infrastructure for AVIARY. Developed by NASA, it is a powerful, open-source platform designed for multidisciplinary analysis and optimization (MDAO). One of its key strengths lies in its efficient handling of derivative computations, which allows for robust gradient-based optimization. Through OpenMDAO, AVIARY benefits from modular integration of various subsystems such as aerodynamics, propulsion, and structures while enabling parallel processing and scalable system coupling.

3. FLOPS:

Flight Optimization System (FLOPS) **well'sFlightOptimizationSystem** is a legacy suite of computational modules originally developed for the conceptual and preliminary design of advanced aircraft. Its models have been selectively integrated into AVIARY to enhance accuracy and expand analytical coverage. It consists of six primary modules:

- **Weights:**
Uses empirical/statistical relationships to estimate component weights, with additional analytical capabilities for complex wing geometries.
- **Aerodynamics:**
Generates drag polar for performance evaluation and allows for input of custom polar with scaling options for varying configurations.
- **Propulsion data scaling and interpolation:**
Interpolates and scales engine deck data to deliver performance parameters across different flight regimes, adapting to various thrust requirements.
- **Mission Performance:**
Computes flight performance across multiple segments such as climb, cruise, descent, acceleration, turning, and holding based on integrated aerodynamic, weight, and propulsion data. It also supports supersonic performance assessments and fuel reserve estimations.
- **Takeoff and Landing:**
Assesses takeoff field lengths (including one-engine-out and abort scenarios), landing distances, approach speeds, and climb gradients, ensuring compliance with FAR Part 25 or MIL-STD-1793 standards.

- **Program Control:**
Facilitates point design analysis, parametric sweeps, and nonlinear optimization routines. It allows optimization against objectives like minimum gross weight, fuel burn, or emissions, supporting a wide range of input configurations.

4. **GASP**

Developed by NASA's Ames Research Center, the General Aviation Synthesis Program (GASP) **haugGASPGeneralAviation1978** is a computational tool designed to support the preliminary design of aircraft, particularly in the general aviation category. Originally focused on small, fixed-wing aircraft powered by configurations such as single piston engines with fixed-pitch propellers or twin turboprops/turbofans, GASP has since evolved to accommodate more advanced and unconventional configurations, including hybrid wing-body designs and truss-braced wing architectures.

GASP operates through a series of integrated modules representing key technical disciplines such as aerodynamics, propulsion, structures, and performance which are computationally linked to reflect the interactions between design variables throughout the sizing and analysis process. This integration allows for consistent evaluation of configuration trade-offs and ensures that cross-disciplinary effects are considered in real time.

The tool enables users to perform rapid parametric studies, making it especially useful for tasks such as comparative analysis of aircraft concepts, evaluation of performance metrics and economic factors, sensitivity analysis, and the investigation of how emerging technologies influence design outcomes. GASP thus serves as a valuable component in the broader suite of tools used by AVIARY for conceptual design and optimization of both conventional and advanced aircraft systems.

2.6.6 **Core Functionalities**

1. **Core Subsystem**

AVIARY is organized into five primary subsystems, each responsible for modeling a fundamental discipline in aircraft design:

- **Aerodynamics:**

This subsystem employs empirical methods to evaluate aerodynamic performance. It also allows the import of tabular data, such as drag polar and lift curves, which enhances accuracy by enabling users to leverage high-fidelity aerodynamic data from external sources.

- **Propulsion:**

The propulsion module uses pre-supplied engine data for interpolation and performance analysis. However, it does not support detailed engine cycle modeling, and therefore, must be supplemented by external tools when such modeling is required.

- **Mass:**

Mass estimation is based on empirical relationships that are primarily tailored to conventional aircraft configurations. Nevertheless, AVIARY allows external subsystem integration to support weight prediction for non-traditional or unconventional aircraft designs.

- **Geometry:**

The geometry module is built around statistical relationships optimized for conventional tube-and-wing designs. However, like the mass module, it is extendable via external subsystems to accommodate novel geometries and emerging configurations.

- **Mission Analysis:**

This subsystem handles trajectory analysis using equations of motion based on two degrees of freedom (2DOF) and height-energy formulations. It supports multiple integration methods including collocation and analytic shooting making it suitable for trajectory optimization in both conventional and advanced mission profiles.

2. Pre-mission, Mission, and Post-mission

AVIARY organizes the simulation workflow into three sequential phases:

- **Pre-mission:**

During this phase, the aircraft is initially sized, and all pre-computed values necessary for the mission simulation are generated. This includes data such as weight estimations, fuel requirements, and aerodynamic properties.

- **Mission:**
This phase simulates the aircraft's flight along a prescribed trajectory. The performance is evaluated at discrete points in time (nodes), capturing dynamic behaviors such as fuel consumption, thrust, drag, and altitude variations throughout the mission.
- **Post-mission:**
After mission simulation, this phase computes final performance metrics and conducts post-processing operations. It includes calculations related to landing performance, economic evaluations, emissions, and any other output parameters necessary for further analysis. The post-mission phase has access to outputs from both pre-mission and mission phases, allowing for holistic system evaluation.

3. Integration of External Subsystem

One of AVIARY's key strengths is its extensibility. Users are provided with the capability to incorporate custom or external subsystems alongside the existing core modules. This design philosophy ensures that while the framework maintains a consistent structure, it also remains adaptable to the diverse needs of modern aircraft design projects.

The integration of external subsystems is designed to be both user-friendly and highly flexible, accommodating even complex models or non-traditional configurations. These subsystems can be added as standard OpenMDAO components or groups and can be integrated as shown in Figure 2.16 into any of AVIARY's three primary system phases:

- **Pre-Mission:** External subsystems can be added here to assist in sizing, environmental modeling, or generating input data needed before the mission simulation.
- **Mission:** Users may inject dynamic subsystems that interact with the trajectory, such as adaptive control models, energy storage management, or real-time sensor models.
- **Post-Mission:** Subsystems in this phase may handle economic assessments, detailed noise analysis, emissions modeling, or additional post-processing tasks.

Some of the examples of the external subsystem category:

- Acoustics
- Battery Modeling
- Motor Modeling
- Structural Analysis
- Thermal Management System
- Sensor Packages

4. Optimizer in AVIARY

There are 3 types of Optimizer Driver available in Aviary which are *SNOPT*, *IPOPT* and *SLSQP*. Each optimizer have their own driver, setting and values to be used as shown in Table 2.6

TABLE 2.6: Comparison of Optimizers, Drivers, and Settings

Optimizers	Drivers	Settings
SNOPT	<code>om.pyOptSparseDriver()</code>	Major iterations limit: 50 Major optimality tolerance: 1×10^{-4} Major feasibility tolerance: 1×10^{-6} iSumm: 6
IPOPT	<code>om.pyOptSparseDriver()</code>	tol: 1×10^{-9} mu_init: 1×10^{-5} max_iter: 50 print_level: 5
SLSQP	<code>om.ScipyOptimizeDriver()</code>	tol: 1.0×10^{-9} maxiter: 50 disp: True

5. Types of aircraft and missions AVIARY can design

AVIARY is purposefully designed to offer broad flexibility in modeling and optimizing a wide range of aircraft configurations and mission profiles.

While many of its core subsystems such as those for aerodynamics, propulsion, and weight estimation were originally developed with transport-category aircraft in mind, they are built with modularity that allows for easy augmentation or replacement to suit other aircraft types.

This adaptability has been demonstrated in prior applications of AVIARY, which include the successful design of single- and twin-aisle commercial jets, regional aircraft, and advanced configurations such as truss-braced wings and hybrid-electric propulsion systems. The framework's structure supports modifications to accommodate both conventional and unconventional designs, making it suitable for modern aerospace innovation.

In addition to airframe versatility, AVIARY also supports custom mission definitions, enabling users to design and optimize a variety of flight profiles. Mission architectures can be defined with multiple phases, and users can control which parameter such as altitude, throttle setting, or flight path angle are subject to optimization. This open mission architecture makes AVIARY well-suited for trajectory optimization and mission-level trade studies across civil, military, and experimental aircraft platforms.

2.6.7 Key Features of AVIARY

- **Open-Source Flexibility:**

Built upon the Python-based OpenMDAO platform, AVIARY is a fully open-source aircraft design environment. This allows users to extend or customize existing modules by adding new design variables, analysis methods, or mission profiles, ensuring that the framework remains adaptable across a broad range of aircraft design projects and research applications.

- **Multidisciplinary Integration:**

AVIARY integrates multiple engineering disciplines including aerodynamics, structures, propulsion, and mission analysis into a cohesive modeling framework. This multidisciplinary integration supports complex subsystem interactions, enabling detailed trade studies and comprehensive system-level optimization.

- **Iterative Optimization:**

The design process in AVIARY employs iterative computational loops to refine aircraft parameters. Variables such as wing area, engine thrust, and fuel weight are continuously adjusted until the design meets or exceeds specified performance targets, ensuring convergence to an optimal solution.

- **Scalability:**

The framework is designed to support a spectrum of applications, from rapid conceptual sizing studies to high-fidelity, physics-based simulations. This scalability makes AVIARY a versatile tool for educational purposes, research explorations, and industrial aircraft development.

- **Support for MDO:**

By leveraging advanced optimization algorithms within OpenMDAO, AVIARY effectively manages competing design objectives such as maximizing range, speed, and fuel efficiency to identify balanced, optimal aircraft configurations.

2.6.8 Draw and Run Mission Profile in AVIARY

AVIARY includes a user-friendly built-in graphical interface for mission definition, accessible via the command line. This interactive tool simplifies the process of defining flight missions by allowing users to specify flight phases with parameters such as altitude, Mach number, and optimization settings.

1. Draw the Mission Profile in Aviary

To use the graphical interface, open a command prompt (terminal window) and run the following command:



```
aviary draw_mission
```

FIGURE 2.17: Aviary draw-mission

This will open a new window with two blank axes and some options as shown in Figure [2.18](#).

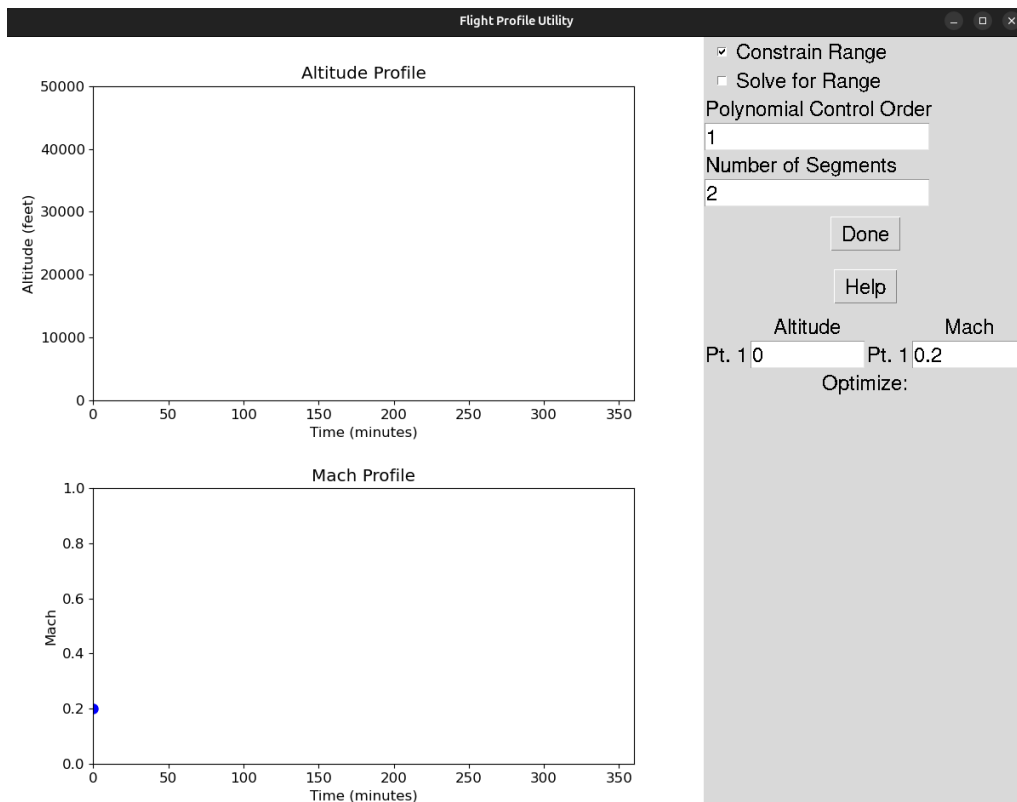


FIGURE 2.18: Flight Profile Utility

The Main component of this GUI flight profile utility are:

- **Altitude Profile:**
Displays the altitude variation over time in a graphical plot. Users can add new altitude points by clicking directly on the plot and adjust existing points through drag-and-drop actions. The interface also supports changing units and axis limits via menu options for greater flexibility.
- **Mach Profile:**
Similar to the altitude profile, this plot shows the Mach number variation throughout the mission. Users can interactively add and modify Mach points by clicking and dragging on the plot, with options to customize units and axes limits through the menu.
- **Optimize Option:**
The GUI allows users to select which flight phases, altitude points, and

Mach values should be included as design variables in the optimization process by simply toggling check boxes. This feature enables targeted and efficient mission optimization tailored to specific design goals.

The AVIARY mission definition interface offers intuitive interactive features that enable precise control over the flight profile:

- **Adding Points:**
Users can add new data points by clicking directly on either the Altitude or Mach plot area. Each point on the Altitude plot corresponds to an altitude value (default in feet) at a specific time (default in minutes). Similarly, points on the Mach plot represent Mach numbers at given times.
- **Dragging Points:**
Existing points on both Altitude and Mach plots are draggable, allowing users to adjust values dynamically for fine-tuning the flight trajectory.
- **Removing Points:**
Points can be deleted by pressing the X button located next to the respective point in the tabular list, facilitating easy modification and cleanup of the flight profile.

As for example as shown in Figure 2.19, it define a relatively simple mission with three phases: climb, cruise, and descent.

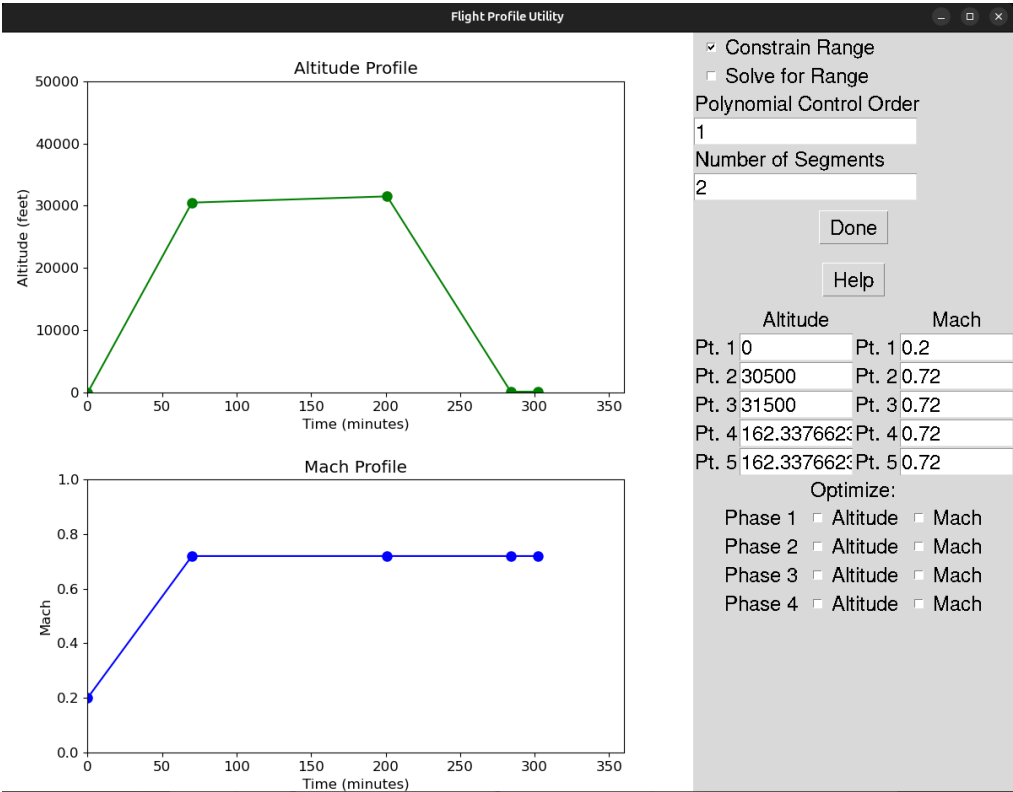


FIGURE 2.19: Drawn Flight Profile Utility

Once done running the GUI of the Flight Profile utility, hit the **Done** button in the top right corner and has been saved to a file called `outputted_phase_info.py` as shown in Appendix B B.4.

The outputted file contains the phase-info dictionary, which holds the flight profile data structured for use in mission simulations. This file could be use for the desire phase parameter for the desired aircraft design model.

2. **Run Mission Simulation**

Once the mission flight profile has been generated, the next step is to simulate the mission using the `run_mission` command as shown in Figure 2.20. This command executes the simulation based on the parameters defined in the `phase_info` dictionary, which is typically saved in a Python file such as `outputted_phase_info.py`.

If you have saved the phase information under a different filename, you can specify it using the `phase_info` flag followed by the path to the desired

file. In the example provided, a benchmark aircraft configuration in .csv format is used as input. However, any valid AVIARY aircraft definition file can be used to simulate a custom mission case.

```
aviary run_mission --phase_info outputted_phase_info.py validation_cases/benchmark_tests/test_aircraft/aircraft_for_bench_FwFm.csv
```

FIGURE 2.20: Aviary Run Mission Simulation

2.6.9 Levels in AVIARY Framework

AVIARY is structured into three levels that increase in complexity and fidelity, allowing users to build up from basic design evaluations to detailed, integrated aircraft analyses. Each level progressively incorporates more sophisticated models, enabling a thorough exploration of design possibilities across various parameters. This section presents an overview of Level 1, Level 2, and Level 3 within the AVIARY framework **UserInterfaceLevels**.

1. Level 1: Baseline Sizing and Conceptual Design

Level 1 of AVIARY serves as the starting point for users who only need basic functionality on basic aircraft sizing and initial design parameter estimation. This level offers a straightforward and accessible approach to aircraft analysis and optimization to establish the general characteristics of an aircraft without delving into detailed subsystem analysis. Users at this level can use AVIARY's expected method to define an aircraft and specify the desired mission through a CSV file. As illustrated in Figure 2.21, the main

inputs for Level 1 include the aircraft model, the types of optimizer, the number of iterations, and the default mission parameters. These inputs feed into the Level 1 process, which then produces a set of design variables, objective metrics, and constraint reports as its output. This forms the basis for subsequent, more sophisticated phases of design and optimization.

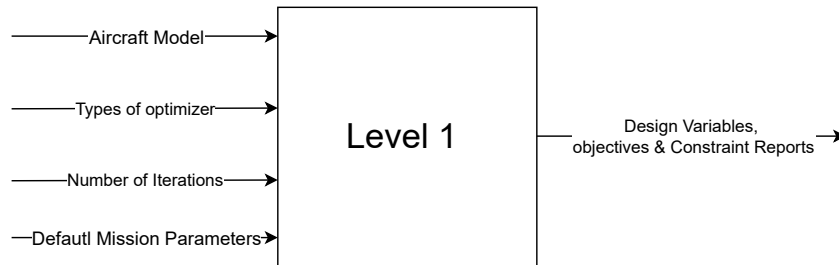


FIGURE 2.21: Level 1 Input Diagram

- Aircraft Model

AVIARY provides samples of the aircraft model. They are all .csv files. This file contains details about the aircraft parameters and its mission. For instance, the file named `aircraft_for_bench_GwGm.csv` represents a mission model for a large single-aisle aircraft.

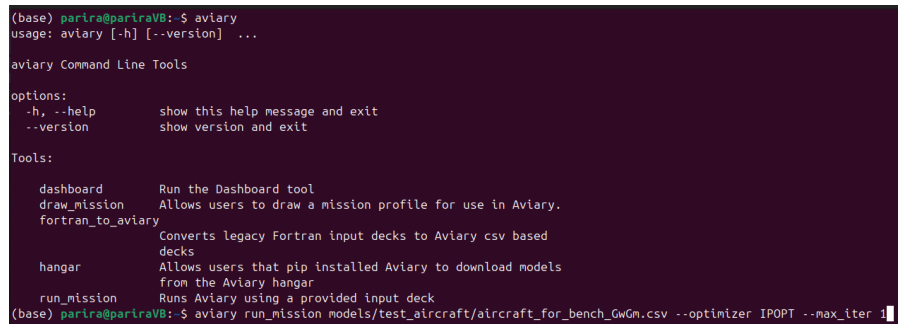
```
aircraft:air_conditioning:mass_coefficient,1.65,unitless
aircraft:anti_icing:mass,551,lbm
aircraft:apu:mass,928,lbm
.....
mission:design:cruise_altitude,37500,ft
mission:design:gross_mass,175400,lbm
mission:design:mach,0.8,unitless
.....
settings:equations_of_motion,2DOF
settings:aerodynamics_method,GASP
settings:mass_method,GASP
.....
actual_takeoff_mass,0
climb_range,0
cruise_mass_final,0
.....
INGASP.ALAR,1.11
INGASP.BENG0B,0.05
INGASP.CINP,0.11
```

FIGURE 2.22: Example Aircraft Model Input File

In an AVIARY input file, you'll find a list of variables used by AVIARY, along with their assigned values and corresponding units, as shown in Figure 2.22.

- Run Level 1

By default, AVIARY allows the optimizer to perform up to 50 iterations to reach an optimal solution. However, in certain cases such as benchmarking, testing, or reducing computation time during early design evaluations it is often desirable to limit the number of iterations. To reduce runtime for such a scenario, the maximum number of optimizer iterations can be limited to a single iteration. For example, to run the `aircraft_for_bench_GwGm.csv` model with this configuration, the model is executed via the command-line interface (CLI) as shown in Figure 2.23 with a specified option to restrict iterations. This approach allows users to quickly validate input configurations or perform rapid assessments without waiting for full convergence.

A terminal window showing the AVIARY command-line interface. The prompt is (base) paritra@paritraVB:~\$. The user enters 'aviary', which displays the usage 'usage: aviary [-h] [--version] ...'. The user then enters 'aviary Command Line Tools', which shows a list of options: '-h, --help' (show this help message and exit) and '--version' (show version and exit). The user then enters 'Tools:', which shows a list of tools: 'dashboard' (Run the Dashboard tool), 'draw_mission' (Allows users to draw a mission profile for use in Aviary), 'fortran_to_aviary' (Converts legacy Fortran input decks to Aviary csv based decks), 'hangar' (Allows users that pip installed Aviary to download models from the Aviary hangar), and 'run_mission' (Runs Aviary using a provided input deck). The user then enters 'aviary run_mission models/test_aircraft/aircraft_for_bench_GwGm.csv --optimizer IPOPT --max_iter 1', which shows the command being executed.

```
(base) paritra@paritraVB:~$ aviary
usage: aviary [-h] [--version] ...

aviary Command Line Tools

options:
  -h, --help            show this help message and exit
  --version              show version and exit

Tools:
  dashboard             Run the Dashboard tool
  draw_mission          Allows users to draw a mission profile for use in Aviary.
  fortran_to_aviary     Converts legacy Fortran input decks to Aviary csv based
                        decks
  hangar                Allows users that pip installed Aviary to download models
                        from the Aviary hangar
  run_mission           Runs Aviary using a provided input deck

(base) paritra@paritraVB:~$ aviary run_mission models/test_aircraft/aircraft_for_bench_GwGm.csv --optimizer IPOPT --max_iter 1
```

FIGURE 2.23: Run Level 1 in CLI

2. Level 2: Mission Analysis and Subsystem Integration

Level 2 in the AVIARY framework builds upon the preliminary sizing results generated in Level 1 by introducing mission-specific performance evaluations and more detailed subsystem interactions. This level serves as a bridge between conceptual design and comprehensive system-level analysis, enabling a more realistic simulation of the aircraft's behavior under operational conditions. A key feature of Level 2 is its support for the integration of user-defined external subsystems. AVIARY facilitates this through

a flexible interface, allowing users to incorporate custom OpenMDAO systems without requiring an in-depth understanding of the internal Python architecture or the full OpenMDAO framework. To include a new subsystem, users simply implement a builder class that conforms to AVIARYs expected format. At this level, the analysis begins to consider critical design factors such as fuel efficiency, aerodynamic drag optimization, and the coupling between structural and propulsion systems. These enhancements provide a more holistic view of aircraft performance, supporting iterative design improvements and mission-tailored optimization.

As illustrated in Figure 2.24, the main inputs for Level 2 include the aircraft model, the types of optimizer, the number of iterations, the mission parameters, the objective to be optimized, and the AVIARY-specific problem formulation. This information feeds into the Level 2 process, which then produces updated design variables, objective metrics, and constraint reports, reflecting the multidisciplinary nature of the aircraft design. The results enable designers to perform more realistic and robust evaluations of their concepts, guiding further design decisions.

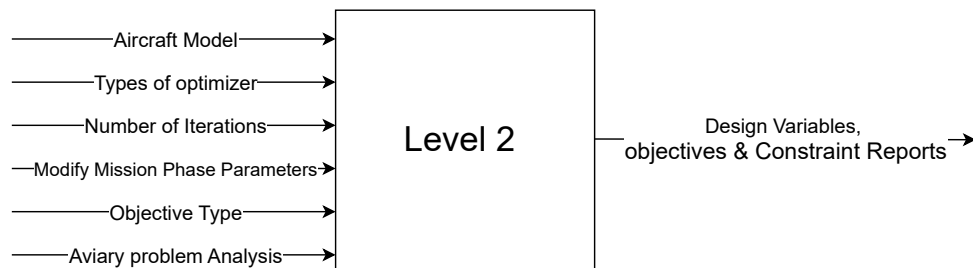


FIGURE 2.24: Level 2 Input Diagram

In the Python script, Level 1 prepares the basic set of arguments and then calls the `run-aviary()` function to execute the sizing analysis. In contrast, Level 2 introduces additional arguments into the script to support the enhanced fidelity and integration of mission-specific and subsystem-level details which are:

- Aircraft Filename:

Specifies the path to the aircraft definition file (`models/test-aircraft/aircraft_for_bench_GwGm.csv`). This file contains key sizing parameters such as geometry, weight, propulsion, and aerodynamic properties.

- **Phase Info:**
A dictionary that defines the mission phases (e.g., climb, cruise, descent), including boundary conditions such as altitude, Mach number, and duration for each phase.
- **Objective Type:**
Specifies the optimization objective for the mission analysis. Common objectives include minimizing fuel burn, maximizing range, or minimizing takeoff gross weight.
- **Analysis Scheme:**
Indicates the numerical method used for solving the equations of motion, such as transcription schemes in Dymos.
- **Optimizer:**
Selects the gradient-based optimizer to be used during the simulation (e.g., *SNOPT*, *SLSQP*, or *IPOPT*).
- **Record File Name:**
Defines the name of the output file used to store optimization results and iteration history for post-processing.
- **Restart File Name:**
Allows the simulation to resume from a previously saved state, reducing computation time in iterative design workflows.
- **Max Iteration:**
Sets the upper limit for the number of optimization iterations, controlling runtime and convergence behavior.

All of the arguments listed earlier are fairly straightforward, except for the

Objective Type. In Level 2, the Objective Type is set to None by default. This means the system automatically chooses the objective based on the Problem Type but only when using the GASP-based mission method. If you are using the FLOPS-based mission method, then the objective must be defined manually. There are three options for problem type that is shown in Table 2.7.

TABLE 2.7: Types of problems for the Objective Type

Problem Type	Objectives
Sizing	Mission.Objective.Fuel
Alternate	Mission.Objective.Fuel
Fallout	Mission.Objective.Range

- **Run Level 2**

To run Level 2, you need to create a Python script to reproduce the run of the `aircraft_for_bench_GwGm` model, which was originally used as an example in Level 1.

However, unlike Level 1 where only basic arguments were needed, Level 2 requires additional arguments and options for more detailed mission analysis and optimization. This includes specifying things like the aircraft file, phase information, optimizer settings, and how many iterations to run as shown in Appendix B B.1.

In the python script, we have the flexibility to modify the phase info parameters for the desired aircraft from default phase info of FLOPS and GASP as shown in Appendix B B.2 and B.3.

The users are granted the flexibility to define external subsystems through the Phase Info configuration. As described in the Custom Subsystem subsection of the AVIARY documentation, multiple categories of external subsystems can be incorporated into the modeling process. These external components may include user-defined aerodynamic models, propulsion modules, or mission-specific control systems. Here are the example python script to applied in the Phase Info as shown in Appendix B B.5.

As shown in that example, it insert the external subsystem of battery and simple weight. This is a simplified example of a component that computes a weight for the wing and horizontal tail. It does not provide realistic computations but rough estimates to `Aircraft.Wing.MASS` and `Aircraft.HorizontalTail.MASS`. When this external subsystem is added to your pre-mission phase, Aviary will compute these weights in its core subsystem as usual, but then the wing mass and tail mass values will be overridden by this external subsystem.

3. Level 3: Detailed Multidisciplinary Optimization (MDO)

Level 3 represents the highest level of fidelity within the AVIARY framework, emphasizing comprehensive multidisciplinary design and optimization (MDO). At this stage, the design process incorporates highly detailed subsystem models and captures the complex inter-dependencies between aerodynamics, propulsion, structural components, mission performance, and other aircraft systems. This level is particularly valuable for refin-

ing aircraft concepts based on realistic performance data and simulating mission-specific behavior with high accuracy. Iterative optimization processes are employed to adjust critical parameters such as wing geometry, thrust levels, and fuel consumption ensuring that the aircraft configuration meets all operational and performance constraints. By integrating detailed

simulations with optimization loops, Level 3 enables engineers to conduct system-level trade studies and arrive at well-balanced, optimal aircraft designs that are ready for advanced development or prototyping phases as illustrate in [Figure 2.25](#).

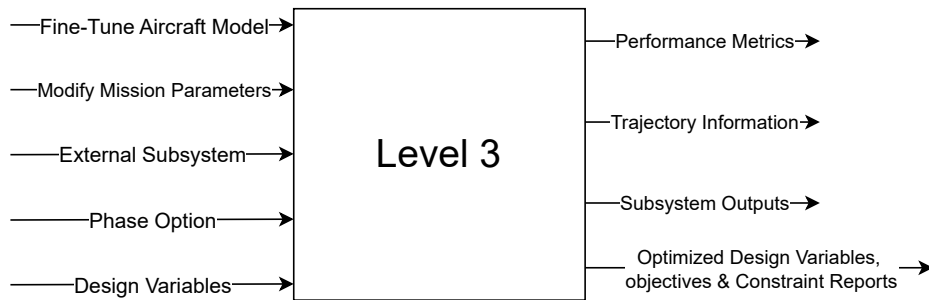


FIGURE 2.25: Level 3 Input Diagram

In the `aviary/validation-cases/benchmark-tests` directory, AVIARY provides a comprehensive full-mission benchmark test for the NASA N3CC aircraft model shown in Appendix B B.6. This example demonstrates the setup and execution of a high-fidelity, multidisciplinary design and optimization (MDO) analysis using AVIARY’s Level 3 interface. Level 3 offers the highest degree of user control, allowing for detailed customization of the aircraft model, mission profile, and optimization parameters. By following this example, users can gain insights into constructing and analyzing complex aircraft models beyond the constraints of predefined templates.

This structured approach facilitates a comprehensive analysis of the N3CC aircraft’s performance across various mission segments, including takeoff, climb, cruise, descent, and landing. By leveraging AVIARY’s Level 3 capabilities, users can perform detailed trade studies and optimization tasks tailored to specific design requirements.

2.6.10 Outputted Result Files

The output files generated by AVIARY vary depending on the type and level of analysis performed. Using the `aircraft_for_bench_GwGm.csv` aircraft model, it generates several output files in .HTML:

1. **Driver_scaling_report.html**

This HTML report summarizes the driver scaling information used during the optimization process as shown in Figure 2.26. After defining all the design variables, objectives, and constraints, and once the optimization problem has been properly configured, this file serves as a centralized summary of the problem setup. The contents are typically divided into three main sections:

- **Design Variables:**
Lists all the variables involved in the optimization process, organized by phase.
- **Constraints:**
Displays the imposed limits or requirements on the system, also grouped by mission phase.
- **Objectives:**
Indicates the primary performance metrics being optimized.

In addition to these sections, the report includes **Jacobian information**, which presents the sensitivities (derivatives) of responses with respect to the design variables. This information is crucial for assessing the behavior of the optimization algorithm and diagnosing potential issues related to scaling or convergence.

Design Variables													
name	size	indices	Driver		Model		ref	ref0	scaler	adder	upper	lower	
			value	units	value	units							
mission:takeoff:ascent_t_initial	1		0.333333		10	s	30		0.0333333		3.33333	0	
mission:takeoff:ascent_duration	1		2.5		25	s	10		0.1		100	0.1	
tau_gear	1		0.2	unitless	0.2	unitless	1				1	0.01	
tau_flaps	1		0.9	unitless	0.9	unitless	1				1	0.01	
mission:design:gross_mass	1		1.00229	lbm	175400	lbm	175000		0.00000571429		2.28571	0.0000571429	
mission:summary:gross_mass	1		1.00229	lbm	175400	lbm	175000		0.00000571429		2.28571	0.0000571429	
traj.accel_t_duration	1		0.129353		13	s	100.5		0.00995025		1.99005	0.00995025	
traj.accel.states:velocity	3		1		250	knot	250	150	0.01	-150	1.2	0	
traj.accel.states:mass	3		1.15764		173646	lbm	150000	0	0.00000666667		6.66667e+15	0	
traj.accel.states:distance	4		0.658315		3.29158	nmi	5	0	0.2		30	0	
traj.ascent.states:flight_path_angle	12		0.139626		0.139626	rad	1	0	1		20	10	
traj.ascent.states:altitude	12		0.5		500	ft	1000	0	0.001		0.7	0	
traj.ascent.states:velocity	12		0.925		185	knot	200	0	0.005		3.5	0	
traj.ascent.states:mass	12		1.15764		173646	lbm	150000	0	0.00000666667		6.66667e+15	0	
traj.ascent.states:distance	12		1.1		10000	ft	10000	0	0.0001		1.5	0	

FIGURE 2.26: Design Variables - Driver Scaling Report

2. Inputs.html

The Inputs.html file provides a sortable and filterable report of all input variables used across the different phases of the `aircraft_for_bench_GwGm.csv`. This HTML report allows for easy inspection and debugging of model inputs and supports an interactive interface for enhanced usability, as illustrated in Figure 2.27.

Upon initial loading, the report displays only those input variables originating from IVC (short for IndepVarComp), which are typically externally provided or user-defined inputs. However, users can expand the view by selecting or deselecting the corresponding checkbox to include other inputs as needed.

The interface allows users to filter input variables based on a variety of criteria, including:

- Input name
- Source name
- Units
- Shape
- Tags
- Value (Val)
- Design Variable status

This report is especially valuable during model setup and verification stages, as it allows users to trace variable definitions, verify initial conditions, and ensure consistency across different mission phases and subsystem inputs.

Inputs Report for aviary									
Input Name	Source Name	Source is IVC	Source is DV	Units	Shape	Tags	Val	Min Val	Max Val
		☒	☐						
aircraft:fuel:fuel_margin	_auto_ivc.v4	✓		unitless	(1,)	[]	[1]	1	1
aircraft:air_conditioning:mass	_auto_ivc.v7	✓		lbm	(1,)	[]	[0]	0	0
aircraft:air_conditioning:mass_scaler	_auto_ivc.v8	✓		unitless	(1,)	[]	[1]	1	1
aircraft:anti_icing:mass	_auto_ivc.v9	✓		lbm	(1,)	[]	[0]	0	0
aircraft:anti_icing:mass_scaler	_auto_ivc.v10	✓		unitless	(1,)	[]	[1]	1	1
aircraft:apu:mass	_auto_ivc.v11	✓		lbm	(1,)	[]	[0]	0	0
aircraft:apu:mass_scaler	_auto_ivc.v12	✓		unitless	(1,)	[]	[1]	1	1
aircraft:avionics:mass	_auto_ivc.v13	✓		lbm	(1,)	[]	[0]	0	0
aircraft:avionics:mass_scaler	_auto_ivc.v14	✓		unitless	(1,)	[]	[1]	1	1
aircraft:blended_wing_body_design:cabin_area	_auto_ivc.v15	✓		ft**2	(1,)	[]	[0]	0	0
aircraft:blended_wing_body_design:passenger_leading_edge_sweep	_auto_ivc.v16	✓		deg	(1,)	[]	[45]	45	45
aircraft:canard:area	_auto_ivc.v17	✓		ft**2	(1,)	[]	[0]	0	0
aircraft:canard:aspect_ratio	_auto_ivc.v18	✓		unitless	(1,)	[]	[0]	0	0
aircraft:canard:characteristic_length	_auto_ivc.v19	✓		ft	(1,)	[]	[0]	0	0
aircraft:canard:fineness	_auto_ivc.v20	✓		unitless	(1,)	[]	[0]	0	0
aircraft:canard:laminar_flow_lower	_auto_ivc.v21	✓		unitless	(1,)	[]	[0]	0	0
aircraft:canard:laminar_flow_upper	_auto_ivc.v22	✓		unitless	(1,)	[]	[0]	0	0
aircraft:canard:mass	_auto_ivc.v23	✓		lbm	(1,)	[]	[0]	0	0
aircraft:canard:mass_scaler	_auto_ivc.v24	✓		unitless	(1,)	[]	[1]	1	1

FIGURE 2.27: Input Reports for AVIARY

3. N2.html

The N2 diagram, also known as an eXtended Design Structure Matrix (XDSM), is a valuable visualization tool provided by OpenMDAO to help users understand and navigate complex system interactions within a model. This matrix-style diagram captures the functional and physical interfaces between system elements, making it easier to systematically identify, define, tabulate, and analyze relationships across the model structure.

In the context of AVIARY, the N2 diagram becomes particularly insightful when running the run-mission command for a given aircraft model, such as `aircraft_for_bench_GwGm.csv`. An example of the resulting N2 output is illustrated in Figure 2.28.

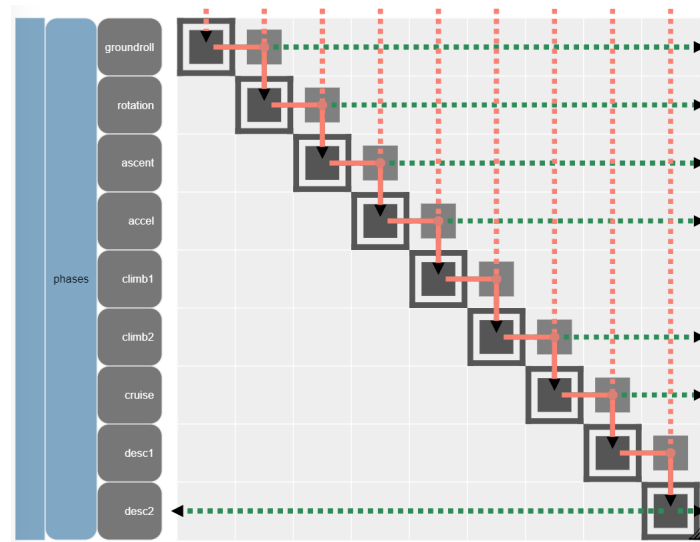


FIGURE 2.29: N2 Phases Diagram

The solid arrow connections in the N2 diagram visually represent the data flow between mission phases. Specifically, they indicate how outputs from one phase serve as inputs for the next. This chaining of phases reflects the sequential nature of flight dynamics within AVIARY's mission analysis. For example, the final state variables of the groundroll phase become the initial conditions for the climb phase, and so forth. This clear representation ensures traceability of data and allows users to verify that each phase is properly initialized from the output of its predecessor, which is critical for maintaining physical and computational continuity throughout the mission simulation.

4. **Opt_Report.html**

This file is an OpenMDAO generated optimization report, which presents all design information in unscaled, physical units for clarity. At the top, it provides a concise summary of the optimization status, including whether convergence was achieved. Below that, it details the objective function, design variables, constraints, and optimizer settings, as illustrated in Figure 2.30. This report is essential for evaluating the performance and feasibility of the optimized aircraft configuration.

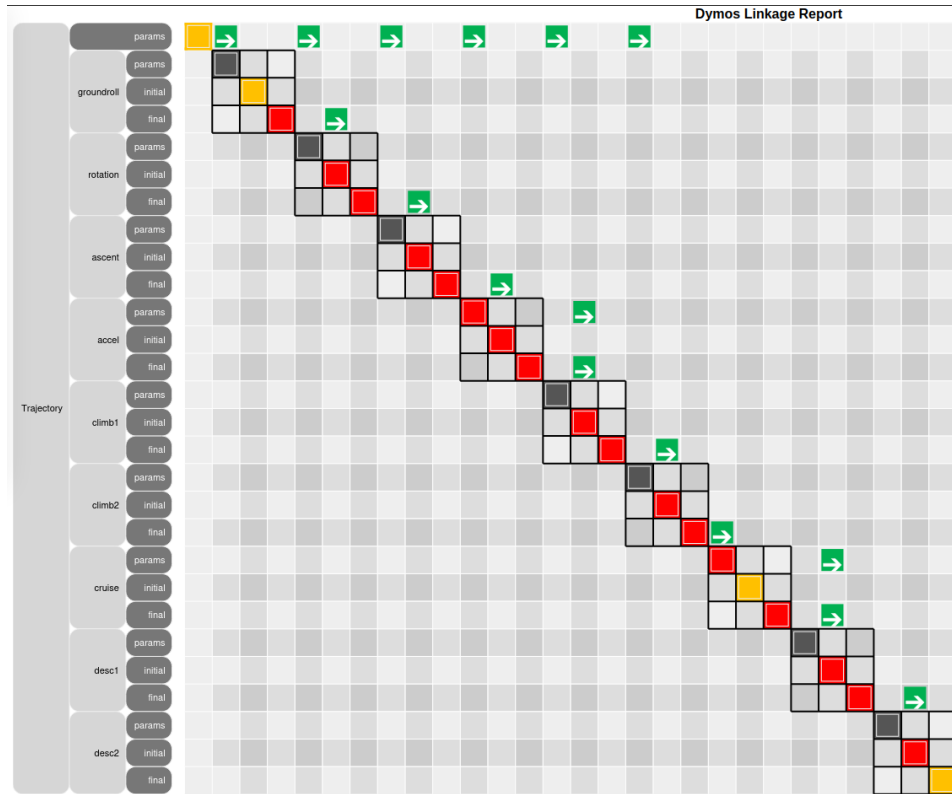


FIGURE 2.31: Dyamos Linkage Report

This tool is particularly useful for identifying inconsistencies or unintended linkages between phases. For instance, it helps ensure that fixed boundary conditions such as takeoff and landing weights, or flight path continuity, are properly enforced. By providing a systematic overview of these linkages, the Traj-Linkage-Report plays a vital role in validating mission setup and improving model robustness within the AVIARY framework.

6. **Traj_Result_Report.html**

This file is one of the most important outputs generated by AVIARY. It allows users to visualize and analyze the optimized mission trajectory of the aircraft. The report includes various tabs containing timeseries data and phase-specific parameters. Based on `aircraft_for_bench_GwGm.csv` aircraft model, the mission is divided into several phases: groundroll, rotation, ascent, acceleration, climb1, climb2, cruise, descent1, and descent2. In the timeseries tab, users can choose which phases to display, as illustrated in

Figure 2.32.

This is one of the key output files generated by the AVIARY framework. It offers a detailed visualization and analysis of the optimized mission trajectory, making it essential for assessing aircraft performance over time and during various mission phases. The report features multiple tabs that display both timeseries data and parameters specific to each phase. For the aircraft model `aircraft_for_bench_GwGm.csv`, the mission is broken down into several discrete phases: groundroll, rotation, ascent, acceleration, climb1, climb2, cruise, descent1, and descent2. Within the time-series tab, users can select and isolate specific mission phases to examine variables such as altitude, Mach number, fuel flow, angle of attack, and thrust-to-weight ratio. This functionality is illustrated in Figure 2.32.

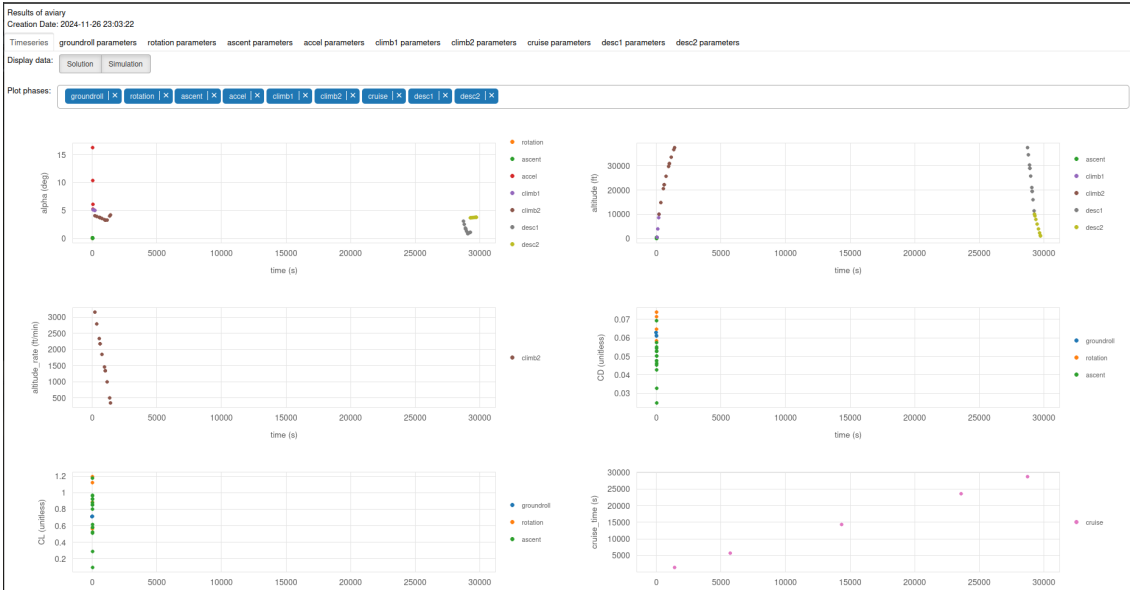


FIGURE 2.32: Trajectory Result Report

Each phase-specific tab contains a detailed summary of key performance metrics and state variables relevant to that segment. For instance, the cruise phase tab, as shown in Figure 2.33, includes data such as cruise altitude, speed, fuel consumption rate, and lift-to-drag ratio. These visualizations are essential for analyzing the behavior and efficiency of the aircraft in each flight phase and for verifying whether mission and design constraints

are being satisfied. This report supports diagnostic validation, performance tuning, and iterative design improvements, making it a powerful tool in both academic research and engineering practice.

Results of aviary
Creation Date: 2024-11-30 21:27:22

Timeseries		groundroll parameters	rotation parameters	ascent parameters	accel parameters	climb1 parameters	climb2 parameters	cruise parameters	descl parameters	desc2 parameters
Parameter		Value								Units
altitude		37500.000022714776								ft
initial_distance		30.547366471141524								NM
initial_time		1234.3748317258866								s
mach		0.8								unitless

FIGURE 2.33: Cruise Parameter from Trajectory Result Report

2.7 Comparative Analysis of AVIARY with Other Design and Optimization Tools

Numerous other framework tools exist for aircraft sizing and design optimization as shown in Table 2.8. However, AVIARY offers unique advantages:

- **Openness and Flexibility:** As an open-source tool built on Python, AVIARY allows customization of modules and the incorporation of new variables as required by specific design goals.
- **Multidisciplinary Optimization (MDO):** AVIARY is highly integrated with OpenMDAO, making it particularly suited for MDO applications, which are essential in balancing the diverse parameters of interceptor design.
- **Modularity:** AVIARYs modular approach enables engineers to focus on specific design aspects, such as aerodynamics or propulsion, without needing to overhaul the entire design.

TABLE 2.8: Comparative Analysis of AVIARY with Other Design and Optimization Tools

Tool	Design Capabilities	Optimization	Analysis Level
AVIARY	Conceptual, Preliminary	Gradient-Based (OpenMDAO)	Multidisciplinary
OpenVSP	Conceptual	Manual or Local Search	Low Fidelity
SUAVE	Conceptual	Metaheuristic (PSO, GA)	Medium Fidelity
XFLR5	Detailed (2D/3D Aero)	None	Aerodynamics (low Reynolds number)
FAST-OAD	Conceptual, Preliminary	Gradient-Based (OpenMDAO)	Multidisciplinary

2.8 Interceptor Aircraft Design Trade Studies

Trade studies play a crucial role in aircraft sizing and design by enabling the systematic evaluation and comparison of different design approaches, configurations, and technologies. Through this analytical process, trade studies help engineers and researchers gain valuable insights into how to balance often competing objectives such as performance, cost, and operational effectiveness.

In the context of supersonic aircraft, mission-specific sizing, and unmanned combat aerial vehicles (UCAVs), various trade studies have been conducted to address key design challenges. These include aerodynamic optimization for reduced drag and improved efficiency, stealth features to minimize radar cross-section, multi-objective trade-offs balancing speed, range, and payload, and mission adaptability to meet diverse operational requirements. Each trade study contributes a unique perspective that informs and guides the overall design process toward optimized and feasible aircraft solutions.

2.8.1 Supersonic Aircraft Design

- **Takasu et al. (1996):**

The study demonstrated effective techniques for sizing supersonic transports with a focus on reducing maximum takeoff weight (MTOW) and improving fuel efficiency. These findings are applicable to interceptors requiring supersonic cruise capabilities for rapid threat response. Mixed-flow turbofan engines with optimized bypass ratios were highlighted as critical for achieving high-speed and efficient propulsion **takasuPreliminarySizingSupersonic1996a**.

- **Furukawa & Makino (2007) :**

Focused on silent supersonic technologies, the research emphasized aerodynamic efficiency and noise reduction. While primarily aimed at civil supersonic aircraft, the findings on drag reduction and sonic boom minimization are relevant for interceptors operating in civilian airspace **furukawaConceptualDesignAero**

2.8.2 Mission Requirement and Aircraft Sizing

- **Parker (1986):**

Highlighted the importance of matching mission-specific scenarios, such as rapid interception and air superiority roles, with design parameters like thrust-to-weight ratio and wing loading. Iterative sizing approaches were employed to balance performance with cost, making this methodology particularly useful for interceptor aircraft that must achieve rapid deployment and high maneuverability **parkerMissionRequirementsAircraft1986**.

2.8.3 Unmanned Combat Aerial Vehicle (UCAV) Design

- **Sathe & Pant (2010):**

Their methodology for UCAV sizing, which included optimizing takeoff weight and wing loading through constraint analysis, provides insights applicable to manned interceptors. The study's focus on low-altitude dash speed and maneuverability constraints aligns with interceptor requirements for high-speed engagements **satheConceptualDesignStudies2010**.

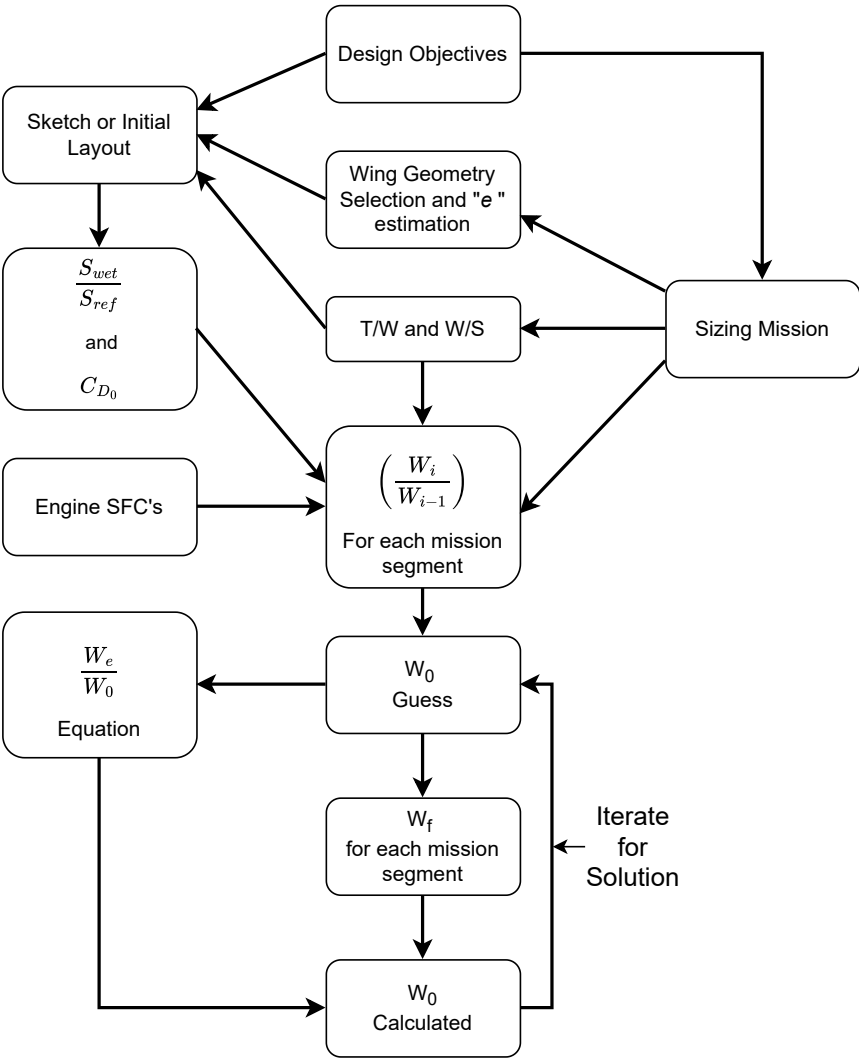


FIGURE 2.12: Sizing Flowchart Diagram
raymerAircraftDesignConceptual2006a



AVIARY

FIGURE 2.13: Aviary AviaryDocumentation

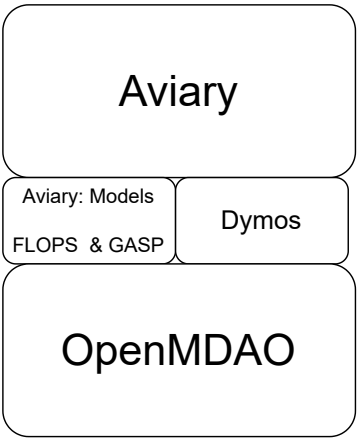


FIGURE 2.14: Aviary Building Tool Blocks **AviaryDocumentation**

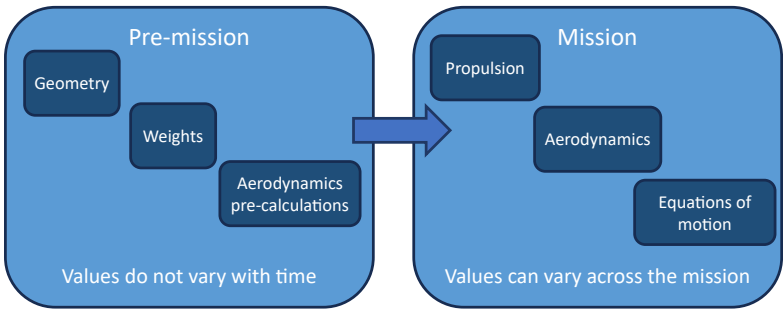


FIGURE 2.15: Pre-Mission and Mission System Diagram **AviaryDocumentation**

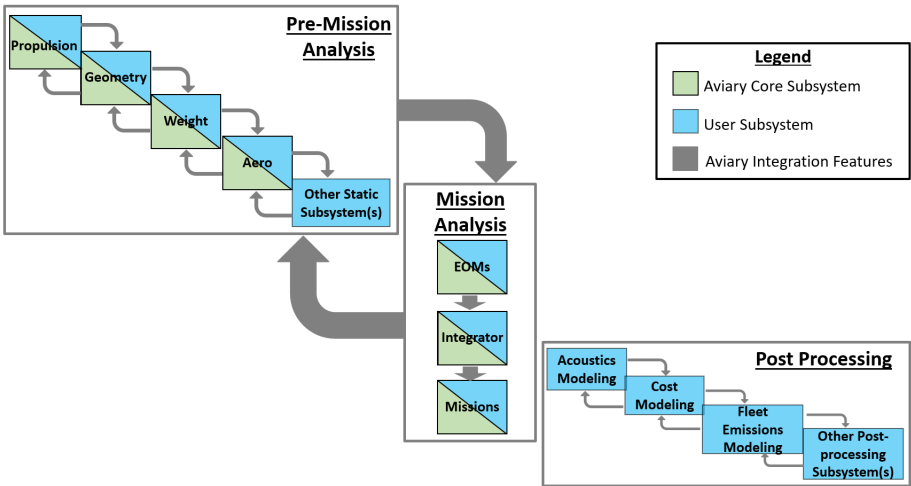


FIGURE 2.16: Add External Subsystem into the Aviary Analysis **AviaryDocumentation**

CHAPTER 3

RESEARCH METHODOLOGY

This chapter defines the research methodology employed to perform the preliminary sizing of the Homeland Defense Interceptor (HDI) aircraft using AVIARY. The methodology is structured to systematically translate the mission requirements defined in the Request for Proposal (RFP) into a feasible aircraft configuration through a step-by-step design and analysis process. The focus of this study is on the conceptual design phase, particularly on preliminary sizing activities, supported by parametric simulation and optimization.

3.1 Research Framework

The research methodology employed in this thesis follows a structured aircraft design process focused on the conceptual design phase, particularly the preliminary sizing of the Homeland Defense Interceptor (HDI). The framework is illustrated in the flowchart in Figure 3.1 and the yellow-highlighted blocks indicate the specific phases covered in this thesis, focusing on the preliminary sizing and early optimization using AVIARY.

3.1.1 Research Flowchart

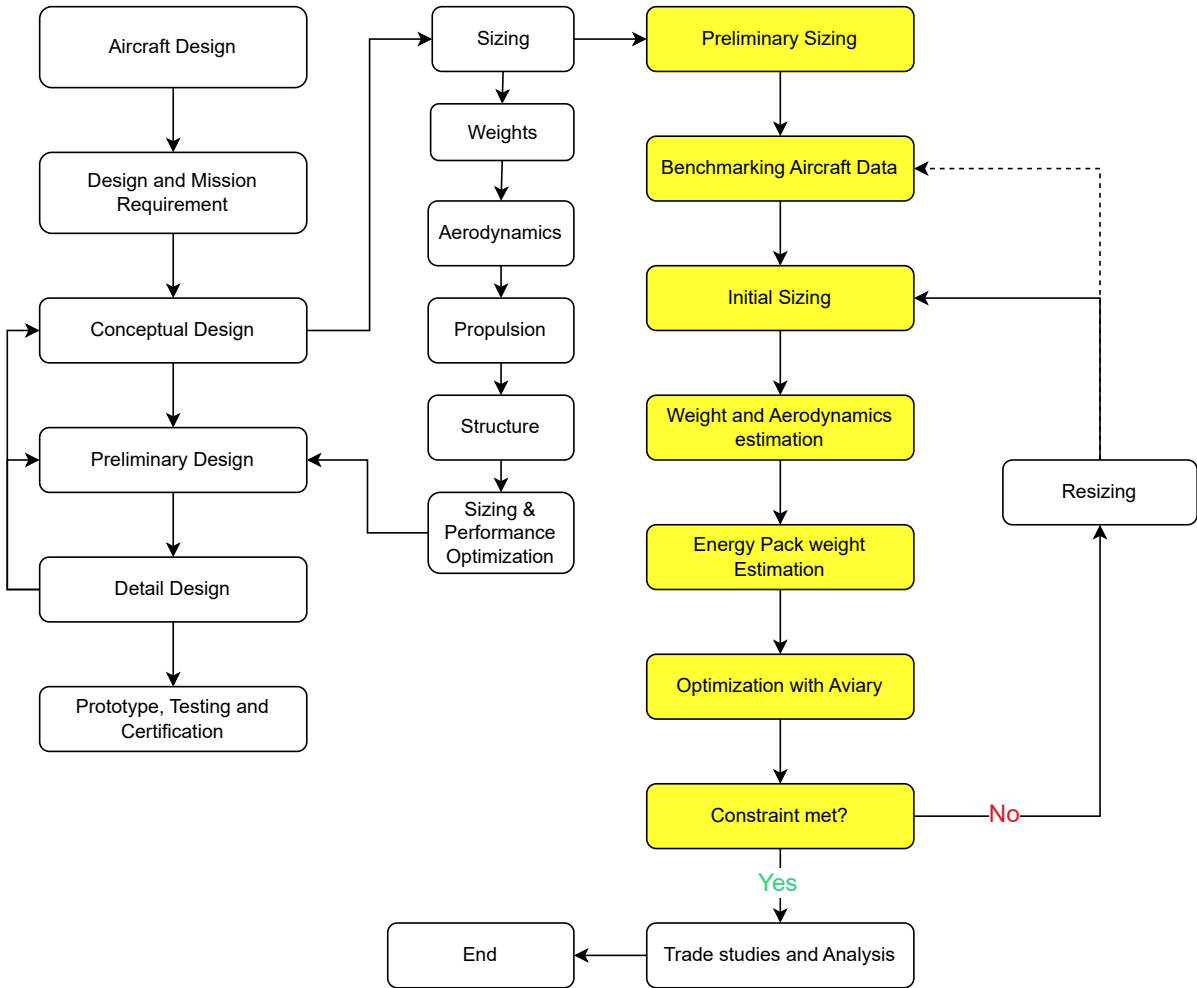


FIGURE 3.1: Research Flowchart

Figure 3.1 represents the steps taken throughout the entire process of making this thesis. The thesis scope is highlighted with yellow color.

3.1.2 Computational Environment

To ensure the reliability, reproducibility, and performance of the simulation and aircraft sizing processes in this research, all computational work was conducted in a controlled and well-documented software environment. The selected tools

and libraries were chosen based on their compatibility with the OpenMDAO framework and the requirements of the Aviary aircraft sizing tool as shown in Table 3.1. This section summarizes the key components of the computational environment used throughout the study.

TABLE 3.1: Computational Environment Used for Simulation

Component	Details
Operating System	Ubuntu 22.04 LTS
Python Version	3.11
Primary Framework	OpenMDAO 3.34.2
Aircraft Sizing Tool	Aviary 0.9.3
Numerical Libraries	NumPy, SciPy
Plotting / Visualization	Matplotlib
Data Handling	Pandas
Environment Management	Python Virtual Environment (venv)
Source Code Management	Git
Execution Platform	Intel Core i7 CPU, 16 GB RAM
Additional Notes	Simulations executed via custom scripts

3.1.3 Design Constraints

Table 2.4 shows the design constraints of the homeland defense interceptor aircraft. Although several performance constraints are outlined in the design requirements including intercept radius, maximum Mach number, and various maneuvering capabilities this study focuses solely on one: the Defensive Counter-Air (DCA) Combat Air Patrol (CAP) endurance. Specifically, the aircraft is required to maintain a four-hour patrol at a distance of 300 nautical miles from base.

This constraint was chosen as the primary sizing driver not only because of its operational significance, but also due to current limitations in the AVIARY framework. At the time of this study, AVIARY does not support direct definition or enforcement of variables such as instantaneous turn rate, specific excess power, or load factor constraints, which prevented those from being included in the sizing analysis.

3.2 AVIARY Framework

In this study, Level 2 AVIARY framework are used and describes the overall aircraft sizing and mission analysis loop as shown in Figure 3.2. The process begins by preparing four major input components:

- **Aircraft Model (CSV file):**
Defines the baseline aircraft configuration, including geometry, weight estimates, propulsion type, and aerodynamic properties.
- **Initial Weight and Aerodynamic Estimations:**
Provides early estimates for takeoff gross weight (W_0), empty weight, fuel weight, and basic aerodynamic characteristics such as lift-to-drag ratio (L/D), based on historical data and preliminary calculations.
- **Design Mission Profile:**
Specifies a mission sequence including different flight segments (e.g., climb, cruise, dash, loiter, combat) with associated performance requirements like altitude, Mach number, and load factors.
- **Energy Pack Estimation:**
An initial estimate of propulsion system mass and fuel requirements based on mission energy needs.

Once these inputs are established, AVIARY conducts an Initial Sizing Block to predict major aircraft parameters such as takeoff weight, wing area, empty operating weight, and fuel consumption. This block also generates mission profile data plots and a performance summary.

Following initial sizing, a Constraint Analysis is performed to verify whether the aircraft meets all mission performance and weight requirements. If the constraints are not satisfied (e.g., insufficient fuel, inadequate range, or performance shortfalls), the aircraft is resized based on updated weights and design adjustments.

If the design passes the constraint checks, it proceeds to the AVIARY Mission Analysis, where detailed evaluation is performed through four modules:

- Aerodynamics
- Structure
- Propulsion

- Mission Analysis

Each analysis block updates and refines the aircrafts flight performance, fuel usage, structural mass distribution, and thrust capabilities.

Finally, a checkpoint evaluates whether the updated takeoff weight and mission performance metrics are satisfied. If they are, the sizing and analysis are complete. If not, the optimization loop continues until all mission and design constraints are fully met.

The outcome of this process is a final, feasible preliminary aircraft design that satisfies all mission requirements and forms the basis for further development.

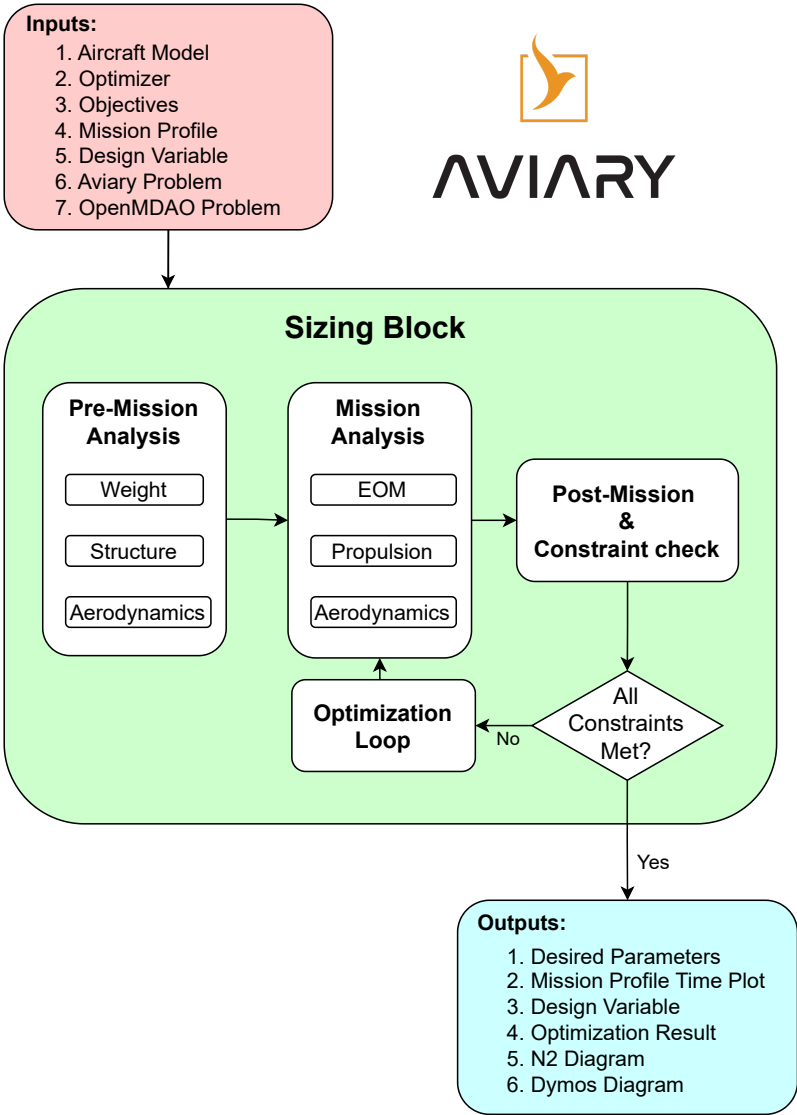


FIGURE 3.2: AVIARY Framework

3.3 Sizing Approach

The sizing methodology involved the following steps:

3.3.1 Benchmarking Aircraft Data Collection

To ensure the validity and relevance of the preliminary sizing process, a benchmark analysis was conducted using publicly available data from a variety of operational manned and unmanned combat aircraft. The goal of this study is to better understand the typical trends in key performance parameters specifically payload versus range, and thrust-to-weight ratio versus wing loading and to use these insights as a reference for validating the design outputs from the AVIARY tool.

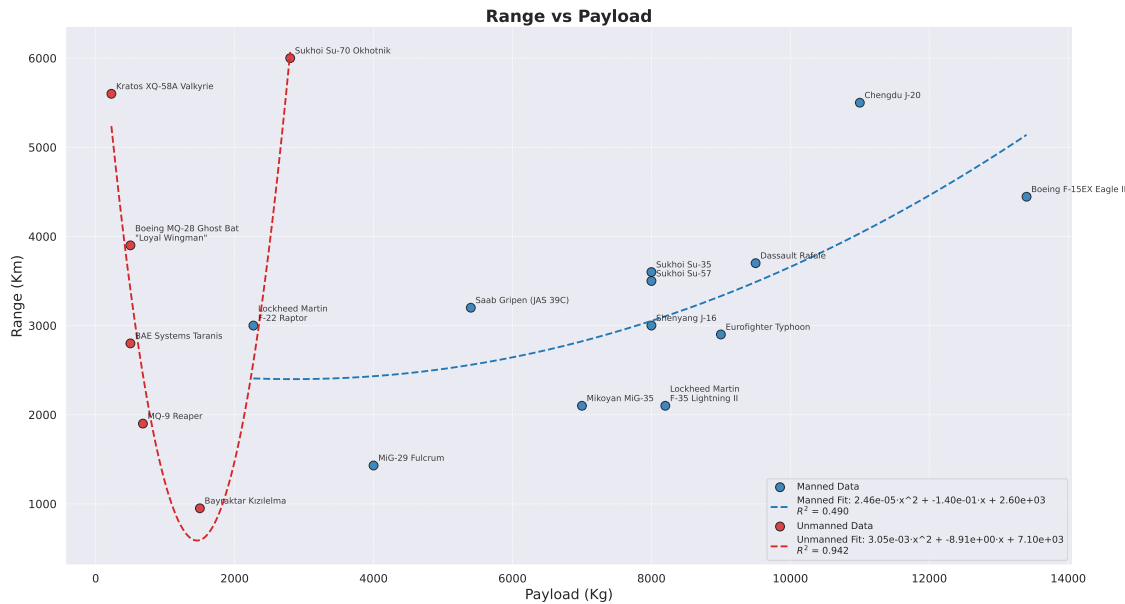


FIGURE 3.3: Range Vs Payload

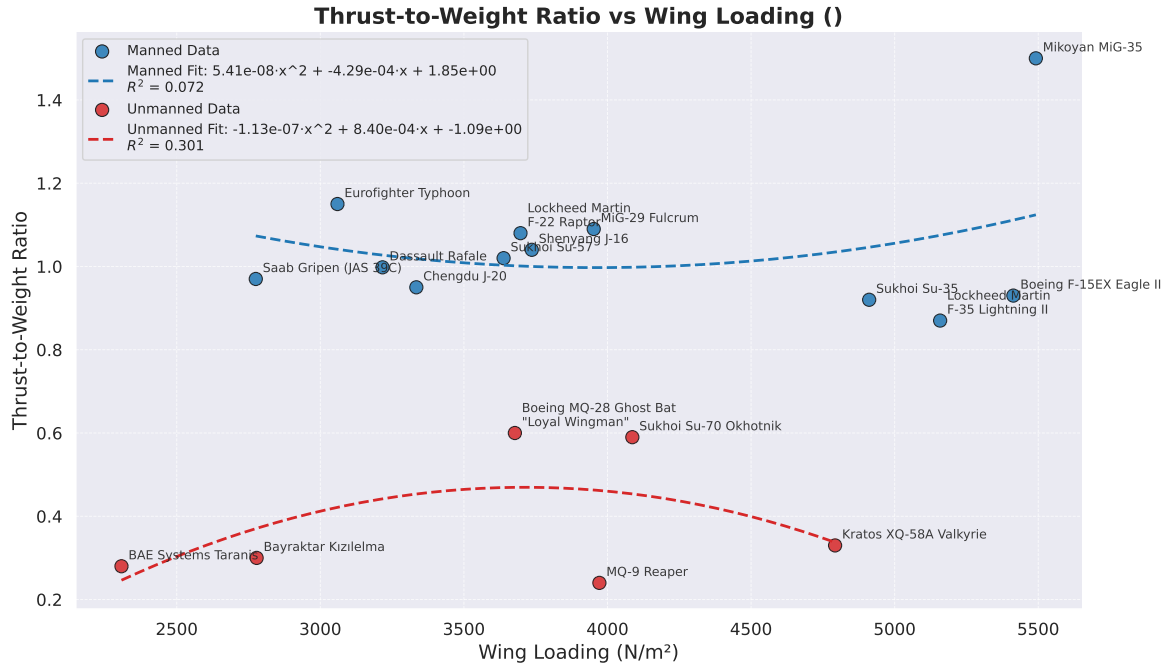


FIGURE 3.4: Thrust-to-Weight Vs Wing Loading

1. Payload vs Range

The first comparison focuses on the trade-off between payload capacity and mission range. This relationship is fundamental in aircraft design, as it highlights how an increase in payload typically reduces the achievable range, and vice versa.

As shown in the Figure 3.3, the data was separated into two groups: manned and unmanned aircraft. Each group was fitted with a second-order polynomial curve to represent the general trend.

- For manned aircraft, the polynomial fit has the form:

$$\text{Range} = 2.46 \times 10^{-5} \cdot \text{Payload}^2 - 0.140 \cdot \text{Payload} + 2600$$

with an $R^2 = 0.490$, the value indicating a moderate correlation. This variability is expected, as manned aircraft often differ significantly in mission roles, payload configurations, and fuel planning strategies.

- In contrast, the unmanned aircraft data shows a much stronger and more predictable relationship:

$$\text{Range} = 3.05 \times 10^{-3} \cdot \text{Payload}^2 - 8.81 \cdot \text{Payload} + 7100$$

with a high value of $R^2 = 0.942$. This strong fit suggests that unmanned systems, often designed for specific roles like surveillance or precision strike, exhibit a more consistent payload-range behavior.

2. Thrust-to-Weight Ratio Vs Wing Loading

The second benchmark evaluates the relationship between thrust-to-weight ratio (T/W) and wing loading (W/S). These parameters are critical in understanding an aircraft's maneuverability, climb performance, and takeoff/-landing characteristics.

- For manned aircraft, the polynomial fit is:

$$T/W = 5.41 \times 10^{-8} \cdot W/S^2 - 4.29 \times 10^{-4} \cdot W/S + 1.85$$

with the result of $R^2 = 0.072$, the value indicating significant spread in the data. This low correlation reflects the wide variety of mission profiles, aerodynamic layouts, and performance requirements among modern fighter jets.

- Unmanned aircraft exhibit a slightly stronger trend:

$$T/W = 1.13 \times 10^{-7} \cdot W/S^2 - 8.40 \times 10^{-4} \cdot W/S + 1.09$$

with $R^2 = 0.301$. While still showing variability, this result suggests a more standardized approach to propulsion and aerodynamic design in unmanned systems, likely due to their more specialized mission envelopes.

A comparative analysis of the selected four benchmark aircraft is shown in Table 3.2. This comparison highlights key performance metrics that are important as the baseline foundation for homeland defense interceptors design in this research.

TABLE 3.2: Aircraft Comparison Table

Aircraft	Type	GTOW (lb)	Payload (lb)	T/W	W/S (lb/ft ²)
F-22 Raptor	Fighter	64,840	5,004	1.08	77.22
Saab Gripen (JAS 39C)	Fighter	19,224	11,905	0.97	57.96
Bayraktar Kizilelma	UCAV	9,920	3,307	0.30	58.02
MiG-29 Fulcrum	Fighter	32,849	8,818	1.09	82.54

3.3.2 Mission Analysis

Table 3.3 shows the comparison of the three missions DCA Patrol, Point Defense Intercept, and Intercept/Escort highlights distinct operational priorities that directly influence the sizing strategy of the interceptor aircraft.

TABLE 3.3: Mission Requirement Comparison for Interceptor Aircraft

Feature / Mission	DCA Patrol	Point Defense Intercept	Intercept / Escort
Mission Duration	Long (1+ hours patrol)	Short (quick reaction)	Medium to Long (escort profile)
Range	Medium	Short	Long
Fuel Requirement	High (loiter, 4 hours)	Low to Medium	Medium to High
Speed Requirement	Medium (cruise + dash)	High (fast intercept)	Medium to High
Weapon Load	Full AAM loadout	Interceptor missile load	Mixed AAM + external tanks
Design Priority	Endurance, awareness	Acceleration, climb rate	Flexibility, range, survivability

By analyzing each mission's performance envelope, a multi mission-capable design can be derived, or a mission-optimized variant can be proposed based on which role is prioritized. The sizing method in AVIARY reflects these trade-offs through parametric input and trajectory-based mission analysis.

3.3.3 Baseline Analysis

- Study of existing interceptor aircraft such as the F-22 Raptor, Saab Gripen (JAS 39C), Bayraktar Kizilelma and MiG-29 Fulcrum.
- Benchmarking the Range, Payload, Thrust-to-Weight ratios and Wing Loading

3.3.4 Initial Sizing and Estimation

Using the insights from benchmarking and Raymer's analytical formulas and typical values, a first-pass sizing is completed. Parameters such as empty weight, fuel weight, and payload are integrated into the calculation of takeoff gross weight (W_0). Wing loading (W/S) and thrust-to-weight ratio (T/W) are then used to estimate wing area, wingspan, and required thrust.

Based on benchmark-informed inputs and preliminary equations, initial values are computed for:

- Takeoff Gross Weight (W_0)
- Wing Area (S)
- Thrust Required (T)
- Wingspan (b)
- Aspect Ratio (AR)
- Takeoff and Landing Max Lift Coefficient (C_{Lmax})
- Takeoff L/D

These parameters serve as initial design foundation to feed into AVIARY's aircraft model input file.

3.3.5 Weight and Aerodynamics Estimation

1. Mission Weight Fractions

Using Breguet formula which is given in Chapter 2 (Equation 2.12 and 2.11) and typical values to estimate the weight fraction for each segment as shown in Table 3.4.

- Cruise Out (300 nm)

$$\begin{aligned}\frac{W_3}{W_2} &= \exp\left(-\frac{R \cdot c}{V \cdot \frac{L}{D}}\right) \\ &= \exp\left(-\frac{300 \cdot 0.8}{480 \cdot 8.7}\right) \\ &= 0.944\end{aligned}\tag{3.1}$$

- **Cruise Back (400 nm)**

$$\begin{aligned}\frac{W_8}{W_7} &= \exp\left(-\frac{R \cdot c}{V \cdot \frac{L}{D}}\right) \\ &= \exp\left(-\frac{400 \cdot 0.8}{480 \cdot 8.7}\right) \\ &= 0.926\end{aligned}\tag{3.2}$$

- **Escort (300 nm)**

$$\begin{aligned}\frac{W_8}{W_7} &= \exp\left(-\frac{R \cdot c}{V \cdot \frac{L}{D}}\right) \\ &= \exp\left(-\frac{300 \cdot 0.7}{270 \cdot 10}\right) \\ &= 0.925\end{aligned}\tag{3.3}$$

- **Combat Air Patrol (Loiter)**

$$\begin{aligned}\frac{W_4}{W_3} &= \exp\left(-\frac{E \cdot c}{\frac{L}{D}}\right) \\ &= \exp\left(-\frac{4 \cdot 0.8}{10}\right) \\ &= 0.786\end{aligned}\tag{3.4}$$

2. Total Mission Weight Fraction

- **DCA Patrol Mission:**

The total mission weight fraction is calculated as:

$$\begin{aligned}\left(\frac{W_{10}}{W_0}\right) &= 0.990 \times 0.985 \times 0.944 \times 0.786 \times 0.977 \\ &\quad \times 0.980 \times 0.990 \times 0.926 \times 0.995 \times 0.980 \\ &= 0.619\end{aligned}\tag{3.5}$$

- **Point Defense Intercept Mission:**

TABLE 3.4: Weight Fraction for each segments

Segment	Weight Fraction
Warm-up and Takeoff	0.990
Climb	0.985
Cruise (300 nm)	0.944
CAP (Loiter)	0.786
Escort (300nm)	0.925
Dash	0.977
Combat maneuver	0.980
Climb (post-maneuver)	0.990
Cruise (400 nm)	0.926
Descent	0.995
Reserve	0.980

The total mission weight fraction is calculated as:

$$\begin{aligned}\left(\frac{W_8}{W_0}\right) &= 0.990 \times 0.985 \times 0.977 \times 0.980 \times 0.990 \\ &\quad \times 0.950 \times 0.995 \times 0.980 \\ &= 0.856\end{aligned}\tag{3.6}$$

- **Intercept/Escort Mission:**

The total mission weight fraction is calculated as:

$$\begin{aligned}\left(\frac{W_8}{W_0}\right) &= 0.990 \times 0.985 \times 0.977 \times 0.925 \times 0.990 \\ &\quad \times 0.970 \times 0.995 \times 0.980 \\ &= 0.825\end{aligned}\tag{3.7}$$

3. Fuel Fraction

By using Raymer's equation given in Chapter 2 Equation 2.2 to obtain each mission fuel fraction as shown in Table 3.5.

4. Takeoff Weight (W_0)

To estimate the takeoff weight using Raymer's formula given in Chapter 2 Equation 2.1, let's assume some parameters which are:

TABLE 3.5: Weight Fraction for each segments

Mission	Weight Fraction	Fuel Fraction
DCA Patrol	0.619	0.40
Point Defense Intercept	0.856	0.15
Intercept/Escort	0.825	0.18

- Payload = 802 lb
- Crew = 300 lbm
- Empty weight fraction = 0.57 (Using Nicolai’s typical value **nicolaiFundamentalsAircr**)
- Fuel weight fraction = 0.40 (DCA Patrol)

$$\begin{aligned} W_0 &= \frac{300 + 802}{1 - (0.61 + 0.36)} \\ &= 36,733 \text{ lbm} \text{ (16,661 Kg)} \end{aligned} \tag{3.8}$$

The result above shows for DCA Patrol mission Takeoff weight estimation which will be served as baseline sizing to be used in other mission profiles. Theoretically, Point Defense Interceptor and Escort Mission will have lighter Gross Takeoff weight that DCA Patrol Mission. As shown the result in Table 3.5, DCA Patrol has bigger fuel fraction than other two missions.

5. Fuel Weight

In this study, the estimation of fuel weight was carried out using a fuel fraction method, widely used in preliminary aircraft sizing. Rather than modeling fuel consumption continuously, this method uses empirically derived fuel weight fractions from Table 3.5 to estimate the total fuel required.

$$\begin{aligned} W_f &= W_0 \times \left(\frac{W_f}{W_0} \right) \\ &= 36,733 \times 0.40 \\ &= 14,693.2 \text{ lbm} \text{ (6,664.7 Kg)} \end{aligned} \tag{3.9}$$

This fuel weight serves as the baseline sizing for the DCA Patrol mission, with the assumption that other missions (Point Defense Intercept and Intercept/Escort) will result in slightly lower fuel requirements due to their lighter fuel fractions.

6. Lift-to-Drag Ratio

The Lift-to-Drag ratio (L/D) is estimated based on the intended mission type, configuration, and benchmarking with existing aircraft of similar class. Rather than detailed aerodynamic modeling, typical values from historical data are used.

For subsonic interceptor aircraft with moderate sweep and clean configuration, L/D values during cruise typically range between 8 and 12. In this study, an average cruise L/D value of 8.6 was assumed based on analogous platforms such as the Saab Gripen and MiG 29, as well as guidance from Raymer and Nicolai approach.

For loiter or CAP (Combat Air Patrol) segments, the aircraft may operate at lower altitudes and optimized configurations, thus slightly increasing L/D. A value of 10.0 was assumed for the loiter phase.

These assumptions are summarized below:

TABLE 3.6: Estimated L/D

Mission Phase	Estimated L/D
Cruise	9.0
Loiter (CAP)	10.0
Dash Segment	7.0–8.0

These values shown in Table 3.6 were used directly in the Breguet range and endurance equations to estimate mission fuel fractions.

7. $C_{L_{\max}}$ Takeoff and Landing

In this study detailed airfoil data is not yet available, so typical values are estimated based on historical data. For a subsonic interceptor with a low-mounted wing and military-style high-lift devices, the following typical values were assumed:

TABLE 3.7: Typical $C_{L_{\max}}$ Values for Takeoff and Landing

Flight Phase	Configuration	Estimated $C_{L_{\max}}$
Takeoff	Flaps/slats deployed	1.7 - 2.0
Landing	Full high-lift configuration	2.2 - 2.6

The following values shown in Table 3.7 were based on Raymer raymerAircraftDesignConc and Nicolai nicolaiFundamentalsAircraftAirship2010.

TABLE 3.8: Estimated $C_{L_{max}}$ Values for Takeoff and Landing

Flight Phase	Estimated $C_{L_{max}}$
Takeoff	1.9
Landing	2.4

Table 3.8 shows the estimated value of $C_{L_{max}}$ that are used as baseline sizing value to be inputted to AVIARY.

8. Thrust-to-weight Ratio

In this study, an initial T/W of 0.98 was selected for baseline sizing, considering the aircraft must achieve rapid climb, efficient patrol, and potential dash phases. This value was derived from historical benchmarking against reference aircraft such as the Saab Gripen and MiG 29 Fulcrum, and adjusted for subsonic operation.

Typical values from Nicolai nicolaiFundamentalsAircraftAirship2010 for subsonic to transonic interceptors are:

- Combat configuration: $T/W = 0.80$ to 1.10
- Cruise/loiter sizing: $T/W = 0.30$ to 0.5

9. Wing Loading

In this study, a baseline wing loading of 82.54 lb/ft^2 was selected. This value was derived from benchmarking aircraft shown in Table ?? the Saab JAS 39C Gripen and similar subsonic-interceptor class aircraft.

10. Wing and Thrust Sizing

To estimate the wing area and required thrust for the homeland defense interceptor aircraft, use the wing loading and thrust-to-weight ratio value from the benchmark plot that shown in Figure 3.4. Let’s try using Mig-29 Fulcrum’s wing loading and thrust-to-weight ratio value where $W/S = 82.54 \text{ lb/ft}^2$ and $T/W = 0.98$. We will be using Raymer’s common formula:

(a) Wing Area

$$\begin{aligned} S &= \frac{W_0}{W/S} \\ &= \frac{36,733}{82.54} \\ &= 445.03 \text{ ft}^2 (41.34 \text{ m}^2) \end{aligned} \tag{3.10}$$

(b) Required Thrust

$$\begin{aligned} T &= W_0 \times T/W \\ &= 26,733 \times 0.98 \\ &= 35,998 \text{ lbf (160.12 kN)} \end{aligned} \tag{3.11}$$

Using the 2 engine configuration, with 17,999 lbf each.

3.3.6 Geometry Estimation

1. Wing Span and Aspect ratio

For a subsonic interceptor, optimized for loiter and agility but not high-altitude efficiency, according to Raymer's the typical value of the aspect ratio for such aircraft is 3.5 - 4. Let's try using $AR = 3.98$. Using the fundamental equation from Raymer's book **raymerAircraftDesignConceptual2006a**:

$$\begin{aligned} AR &= \frac{b^2}{S} \\ b &= \sqrt{AR \times S} \\ b &= \sqrt{3.98 \times 445.03} \\ b &= 42.08 \text{ ft (12.82 m)} \end{aligned} \tag{3.12}$$

2. Horizontal and Vertical Tail

(a) Horizontal Tail Area

$$\begin{aligned} S_h &= \frac{V_h \times S \times c}{l_h} \\ &= \frac{0.9 \times 445.03 \times 10.72}{27.75} \\ &= 154.73 \text{ ft}^2 (14.37 \text{ m}^2) \end{aligned} \tag{3.13}$$

(b) Vertical Tail Area

$$\begin{aligned} S_v &= \frac{V_v \times S \times b}{l_v} \\ &= \frac{0.08 \times 445.03 \times 42.08}{27.75} \\ &= 53.98 \text{ ft}^2 \text{ (5.10 m}^2\text{)} \end{aligned} \tag{3.14}$$

3.3.7 Initial Parameters Used in AVIARY

This sizing step serves as the essential input layer in the full AVIARY modeling chain. The values calculated in this phase are inserted into the Aircraft Model CSV input file, where they define the baseline geometry, mass properties, and propulsion configuration. These inputs are subsequently used in mission simulation, constraint analysis, and performance evaluation throughout the remainder of the design process.

Table 3.9 presents the results of the initial weight and aerodynamic parameter estimation for the proposed homeland defense interceptor aircraft. These values were derived using conceptual sizing methods based on Raymer and Nikolai approach.

TABLE 3.9: List of Weight, Aerodynamics and Geometry initial parameters Estimation

Initial Parameters	
Parameter	Value
W_0 (lb/kg)	36,733 / 16,661
W_{empty} (lb/kg)	20,937 / 9,496
Fuel Weight (lb/kg)	14,693 / 6,664
Payload (lb/kg)	802 / 363.78
Wing Area (ft ²)	445.03 / 41.34
Wing Span (ft)	42.08 / 12.83
Aspect Ratio	3.98
Horizontal Tail Area (ft ²)	154.73
Vertical Tail Area (ft ²)	53.98
Thrust-to-Weight (T/W)	0.98
Wing Loading (lb/ft ²)	82.54
Thrust Needed (lbf/kN)	35,998 / 160.12 kN

These values were estimated using Raymer's empirical weight fraction methods and aerodynamic relationships, and implemented in OpenMDAO to automate parameter estimation. The takeoff gross weight (W_0) accounts for the complete operational mass of the aircraft at mission start, while the empty weight (W_{empty}) includes structural and onboard system components, excluding payload and fuel.

The fuel weight is derived from the mission profile and includes sufficient capacity for loiter, combat, dash, and return-to-base phases. The payload reflects the expected operational equipment and weapon systems for an interceptor role.

Aerodynamically, the aircraft was configured with a wing area of 445.03 ft² and a span of 42.08 ft, resulting in an aspect ratio of 3.98. This choice reflects typical supersonic aircraft characteristics, balancing low drag at high speed with structural compactness.

Performance parameters include a thrust-to-weight ratio of 0.98, which supports high acceleration and vertical performance, and a wing loading of 82.54 lb/ft², indicating emphasis on speed and penetration capability. The required thrust is estimated at 35,998 lbf, which informs the propulsion system selection and validates feasibility against existing engine models.

3.3.8 Engine Deck Selection

Utilized the engine deck model provided by AVIARY as shown in Appendix B [B.7](#) to simulate thrust and specific fuel consumption (SFC) across various flight conditions. This pre-built engine model enabled rapid integration into the simulation framework, ensuring accurate representation of propulsion system performance for trade studies.

3.3.9 Energy Pack Weight Estimation

This stage focuses on the propulsion and fuel system sizing:

- Number of engines and their thrust rating.
- Engine mass based on thrust class.
- Fuel tank capacity requirements to support mission fuel loads and reserves.

Energy pack weight is critical for ensuring that the HDI can sustain long-endurance patrols and high-speed interceptions without exceeding structural limits.

3.3.10 Optimization with AVIARY

The entire aircraft model is simulated within the AVIARY framework. Inputs include:

- Weight breakdown
- Aerodynamics and geometry
- Propulsion data
- Mission phase definitions (climb, cruise, dash, loiter, combat)
- Performance evaluation in terms of trajectory result for each mission simulation.

AVIARY evaluates whether the aircraft can complete the mission within all constraints. If the mission is completed successfully, the design is considered feasible. If not, it progresses to the next step.

3.3.11 Constraint Check

After running simulations, a constraint evaluation is performed:

- Does the aircraft complete the mission within fuel and energy limits?
- Is the dash speed and endurance satisfied?
- Are altitudes requirements met?

If any constraint is not fulfilled, the design proceeds to resizing.

3.3.12 Resizing and Iteration

If performance requirements are not met, resizing occurs. This may involve:

- Adjusting wing area to improve lift and endurance
- Adjusting the altitude speed and duration of each segment to fulfill the missions.
- Increasing engine thrust for better climb and dash.

- Enlarging fuel tanks for extended range.

The updated configuration is re-simulated in AVIARY until all mission requirements are met.

3.3.13 Trade Studies and Analysis

Once a feasible design is achieved, additional trade studies can be performed to optimize:

- Aerodynamic performance (e.g., exploring different wing area, wing span and aspect ratios).
- Weight savings through structural material choices.
- Alternate propulsion options for improved fuel efficiency.

3.3.14 Preliminary Sizing Setup with AVIARY

The preliminary sizing process in this thesis utilizes the Level 2 on boarding structure of the AVIARY framework, as defined in the official documentation **Level2**. This setup provides a more flexible and customizable interface compared to the Level 1 approach, allowing for deeper integration of aircraft design parameters into the simulation workflow. All coding setup also available on [my Gitlab Repository](#).

The steps taken in this setup to build and run the Level 2 mission model were as follows:

1. **Step 1: Aircraft Model in CSV file**

The aircraft model used in this study is structured in a FLOPS legacy format, containing the essential input parameters required by the Aviary framework. This parameters include Gross Takeoff weight (W_O), wing area (S), thrust-to-weight ratio (T/W), and wing loading (W/S), payload, aspect ratio (AR) and other parameters were computed into Aviary Aircraft Model as shown in Appendix A [A.1](#).

2. **Step 2: Insert Phase Info**

Insert phase info that identifies the mission profile information of each mission (DCA Patrol, PDI and Escort) into the python script. In Appendix B

[B.11](#), [B.12](#) and [B.13](#) shows the break down of each mission segments such as takeoff, climb, combat air patrol (CAP), dash, combat maneuver, escort, reserve and descent.

AVIARY's mission analysis framework does not explicitly identify or model distinct mission phases such as dash, acceleration, combat-air-patrol, combat, and escort as separate segments. Instead, these mission profiles are approximated or simplified by treating them as variations of cruise segments. This means that the detailed dynamic behaviors specific to each phasesuch as rapid acceleration during dash, maneuvering during combat, or loitering during air patrolare not individually captured. Rather, the performance characteristics (like speed, altitude, and fuel consumption) for these phases are represented using cruise segment parameters that approximate average or typical conditions.

This approach simplifies the mission modeling within AVIARY by using cruise segments as proxies, enabling the sizing and performance analysis to proceed without requiring complex transient or maneuver-specific modeling. However, it also means that the nuances and specific aerodynamic or propulsion demands of each distinct phase are generalized, which may affect the precision of performance predictions for highly dynamic mission profiles.

3. Step 3: Add Aviary Run Mission arguments

In Aviary's Level 2 interface, the run-mission command provides a flexible way to execute mission analyses with customizable parameters. This command is typically used in a Python environment and allows users to specify various arguments to tailor the simulation to their specific needs as shown in Appendix B [B.14](#). The optimization solver selected for this simulation is IPOPT. IPOPT is well-suited for large-scale nonlinear programming problems and provides robust convergence behavior in the presence of complex constraints, which are common in mission trajectory analyses. It supports sparse matrix operations and barrier methods, making it ideal for optimizing aircraft performance over multiple mission phases.

The COLLOCATION scheme is chosen as the numerical method to solve the dynamic equations of the mission. This method discretizes the time domain

into segments and approximates the state and control trajectories using polynomial basis functions. It is particularly advantageous for missions involving rapid changes in state variables, such as climb and descent. The collocation method offers greater numerical stability and solution accuracy compared to simpler schemes like shooting, especially when dealing with stiff or tightly coupled dynamic systems.

The objective type parameter is set to None, meaning AVIARY set objective to `Mission.Objectives.FUEL` which is Sizing. This configuration is intentionally used during preliminary simulation stages to perform a baseline mission analysis. It allows observation of how the aircraft behaves under nominal conditions using fixed mission profiles, without the influence of an optimization target.

The `aviary_history.db`, indicates the simulation retains a detailed log of state variables, control inputs, fuel usage, and phase transitions throughout the mission. This recorded data can later be visualized or used for post-processing analysis to evaluate aircraft performance, identify potential inefficiencies, and support design refinement.

In this simulation, no restart file is used. Setting `restart-filename = None` indicates that the simulation is executed from scratch rather than continuing from a previous run. This decision is appropriate when conducting initial runs or when modifying mission configurations, as it avoids inheriting any prior state that might bias the analysis.

Lastly, the maximum number of optimizer iterations is deliberately limited to 5. This low iteration count is chosen for debugging and validation purposes, allowing rapid feedback on the setup without committing to long run times.

4. Step 4: Insert Aviary Analysis Problem

The `AviaryProblem` class in the AVIARY framework is used to define, configure, and execute aircraft mission simulations. The following ordered sequence of method calls represents the complete process of setting up and running an aircraft mission using AVIARY as shown in Appendix B [B.15](#).

5. Step 5: Add the Design Variables

To perform parametric studies and potential optimization of the interceptor aircraft mission profile, several design variables were introduced using the add-design-var method from the AVIARY framework. These variables were selected based on their direct impact on aircraft performance, mission feasibility, and aerodynamic behavior. Each variable is defined with a specified range (lower, upper) and a reference value (ref) to guide scaling during optimization or sensitivity analysis as shown in Appendix B [B.16](#). The variables and their purposes are described as follows:

- `av.Mission.Design.GROSS MASS`
This variable represents the takeoff gross weight of the aircraft. It was allowed to vary between 32,000 and 37,000 pounds. This range reflects the expected operational envelope of a lightweight interceptor class aircraft. The reference value is set at 36,733 lb, based on preliminary weight estimation results. Gross mass significantly influences fuel consumption, required thrust, and overall aircraft size.
- `av.Aircraft.Wing.AREA`
The wing platform area is a critical aerodynamic parameter that affects lift generation, wing loading, and stall speed. The area is allowed to vary between 400 and 500 ft², with a reference value of 445.03 ft², consistent with initial sizing outputs. This variable directly affects both takeoff and landing performance.
- `av.Aircraft.Wing.SPAN`
The wingspan defines the lateral extent of the wing and contributes to aspect ratio, induced drag, and structural weight. The span is constrained between 43 and 50 feet. A reference span of 42.08 ft reflects the configuration from baseline sizing.
- `av.Mission.Design.RANGE`
The design range is the mission-specific combat radius or operational range. Here, it is varied between 800 and 1100 nautical miles, with a nominal reference of 1000 NM. This range bracket supports scenarios from short-range interception to regional patrol missions.
- `av.Aircraft.Wing.ASPECT RATIO`
The aspect ratio governs aerodynamic efficiency, especially during cruise.

A range of 3 to 5 is specified, with a baseline value of 3.98. This value represents a balance between structural feasibility and low induced drag, which is suitable for a supersonic-capable airframe.

- `av.Aircraft.HorizontalTail.AREA`

The horizontal tail area influences longitudinal stability and control authority. It is constrained between 150 and 160 ft², with a nominal reference of 154.73 ft², based on tail volume coefficient estimation for a tailed configuration.

- `av.Aircraft.VerticalTail.AREA`

The vertical tail area governs yaw stability and directional control. The area is allowed to vary from 52 to 55 ft², with a reference of 53.98 ft². This design space ensures adequate stability across maneuvering and high-angle-of-attack flight regimes.

- `av.Mission.Takeoff.LIFT OVER DRAG`

This variable represents the aircraft's lift-to-drag ratio during the take-off phase. A higher value typically indicates better aerodynamic efficiency during ground roll and initial climb. The allowed range is 3 to 4, with a reference of 3.5. This variable indirectly influences required thrust and takeoff distance.

- `av.Mission.Takeoff.LIFT COEFFICIENT MAX`

The maximum lift coefficient during takeoff affects stall speed and minimum takeoff distance. It is varied between 1.6 and 2.0, with a reference value of 1.8, representing moderate lift enhancement through leading-edge devices or flaps.

- `av.Mission.Landing.LIFT COEFFICIENT MAX`

Similar to takeoff, this variable governs maximum lift during the landing phase. A higher $C_{L_{\max}}$ allows for slower approach speeds and shorter landing distances. The range is set from 1.8 to 2.5, with a nominal value of 2.2, assuming the presence of high-lift systems such as trailing-edge flaps.

6. Step 6: Print Desired Variables

After running the optimization simulation using AVIARY, the last step involves retrieving the computed parameters that define the aircrafts geometry, performance, and mission-specific metrics as shown in [Appendix B B.17](#).

3.4 Limitations

- The aerodynamic and propulsion models rely on empirical approximations.
- Real-world operational factors such as atmospheric disturbances are not modeled.
- The scope is limited to preliminary design; detailed system-level analysis is excluded.
- Supersonic performance is not analyzed, as the design focuses exclusively on subsonic regimes.

CHAPTER 4

RESULTS AND DISCUSSIONS

4.1 Introduction

This chapter presents the results of the preliminary sizing of the homeland defense interceptor aircraft using AVIARY. The discussion emphasizes the critical design parameters, performance characteristics, and their alignment with the mission objectives. Key findings are analyzed in the context of design goals, ensuring clarity and relevance to the objectives of the study.

4.2 Aircraft Sizing Results

The refined parameters were tested using AVIARY, producing the following results for each mission:

TABLE 4.1: Sizing Results for Different Missions

Parameter	Initial	DCA Patrol	Point Defense	Intercept/Escort
Gross Weight (lb)	36,733	36,066	35,905	36,000
Range (nmi)	800	800	500	500
Wing Area (ft ²)	445.03	486.61	486.42	486.50
Wing Span (ft)	42.08	42	42	42
Aspect ratio	3.98	3.98	3.98	3.98
Horizontal Tail Area (ft ²)	153.46	153.46	153.46	153.46
Vertical Tail Area (ft ²)	53.98	53.98	53.98	53.98
Thrust Required (lbf)	35,998	35,500	35,500	35,500
$C_{L_{Max}}$ Takeoff	1.8	1.8	1.8	1.8
$C_{L_{Max}}$ Landing	2.5	2.5	2.49	2.5
Take-off L/D	3.55	3.55	3.55	3.55

Table 4.1 shows the changes of the HDI design from its initial sizing through three key mission profiles: DCA Patrol, Point Defense, and Intercept/Escort. Each

mission scenario introduces small yet meaningful refinements to the aircrafts configuration to optimize it for specific operational roles.

The initial gross weight of 36,733 lb was refined to 36,066 lb for the DCA Patrol mission and slightly reduced for Point Defense (35,905 lb) and Intercept/Escort (36,000 lb). These changes reflect on fuel differences across all three mission. The wing area increased from 445.03 ft² in the initial design to approximately 486.5 ft² across all three mission-specific configurations. A slight reduction in thrust required is seen from 35,998 lbf initially to 35,500 lbf in the final designs. Other parameters remain unchanged across all mission profiles.

4.3 Analysis

The configuration adjustments shows in Table 4.1 made during the mission-specific sizing process demonstrate a strategic refinement of the HDI design, leveraging the modular capability of the AVIARY tool to adapt the aircraft for varying operational demands without a complete redesign.

The increase in wing area across all missions reflects a deliberate attempt to improve the aerodynamic efficiency and maneuverability of the aircraft, particularly at lower speeds during takeoff and landing. This change resulted in a reduced wing loading, which benefits overall handling qualities and contributes to the aircrafts operational flexibility.

The gross weight adjustments were relatively minor but purposeful. For shorter-range missions like Point Defense and Intercept/Escort, fuel capacity and onboard systems were optimized to reduce unnecessary weight, resulting in improved climb rates and potentially lower fuel consumption. These reductions in weight directly influenced the thrust requirement, allowing for a drop of nearly 500 lbf while maintaining performance goals.

It is important to note that the aerodynamic coefficients and tail sizing remained unchanged throughout the mission profiles. This consistency suggests that the original aerodynamic assumptions were robust and that the control surface sizing was sufficient across all considered mission conditions.

Overall, these adjustments confirm that the initial design was well-calibrated, requiring only minor refinements to meet the distinct performance needs of various homeland defense scenarios. The ability to tailor the aircraft for each mission while preserving aerodynamic integrity and propulsion efficiency illustrates the flexibility and power of AVIARYs mission-based design framework, reinforcing its suitability for conceptual and preliminary aircraft design.

4.4 Comparison with Selected Aircraft

TABLE 4.2: Comparison of HDI Design and Selected Aircraft

Parameter	HDI Design	F-22 Raptor	Gripen JAS 39C	Bayraktar Kzlelma	MiG-29 Fulcrum
Gross Weight (lb)	36,066	64,860	19,224	Not Available	32,849
Wing Area (ft ²)	486.61	840	320	Not Available	409
Wing Span (ft)	42	44.5	27.6	32	37.3
Aspect Ratio	3.98	2.35	2.35	Not Available	3.4
Thrust (lbf)	35,500	70,000	18,100	9,900	36,660
Range (nmi)	800	1,839	810	500	890
Thrust-to-Weight (<i>T/W</i>)	0.98	1.08	0.97	Not Available	1.09
Wing Loading (lb/ft ²)	74.21	77.2	58	Not Available	83

Table 4.2 presents a comparative analysis between the Homeland Defense Interceptor (HDI) design and the selected aircraft, namely the F-22 Raptor, Gripen JAS 39C, Bayraktar Kzlelma, and MiG-29 Fulcrum. The comparison highlights the key sizing and performance parameters such as gross weight, wing area, thrust, range, and aerodynamic ratios.

The HDI exhibits a gross weight of 36,066 lb, placing it between the heavier F-22 (64,860 lb) and the lighter Gripen (19,224 lb). With a wing area of 486.61 ft² and a wingspan of 42 ft, the HDIs design is optimized for subsonic performance and low-to-moderate wing loading. The aspect ratio of 3.98 is notably higher than those of the F-22 (2.35) and MiG-29 (3.4), indicating enhanced aerodynamic efficiency and favorable loitering performance.

In terms of propulsion, the HDI requires 35,500 lbf of thrust, yielding a thrust-to-weight ratio of 0.98, which is similar to the Gripen (0.97) and just below the MiG-29 (1.09) and F-22 (1.08). This ratio supports rapid climb and acceleration performance, suitable for point-interception and patrol roles. The range of 800 nmi is sufficient for homeland defense missions, falling between the Gripen (810

nmi) and MiG-29 (890 nmi), though well below the F-22s extended 1,839 nmi reach.

The wing loading of 74.21 lb/ft² places the HDI in a moderate range lower than the MiG-29 (83 lb/ft²) and F-22 (77.2 lb/ft²), yet higher than the Gripen (58 lb/ft²). This balance reflects a compromise between high-speed performance and maneuverability.

Figure 4.1 provides a performance envelope plot of various combat aircraft, plotting thrust-to-weight ratio (T/W) against wing loading (W/S) in SI units (N/m²). The plot includes both manned fighters (e.g., F-22, F-35, J-20, MiG-35, Rafale, Typhoon) and unmanned combat air vehicles (UCAVs) (e.g., Bayraktar Kzlelma, MQ-28 Ghost Bat, Su-70 Okhotnik). Regression trends are fitted separately for manned and unmanned platforms.

The HDI design falls squarely within the performance envelope of modern manned multirole fighters, with a wing loading of approximately 3615 (N/m²) and a thrust-to-weight ratio near 0.98. Its proximity to aircraft such as the Gripen JAS 39C and MiG-29 Fulcrum demonstrates that the HDI was sized for similar performance expectations: high responsiveness, efficient subsonic cruise, and moderate loiter capability.

The manned aircraft trendline exhibits a wide spread in values with a weak positive correlation, while unmanned aircraft tend to cluster in lower thrust and lower wing loading zones, optimized for endurance rather than speed or agility. The HDI's location away from the UCAV trend confirms that it was designed to fulfill interceptor-level mission agility and climb performance, not endurance-focused surveillance or loitering.

4.5 Aviary Mission Performance Analysis

The Aviary mission performance analysis provides a detailed look into the aircraft's behavior across different mission segments.



FIGURE 4.1: T/W Vs W/S of HDI Design

4.5.1 DCA Patrol Mission Analysis

The highest rate of mass loss occurs during the climb phase as shown in Figure 4.2, which is expected due to high engine thrust. In cruise segment show relatively stable mass with minimal fuel consumption, likely due to a simulation of dynamic maneuvering. The climb phase exhibits a high energy gain rate, demonstrating the aircrafts strong thrust-to-weight ratio. Cruise phases show low and stable energy rates, reflecting efficient level flight. Spikes in energy rate during certain cruise segments likely correspond to maneuvering or altitude changes. Thrust levels are high during climb. Thrust spikes in cruise segments indicate increased power demands for acceleration or maneuvers.

4.5.2 PDI Mission Analysis

Mass decreases from approximately 16,250 kg to 15,000 kg as shown in Figure 4.5. The rate of mass decrease is lower in cruise than climb, showing improved fuel efficiency at cruising altitude. Drag remains low and steady during cruise, indicating efficient aerodynamics. In Figure 4.6, a sharp drag increase in the cruise1 segment due to speed changes. Fuel consumption is lower in cruise than

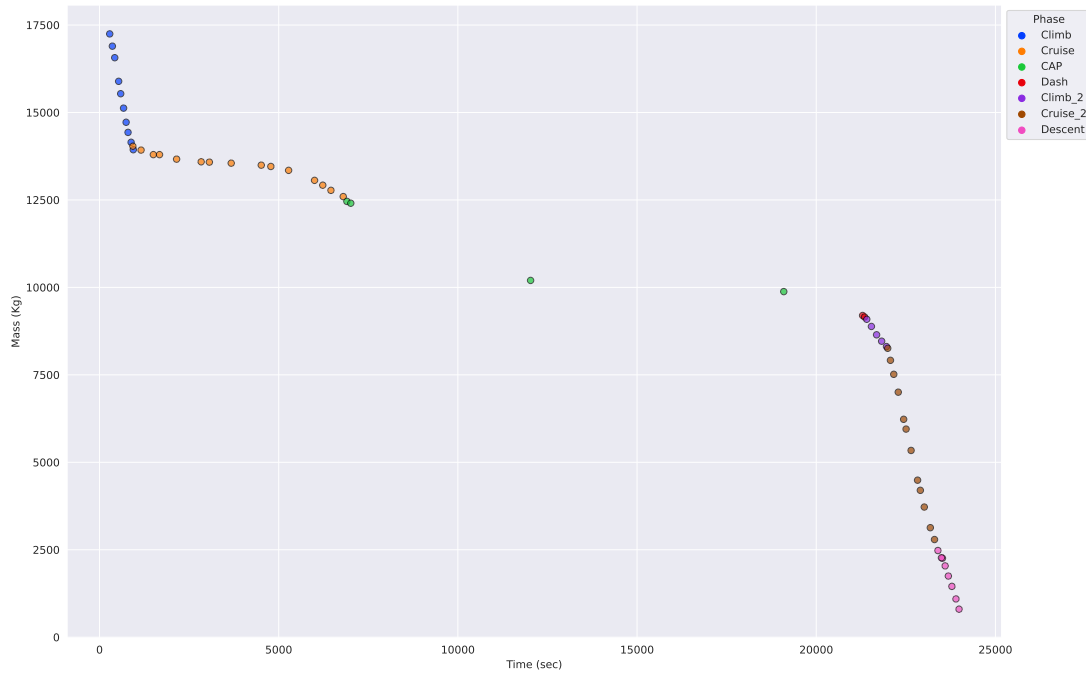


FIGURE 4.2: DCA Patrol: Mass over time

climb but remains relatively high to maintain altitude and speed. Increased negative fuel flow rate during descent1 may relate to thrust modulation for descent control as shown in Figure 4.7. Thrust varies; increases in cruise2 and descent2 segments are attributed to maneuvers and stability maintenance.

4.5.3 Escort Mission Analysis

The Escort segment stands out as the longest and most telling part of the mission, lasting from around 2,000 to 8,000 seconds as shown in Figure 4.8. Throughout this stretch, the aircraft's weight holds steady at roughly 14,000 kg. This consistency points to an efficient use of fuel, suggesting the aircraft is well-suited for extended loitering an essential trait for escort operations. After the Escort segment, there's a sharp drop in mass during the Climb2 phase, falling from 14,000 kg to about 11,500 kg between 8,500 and 9,500 seconds. This rapid decrease likely reflects a burst of fuel use for gaining altitude.

As shown in Figure 4.9 Climb 1 and Dash phases from 0 to approximately 2000 seconds, the drag force fluctuates, starting at higher values around 6-7 lbf

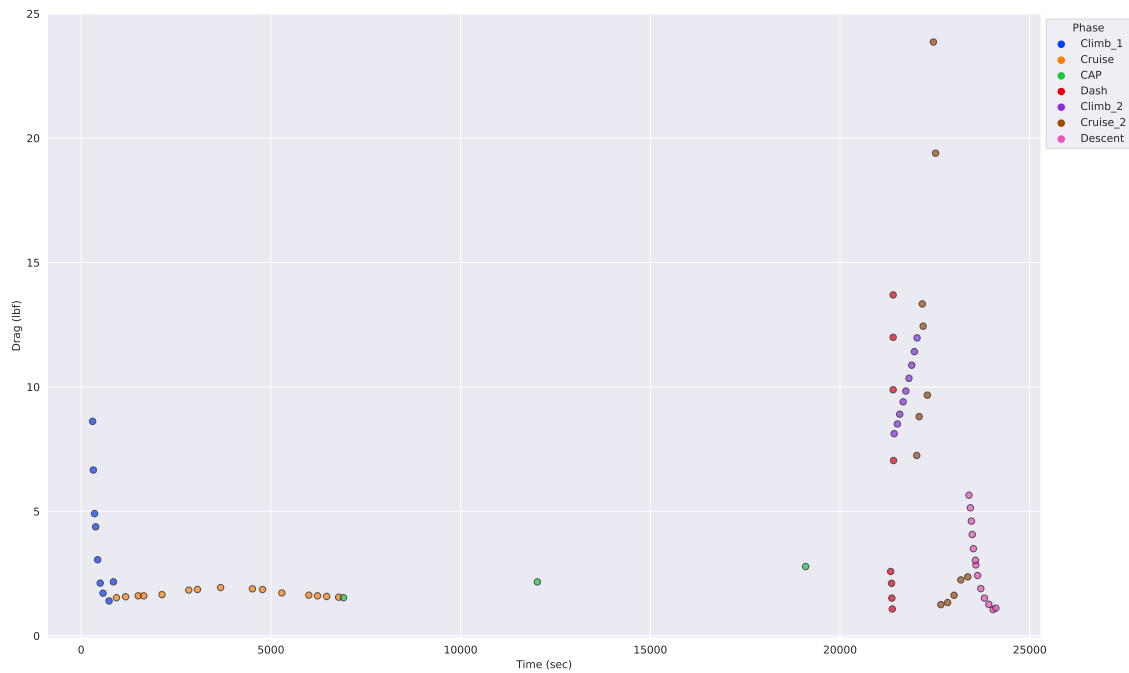


FIGURE 4.3: DCA Patrol: Drag over time

and then settling to lower levels approximately around 2 lbf. These fluctuations are expected during the dynamic nature of takeoff, initial climb, and acceleration. During escort phase is characterized by remarkably low and stable drag values, consistently hovering around 2 lbf in a duration from 2000 to 7500 seconds. This indicates that the aircraft is operating at an aerodynamically efficient condition, which is crucial for maximizing endurance during an escort mission.

In Climb 1 segment, approximately from 0 to 2000 seconds, the specific energy rate excess is initially high around 100 m/s and then decreases as the aircraft transitions out of the initial climb, stabilizing at lower values as shown in Figure 4.10. Then it show increase energy rate during Dash segment due to speed changes which increases. This reflects the initial energy expenditure for gaining altitude and speed. A dramatic increase in specific energy rate excess occurs during the Climb 2 and Cruise phases for approximately 9000 to 12000 seconds, reaching values well over 200 m/s. This significant rise indicates that the aircraft is undergoing a high-energy maneuver, such as a rapid climb to accelerate to a higher cruise speed.

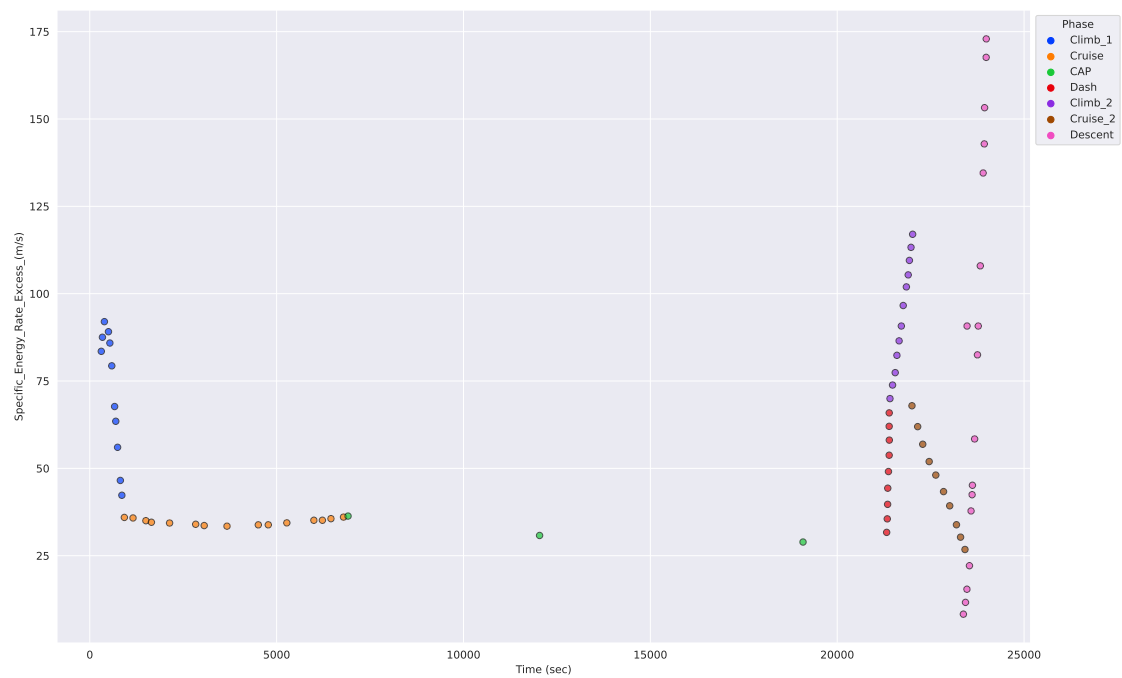


FIGURE 4.4: DCA Patrol: Specific Energy Rate Excess over time

4.6 Discussion of Results

The iterative sizing process using the AVIARY framework revealed several important insights into the optimal design and performance of the Homeland Defense Interceptor (HDI) aircraft. These results that shown in Table 4.1 directly support the research goals of identifying key design parameters and evaluating mission effectiveness.

To begin with, the optimization settled on a Gross Takeoff Weight (GTOW) of 36,066 lbm (16,329 kg). This figure represents a well-balanced compromise large enough to carry the required payload and fuel for extended missions, yet light enough to maintain the agility and responsiveness expected of an interceptor. The chosen GTOW places the HDI in the mid-size unmanned aerial vehicle category, aligning with its intended role as a capable yet efficient asset for national defense.

The study also confirmed several important performance and geometric characteristics. Notably, a wing area of 486.61 ft² (45.17 m²) was identified as ideal. This size offers the lift needed for both long-endurance patrols and rapid interception maneuvers. Combined with a thrust-to-weight ratio of approximately

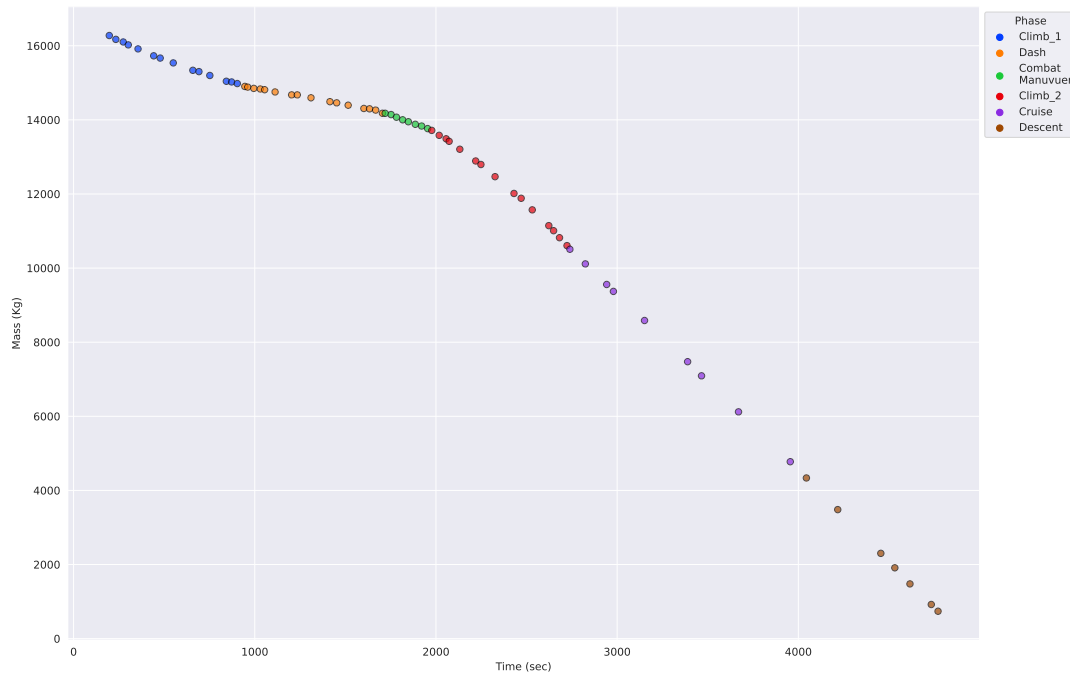


FIGURE 4.5: PDI: Mass over time

0.98, the aircraft demonstrates strong acceleration and climb performance key traits for quick-response missions.

The DCA Patrol mission profile emerged as the most influential factor in shaping the aircrafts overall design. The long endurance and loiter time required for this mission heavily influenced fuel capacity and aerodynamic efficiency.

With an optimized gross takeoff weight (GTOW) of around 36,066 lbm (16,359 Kg), the HDI falls into a distinct category. It is significantly lighter than larger fifth-generation stealth fighters like the F-22 Raptor, which has an empty weight of approximately 64,460 lbm (29,238.6 Kg) and an even higher GTOW. Compared to multirole fighters such as the MiG-29, with an empty weight of 24,251 lbs (11,000 Kg), the HDI also stands apart designed not for multirole versatility, but for focused interceptor performance. Its overall mass aligns more closely with aircraft like the Gripen JAS 39C, which has an empty weight near 15,000 lbs. However, the HDI's higher GTOW reflects the advantages of an unmanned design where it doesn't have a cockpit, pilot safety systems, and other human-related mass and its emphasis on extended endurance and payload capacity.

In relation to unmanned counterparts like the Bayraktar Kzlelma, which has

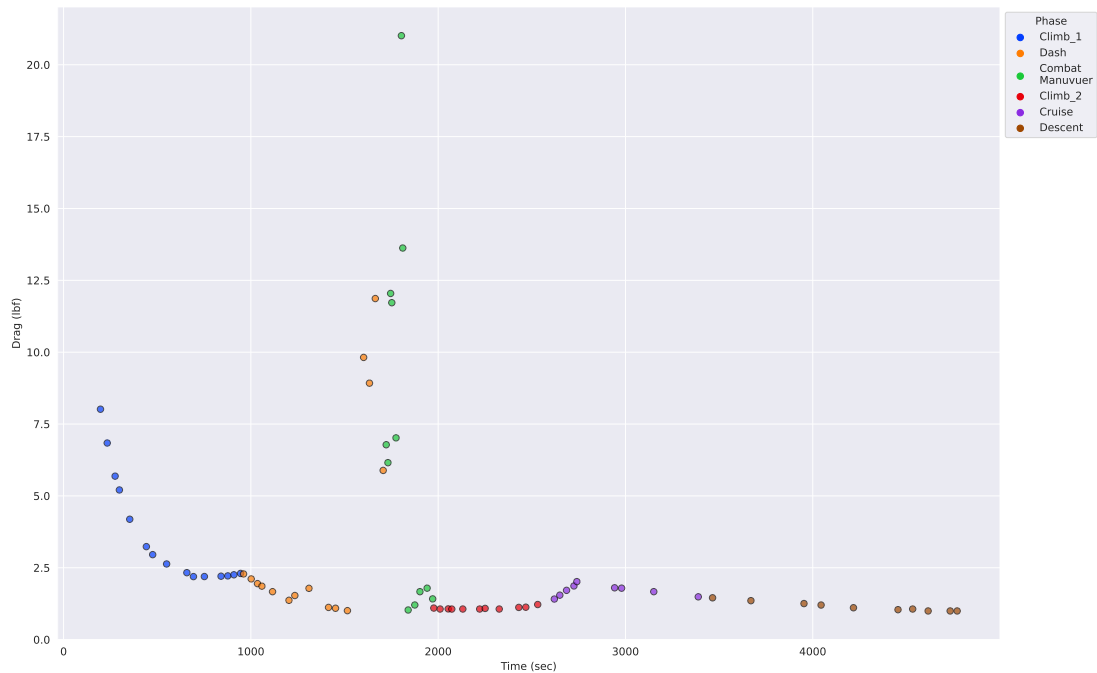


FIGURE 4.6: PDI: Drag over time plot

a GTOW around 13,000 lbm (5,987.4 Kg), the HDI is nearly double in size. This suggests a platform designed for more demanding missions: longer range, larger payloads, and faster response times. These characteristics support the HDIs intended role in defending wide territorial areas, rather than engaging in limited tactical strikes.

The HDIs thrust-to-weight ratio of 0.98 sits just below typical values for modern manned fighters, which often range from 1.0 to 1.2. While slightly lower, it remains within a range that ensures fast acceleration and effective climb rates both essential for interception tasks. The wing loading of 74.21 lb/ft² places the HDI in a moderate range lower than the MiG-29 (83 lb/ft²) and F-22 (77.2 lb/ft²), yet higher than the Gripen (58 lb/ft²). Its wing area of 486 ft² provides a practical compromise between efficient cruise capability (needed for patrol endurance) and the agility required for responsive interception, distinguishing it from fighter designs that prioritize close-in, high-G maneuverability.

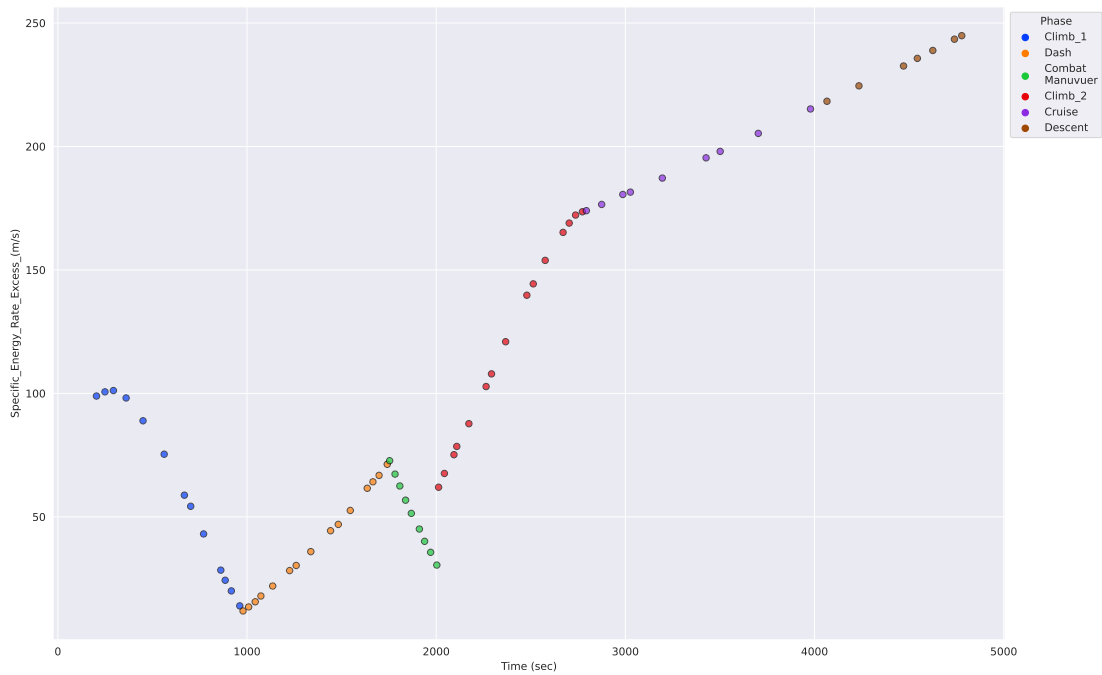


FIGURE 4.7: PDI: Specific Energy Rate Excess over time

4.6.1 Design Limitations and Challenges

Discussion on design constraints, such as:

- A key trade-off was between geometry and supersonic performance; the Mach 0.9 limit was chosen because the limitation on building the engine deck in AVIARY.
- Potential deviations from ideal parameters due to iterative assumptions.
- Balancing fuel requirements for high-speed dash and extended loiter was a significant challenge, influencing fuel capacity and wing sizing.

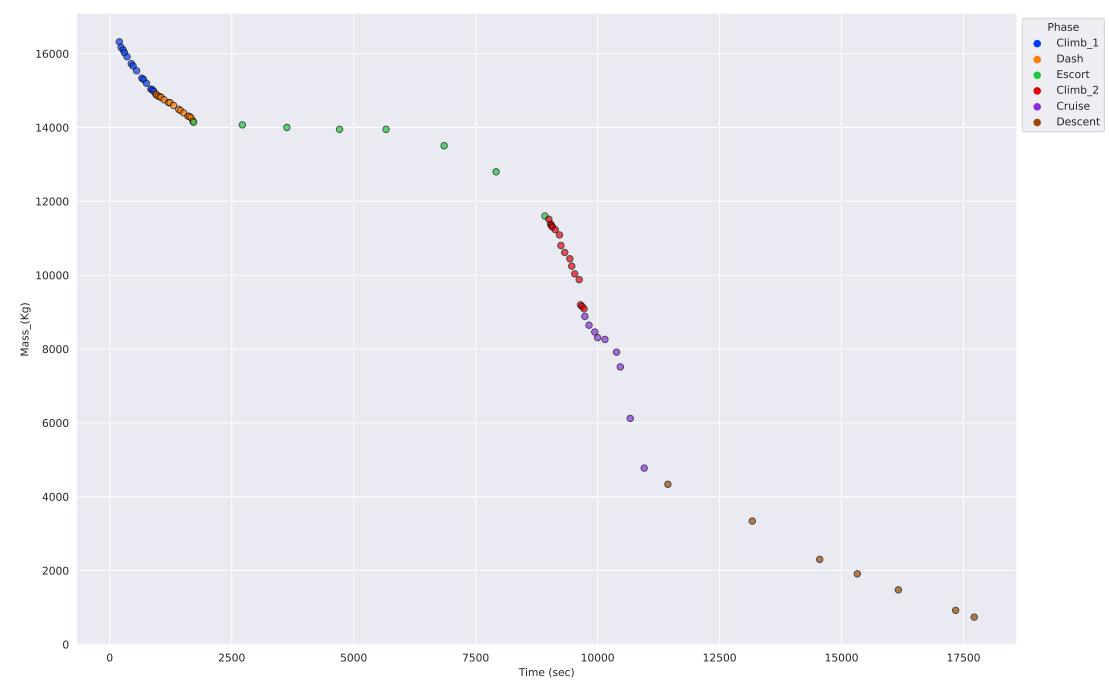


FIGURE 4.8: Escort: Mass over time

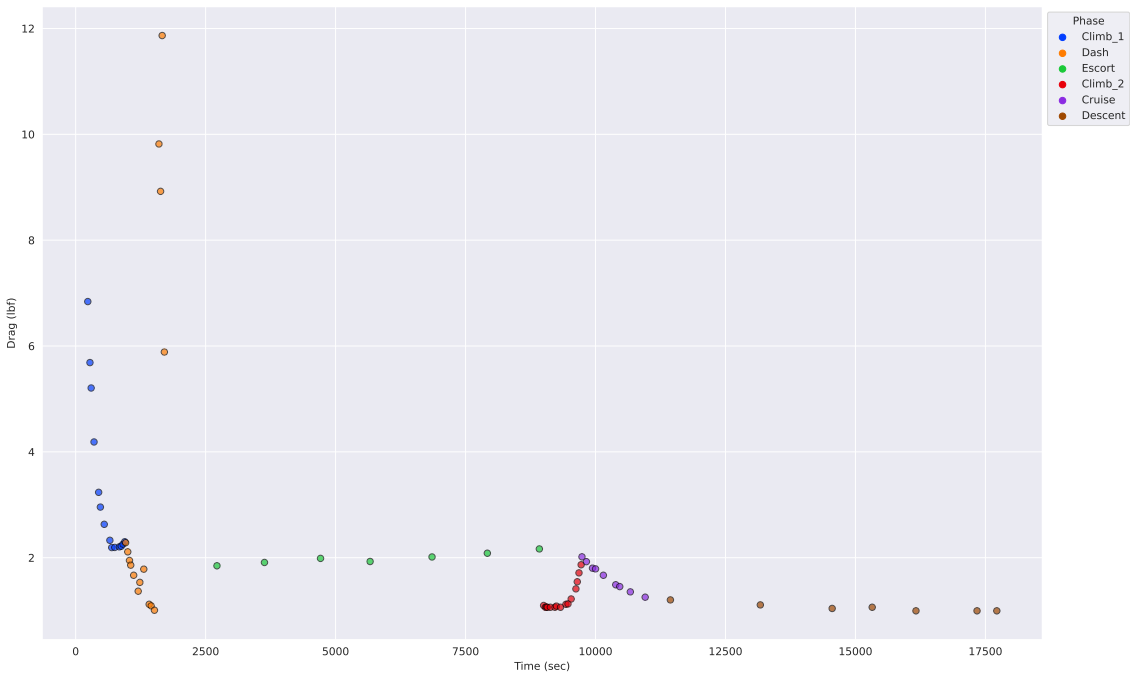


FIGURE 4.9: Escort: Drag over time

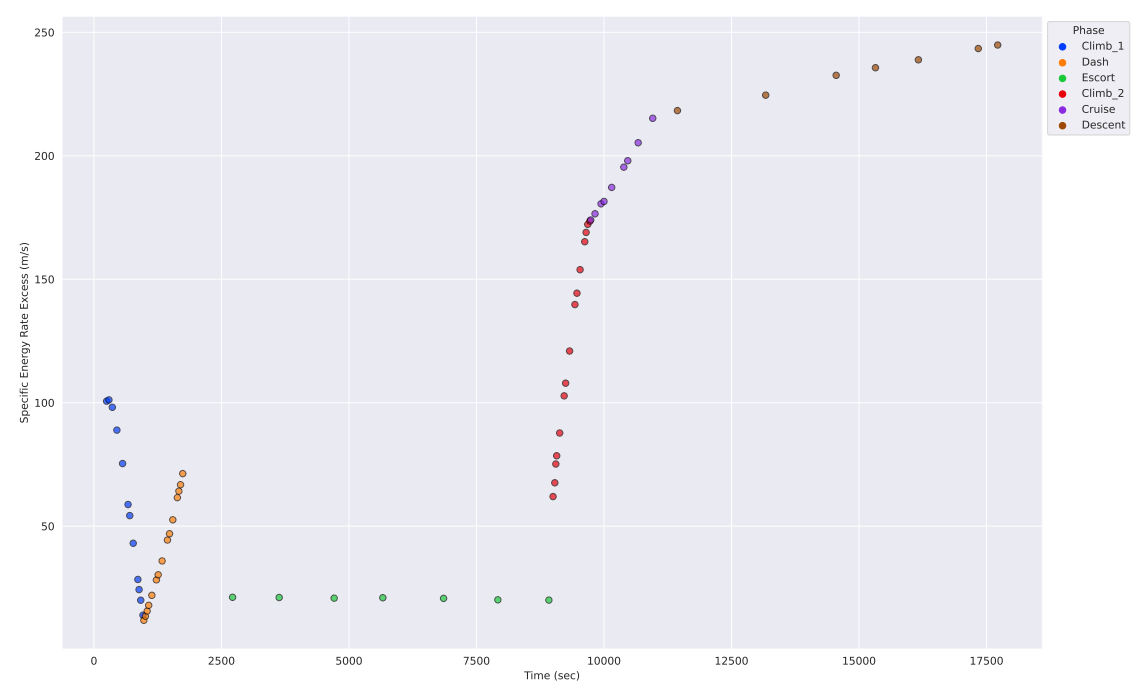


FIGURE 4.10: Escort: Energy Rate over time

CHAPTER 5

SUMMARY, CONCLUSION, RECOMMENDATION

5.1 Summary

This research set out to accomplish the preliminary sizing of an Homeland Defense Interceptor (HDI) aircraft, leveraging the powerful, open-source AVIARY framework. The study was driven by the growing demand for a new generation of interceptors aircraft capable of effectively countering advanced aerial threats.

To achieve this, AVIARY's integrated parametric environment, built upon OpenMDAO, was employed to conduct a detailed mission-specific sizing analysis. This analysis spanned three critical mission profiles outlined in the 2025 AIAA Undergraduate Design Team Request for Proposal (RFP): Defensive Counter-Air (DCA) Patrol, Point Defense Interception, and Intercept/Escort. It is important to note that due to the current capabilities of AVIARY, this design focused exclusively on subsonic flight regimes, thus excluding any supersonic aerodynamic effects from the analysis. From the comprehensive RFP requirements, the design was primarily driven by the intercept radius and the Defensive Counter-Air (DCA) Patrol mission's endurance capability. Initial design estimates were calibrated with robust benchmarking data drawn from well-established fighter aircraft, including the F-22 Raptor, Saab JAS 39C Gripen, MiG-29 Fulcrum, and Bayraktar Kzlelma. Through an iterative process involving simulation and constraint analysis within AVIARY, key parameters such as takeoff gross weight, fuel weight, wing area, thrust-to-weight ratio, and mission fuel fractions were meticulously determined. Notably, Raymers weight fraction estimation method, integrated within OpenMDAO, proved instrumental during the initial sizing phase.

A striking consistency in the HDI design's performance across all simulated mission profiles became evident, particularly in its impressive ability to fulfill

both loiter and dash requirements during the demanding DCA mission. Among the specific discoveries:

- An optimal Gross Take-Off Weight (GTOW) of 36,066 lbm (16,359 Kg) was pinpointed. This weight proved to be a sweet spot, effectively balancing the aircraft's payload capacity, range, and maneuverability.
- Crucial geometric parameters, including a wing area of 486 ft² (45.17 m²) and an Aspect Ratio of 3.98, designed to ensure ample lift for both patrol and interception duties.
- A total Thrust of 35,000 lbf (155.69 kN), resulting in a Thrust-to-Weight ratio of 0.98, ensuring potent acceleration and climb performance.
- A Wing Loading of 72.04 lb/ft² (351.73 kg/m²), supporting efficient flight across the mission profiles.
- HDI Design gross weight, thrust-to-weight ratio, wing loading, and range place it within the operational performance envelope of lightweight multirole fighters such as the Gripen JAS 39C and MiG-29 Fulcrum, while remaining aerodynamically efficient with a relatively high aspect ratio. The HDIs positioning in the Thrust-to-Weight vs Wing Loading plot validates its agility and responsiveness, which are essential for quick-intercept and defensive patrol missions.
- Delving into mission performance, the highest rate of mass loss was observed during the climb phase, a direct result of the high engine thrust demanded. Conversely, cruise segments demonstrated remarkably stable mass with minimal fuel consumption. The climb phase also showcased a vigorous energy gain rate, underlining the aircraft's potent thrust-to-weight ratio, while drag remained consistently low and steady during cruise, indicative of highly efficient aerodynamics.

This study marks a significant contribution to the field of preliminary aircraft design. It vividly demonstrates the practical application of AVIARY as a cutting-edge, open-source, and truly multidisciplinary tool for conceptual sizing. Furthermore, it offers a replicable and scalable methodology for sizing aircraft under demanding mission constraints, enabling designers to rapidly evaluate crucial trade offs concerning weight, range, thrust, and mission endurance.

5.2 Conclusion

In conclusion, this research successfully delivered a preliminary sizing model for a Homeland Defense Interceptor aircraft, thoughtfully developed using the AVIARY framework. This work effectively addresses the ambitious objectives set forth in the AIAA 2025 RFP. The study firmly establishes the feasibility of designing an unmanned interceptor fully capable of executing a diverse array of homeland defense missions, encompassing Defensive Counter-Air Patrol, Point Defense Interception, and Intercept/Escort as the result shown in Chapter 4 in Table 4.1. The iterative design process facilitated by AVIARY allowed for the precise determination of critical design parameters that align with the required performance boundaries. The consistent performance of the HDI design across various mission profiles, particularly its ability to meet demanding loiter and dash requirements, stands as strong validation for AVIARY's effectiveness as a rapid, multidisciplinary tool for conceptual aircraft design. It is important to reiterate that this design and analysis were conducted within the subsonic flight regime, primarily driven by the intercept radius and the DCA Patrol mission's endurance requirements, acknowledging the current limitations of the AVIARY tool in modeling supersonic aerodynamics. Ultimately, this effort provides a robust and practical methodological framework for future conceptual design endeavors, especially within the exciting domain of unmanned combat aircraft.

5.3 Recommendation

Building upon the insights gained from this preliminary sizing study, several avenues for future research and development emerge that could significantly enhance the HDI aircraft concept:

- **Supersonic Flight Regime Integration:**

A critical next step involves extending the design and analysis to include supersonic flight capabilities. This would necessitate exploring alternative or augmented multidisciplinary design optimization (MDO) frameworks capable of robustly modeling supersonic aerodynamics, propulsion integration for supersonic performance, and associated structural considerations.

- Comprehensive RFP Compliance:

While this study focused on key driving requirements, future work should aim to incorporate and satisfy all remaining RFP specifications, ensuring a more complete and compliant design solution. This includes a detailed analysis of all performance parameters, payload requirements, and operational constraints.

- Advanced Optimization and Higher-Fidelity Analysis:

The preliminary sizing could be further refined through more advanced MDO techniques. Incorporating higher-fidelity analysis tools, such as Computational Fluid Dynamics (CFD) for detailed aerodynamic analysis, Finite Element Analysis (FEA) for structural integrity, and more sophisticated propulsion system modeling, would provide greater precision in the design parameters.

- Trade-off Studies and Sensitivity Analysis:

Conducting extensive trade-off studies on various design variables (wing sweep, aspect ratio, engine cycle) and performing sensitivity analyses on key input parameters would provide a deeper understanding of design drivers and performance envelopes.

- Enhanced AVIARY Potential Analysis

Enhance the AVIARY aircraft model to support detailed static and dynamic stability analysis, including the integration of control surface sizing, moments of inertia estimation, and trim analysis across multiple flight regimes. Integrate aerodynamic databases (CFD or DATCOM) with AVIARY's framework to capture nonlinear aerodynamic effects more accurately, particularly for post-stall behavior or high-angle-of-attack scenarios.

These recommendations aim to guide subsequent design iterations toward a more refined, comprehensive, and ultimately deployable Homeland Defense Interceptor aircraft.

Appendices

APPENDIX A

AIRCRAFT MODEL FILE

TABLE A.1: Interceptor Aircraft Model Input CSV File

No.	Parameter	Value	Unit
1	aircraft:air-conditioning:mass-scaler	0.8	Unitless
2	aircraft:anti-icing:mass-scaler	0.2	Unitless
3	aircraft:apu:mass-scaler	0.5	Unitless
4	aircraft:avionics:mass-scaler	1.2	Unitless
5	aircraft:canard:area	0	ft ²
6	aircraft:canard:aspect-ratio	0	Unitless
7	aircraft:canard:thickness-to-chord	0	Unitless
8	aircraft:crew-and-payload:baggage-mass-per-passenger	0	lbm
9	aircraft:crew-and-payload:cargo-container-mass-scaler	0.5	Unitless
10	aircraft:crew-and-payload:flight-crew-mass-scaler	0	Unitless
11	aircraft:crew-and-payload:mass-per-passenger	300	lbm
12	aircraft:crew-and-payload:misc-cargo	0	lbm
13	aircraft:crew-and-payload:non-flight-crew-mass-scaler	0	Unitless
14	aircraft:crew-and-payload:num-business-class	0	Unitless
15	aircraft:crew-and-payload:num-first-class	0	Unitless
16	aircraft:crew-and-payload:num-flight-attendants	1	Unitless

TABLE A.2: Interceptor Aircraft Model Input CSV File

No.	Parameter	Value	Unit
17	aircraft:crew-and-payload:num-flight-crew	0	Unitless
18	aircraft:crew-and-payload:num-galley-crew	0	Unitless
19	aircraft:crew-and-payload:num-non-flight-crew	0	Unitless
20	aircraft:crew-and-payload:num-passengers	0	Unitless
21	aircraft:crew-and-payload:num-tourist-class	0	Unitless
22	aircraft:crew-and-payload:passenger-service-mass-scaler	0	Unitless
23	aircraft:crew-and-payload:wing-cargo	0	lbm
24	aircraft:crew-and-payload:total-payload-mass	802	lbm
25	aircraft:design:base-area	0	ft ²
26	aircraft:design:empty-mass	21,407	lbm
27	aircraft:design:empty-mass-margin-scaler	1.1	Unitless
28	aircraft:design:lift-dependent-drag-coeff-factor	0.03	Unitless
29	aircraft:design:touchdown-mass	25,000	lbm
30	aircraft:design:reserve-fuel-additional	1,102.3	lbm
31	aircraft:design:subsonic-drag-coeff-factor	0.015	Unitless
32	aircraft:design:supersonic-drag-coeff-factor	1.2	Unitless

TABLE A.3: Interceptor Aircraft Model Input CSV File

No.	Parameter	Value	Unit
33	aircraft:design:use-alt-mass	True	Unitless
34	aircraft:design:zero-lift-drag-coeff-factor	0.012	Unitless
35	aircraft:electrical:mass-scaler	0.03	Unitless
36	aircraft:engine:additional-mass-fraction	0.05	Unitless
37	aircraft:engine:constant-fuel-consumption	0.9	lbm/h
38	aircraft:engine:data-file	turbofan-28k.deck	Unitless
39	aircraft:engine:flight-idle-thrust-fraction	0.1	Unitless
40	aircraft:engine:flight-idle-max-fraction	0.2	Unitless
41	aircraft:engine:flight-idle-min-fraction	0.05	Unitless
42	aircraft:engine:fuel-flow-scaler-constant-term	1	Unitless
43	aircraft:engine:fuel-flow-scaler-linear-term	1	Unitless
44	aircraft:engine:generate-flight-idle	True	Unitless
45	aircraft:engine:geopotential-alt	False	Unitless
46	aircraft:engine:ignore-negative-thrust	True	Unitless
47	aircraft:engine:interpolation-method	slinear	Unitless
48	aircraft:engine:mass-scaler	1	Unitless

TABLE A.4: Interceptor Aircraft Model Input CSV File

No.	Parameter	Value	Unit
49	aircraft:engine:mass	5,000	lbm
50	aircraft:engine:num-engines	2	Unitless
51	aircraft:engine:num-fuselage-engines	2	Unitless
52	aircraft:engine:num-wing-engines	0	Unitless
53	aircraft:engine:reference-mass	5,000	lbm
54	aircraft:engine:reference-sls-thrust	18,000	lbf
55	aircraft:engine:scale-mass	True	Unitless
56	aircraft:engine:scale-performance	True	Unitless
57	aircraft:engine:scaled-sls-thrust	18,000	lbf
58	aircraft:engine:subsonic-fuel-flow-scaler	0.9	Unitless
59	aircraft:engine:supersonic-fuel-flow-scaler	1.2	Unitless
60	aircraft:engine:thrust-reversers-mass-scaler	0	Unitless
61	aircraft:engine:wing-locations	[0.0]	Unitless
62	aircraft:fins:area	58.6	ft ²
63	aircraft:fins:mass-scaler	1.2	Unitless
64	aircraft:fins:mass	661	lbm

TABLE A.5: Interceptor Aircraft Model Input CSV File

No.	Parameter	Value	Unit
65	aircraft:fins:num-fins	2	Unitless
66	aircraft:fins:taper-ratio	0.5	Unitless
67	aircraft:fuel:auxiliary-fuel-capacity	0	lbm
68	aircraft:fuel:density-ratio	0.8	Unitless
69	aircraft:fuel:fuel-system-mass-scaler	1	Unitless
70	aircraft:fuel:fuselage-fuel-capacity	3,000	lbm
71	aircraft:fuel:num-tanks	5	Unitless
72	aircraft:fuel:total-capacity	15,000	lbm
73	aircraft:fuel:unusable-fuel-mass-scaler	0.02	Unitless
74	aircraft:furnishings:mass-scaler	0	Unitless
75	aircraft:fuselage:length	50	ft
76	aircraft:fuselage:mass-scaler	1	Unitless
77	aircraft:fuselage:max-height	8.2	ft
78	aircraft:fuselage:max-width	5.2	ft
79	aircraft:fuselage:military-cargo-floor	False	Unitless
80	aircraft:fuselage:num-fuselages	1	Unitless

TABLE A.6: Interceptor Aircraft Model Input CSV File

No.	Parameter	Value	Unit
81	aircraft:fuselage:passenger-compartment-length	0	ft
82	aircraft:fuselage:planform-area	200	ft ²
83	aircraft:fuselage:wetted-area-scaler	1	Unitless
84	aircraft:fuselage:wetted-area	753	ft ²
85	aircraft:horizontal-tail:area	154.73	ft ²
86	aircraft:horizontal-tail:aspect-ratio	4	Unitless
87	aircraft:horizontal-tail:mass-scaler	1	Unitless
88	aircraft:horizontal-tail:taper-ratio	0.4	lbm
89	aircraft:horizontal-tail:thickness-to-chord	0.1	Unitless
90	aircraft:horizontal-tail:vertical-tail-fraction	0.3	Unitless
91	aircraft:horizontal-tail:wetted-area-scaler	1	ft
92	aircraft:horizontal-tail:wetted-area	172	ft ²
93	aircraft:hydraulics:mass-scaler	1	ft
94	aircraft:hydraulics:system-pressure	720,000	lbf/ft ²
95	aircraft:instruments:mass-scaler	1	Unitless
96	aircraft:landing-gear:carrier-based	False	Unitless

TABLE A.7: Interceptor Aircraft Model Input CSV File

No.	Parameter	Value	Unit
97	aircraft:landing-gear:main-gear-mass-scaler	1	Unitless
98	aircraft:landing-gear:main-gear-oleo-length	23.6	inch
99	aircraft:landing-gear:nose-gear-mass-scaler	1	Unitless
100	aircraft:landing-gear:nose-gear-oleo-length	15.75	inch
101	aircraft:nacelle:avg-diameter	3,3	ft
102	aircraft:nacelle:avg-length	16.5	ft
103	aircraft:nacelle:count-factor	1	Unitless
104	aircraft:nacelle:mass-scaler	1	Unitless
105	aircraft:nacelle:wetted-area-scaler	1	Unitless
106	aircraft:paint:mass-per-unit-area	14.23	/lbm/ft ²
107	aircraft:propulsion:engine-oil-mass-scaler	1	Unitless
108	aircraft:propulsion:misc-mass-scaler	1	Unitless
109	aircraft:vertical-tail:area	53.98	ft ²
110	aircraft:vertical-tail:aspect-ratio	1.5	Unitless
111	aircraft:vertical-tail:mass-scaler	1	Unitless
112	aircraft:vertical-tail:num-tails	2	Unitless

TABLE A.8: Interceptor Aircraft Model Input CSV File

No.	Parameter	Value	Unit
113	aircraft:vertical-tail:taper-ratio	0.5	Unitless
114	aircraft:vertical-tail:thickness-to-chord	0.1	Unitless
115	aircraft:vertical-tail:wetted-area-scaler	1.1	Unitless
116	aircraft:vertical-tail:wetted-area	97.6	ft ²
117	aircraft:wing:aeroelastic-tailoring-factor	1	Unitless
118	aircraft:wing:airfoil-technology	2	Unitless
119	aircraft:wing:area	445.03	ft ²
120	aircraft:wing:aspect-ratio	3.98	Unitless
121	aircraft:wing:bending-factor	1	Unitless
122	aircraft:wing:bending-mass-scaler	1	Unitless
123	aircraft:wing:chord-per-semispan	$4 * 0.23 * 0.084$	Unitless
124	aircraft:wing:composite-fraction	0.5	Unitless
125	aircraft:wing:control-surface-area	107.6	ft ²
126	aircraft:wing:control-surface-area-ratio	0.2	Unitless
127	aircraft:wing:glove-and-bat	0	ft ²
128	aircraft:wing:input-station-dist	$0 * 0.2759 * 0.9367$	Unitless

TABLE A.9: Interceptor Aircraft Model Input CSV File

No.	Parameter	Value	Unit
129	aircraft:wing:load-distribution-control	0.8	Unitless
130	aircraft:wing:load-fraction	0.5	Unitless
131	aircraft:wing:load-path-sweep-dist	$1.5 * 22$	deg
132	aircraft:wing:mass-scaler	1	Unitless
133	aircraft:wing:max-camber-at-70-semispan	0.02	Unitless
134	aircraft:wing:misc-mass-scaler	1	Unitless
135	aircraft:wing:num-integration-stations	5	Unitless
136	aircraft:wing:shear-control-mass-scaler	1	Unitless
137	aircraft:wing:span-efficiency-reduction	True	Unitless
138	aircraft:wing:span	44	ft
139	aircraft:wing:strut-bracing-factor	0	Unitless
140	aircraft:wing:surface-ctrl-mass-scaler	1	Unitless
141	aircraft:wing:sweep	50	deg
142	aircraft:wing:taper-ratio	0.4	Unitless
143	aircraft:wing:thickness-to-chord-dist	$0.1 * 0.115 * 0.104$	Unitless
144	aircraft:wing:thickness-to-chord	0.08	Unitless

TABLE A.10: Interceptor Aircraft Model Input CSV File

No.	Parameter	Value	Unit
145	aircraft:wing:ultimate-load-factor	9	Unitless
146	aircraft:wing:var-sweep-mass-penalty	0	Unitless
147	aircraft:wing:wetted-area-scaler	1	Unitless
148	aircraft:wing:wetted-area	960	ft ²
149	mission:constraints:max-mach	1.6	Unitless
150	mission:design:cruise-altitude	35,000	ft
151	mission:design:gross-mass	36,773	lbm
152	mission:design:range	800	Nm
153	mission:cruise:range	500	Nm
154	mission:design:thrust-takeoff-per-eng	36,000	lbf
155	mission:landing:lift-coefficient-max	2.2	Unitless
156	mission:summary:cruise-mach	0.9	Unitless
157	mission:summary:fuel-flow-scaler	1	Unitless
158	mission:takeoff:fuel-simple	1,102	lbm
159	mission:takeoff:lift-coefficient-max	2	Unitless
160	mission:takeoff:lift-over-drag	10	Unitless
161	settings:equations-of-motion	Height-Energy	Unitless
162	settings:mass-method	FLOPS	Unitless

APPENDIX B

PYTHON CODES

B.1 Level 2 Example

```
1 from copy import deepcopy
2
3 import aviary.api as av
4
5 # inputs that run_aviary() requires
6 aircraft_data = 'models/test_aircraft/aircraft_for_bench_GwGm.csv'
7 optimizer = 'IPOPT'
8 analysis_scheme = av.AnalysisScheme.COLLOCATION
9 objective_type = None
10 record_filename = 'aviary_history.db'
11 restart_filename = None
12 max_iter = 0
13 phase_info = deepcopy(av.default_2DOF_phase_info)
14
15 # Build problem
16 prob = av.AviaryProblem(analysis_scheme)
17
18 # Load aircraft and options data from user
19 # Allow for user overrides here
20 prob.load_inputs(aircraft_data, phase_info)
21
22 # Preprocess inputs
23 prob.check_and_preprocess_inputs()
24
25 # adds a pre-mission group (propulsion, geometry, aerodynamics,
    and mass)
26 prob.add_pre_mission_systems()
27
```

```
28 # adds a sequence of core mission phases.
29 prob.add_phases()
30
31 # adds a landing phase
32 prob.add_post_mission_systems()
33
34 # Link phases and variables
35 prob.link_phases()
36
37 # adds an optimizer to the driver
38 prob.add_driver(optimizer, max_iter=max_iter)
39
40 # adds relevant design variables
41 prob.add_design_variables()
42
43 # Load optimization problem formulation
44 # Detail which variables the optimizer can control
45 prob.add_objective(objective_type=objective_type)
46
47 # setup the problem
48 prob.setup()
49
50 # set initial guesses of states and controls variables
51 prob.set_initial_guesses()
52
53 # run the problem we just set up
54 prob.run_aviary_problem(record_filename, restart_filename=
    restart_filename)
```

B.2 Default Phase Info: FlOPS

```
1 from aviary.subsystems.propulsion.propulsion_builder import
    CorePropulsionBuilder
2 from aviary.subsystems.geometry.geometry_builder import
    CoreGeometryBuilder
3 from aviary.subsystems.mass.mass_builder import CoreMassBuilder
4 from aviary.subsystems.aerodynamics.aerodynamics_builder import
    CoreAerodynamicsBuilder
5 from aviary.variable_info.variable_meta_data import _MetaData as
    BaseMetaData
```

```
6 from aviary.variable_info.variables import Dynamic, Mission
7 from aviary.variable_info.enums import LegacyCode
8
9 FLOPS = LegacyCode.FLOPS
10
11 prop = CorePropulsionBuilder('core_propulsion', BaseMetaData)
12 mass = CoreMassBuilder('core_mass', BaseMetaData, FLOPS)
13 aero = CoreAerodynamicsBuilder('core_aerodynamics', BaseMetaData,
14                                FLOPS)
15
16 geom = CoreGeometryBuilder('core_geometry', BaseMetaData, FLOPS)
17
18 default_premission_subsystems = [prop, geom, mass, aero]
19 default_mission_subsystems = [aero, prop]
20
21 phase_info = {
22     "pre_mission": {"include_takeoff": False, "optimize_mass":
23                     True},
24     "climb": {
25         "subsystem_options": {"core_aerodynamics": {"method": "
26                             computed"}},
27         "user_options": {
28             "optimize_mach": False,
29             "optimize_altitude": False,
30             "num_segments": 5,
31             "order": 3,
32             "solve_for_distance": False,
33             "initial_mach": (0.2, "unitless"),
34             "final_mach": (0.72, "unitless"),
35             "mach_bounds": ((0.18, 0.74), "unitless"),
36             "initial_altitude": (0.0, "ft"),
37             "final_altitude": (32000.0, "ft"),
38             "altitude_bounds": ((0.0, 34000.0), "ft"),
39             "throttle_enforcement": "path_constraint",
40             "fix_initial": True,
41             "constrain_final": False,
42             "fix_duration": False,
43             "initial_bounds": ((0.0, 0.0), "min"),
44             "duration_bounds": ((64.0, 192.0), "min"),
45             "add_initial_mass_constraint": False,
```

```
43     },
44 },
45 "cruise": {
46     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
47     "user_options": {
48         "optimize_mach": False,
49         "optimize_altitude": False,
50         "num_segments": 5,
51         "order": 3,
52         "solve_for_distance": False,
53         "initial_mach": (0.72, "unitless"),
54         "final_mach": (0.72, "unitless"),
55         "mach_bounds": ((0.7, 0.74), "unitless"),
56         "initial_altitude": (32000.0, "ft"),
57         "final_altitude": (34000.0, "ft"),
58         "altitude_bounds": ((23000.0, 38000.0), "ft"),
59         "throttle_enforcement": "boundary_constraint",
60         "fix_initial": False,
61         "constrain_final": False,
62         "fix_duration": False,
63         "initial_bounds": ((64.0, 192.0), "min"),
64         "duration_bounds": ((56.5, 169.5), "min"),
65     },
66 },
67 "descent": {
68     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
69     "user_options": {
70         "optimize_mach": False,
71         "optimize_altitude": False,
72         "num_segments": 5,
73         "order": 3,
74         "solve_for_distance": False,
75         "initial_mach": (0.72, "unitless"),
76         "final_mach": (0.36, "unitless"),
77         "mach_bounds": ((0.34, 0.74), "unitless"),
78         "initial_altitude": (34000.0, "ft"),
79         "final_altitude": (500.0, "ft"),
80         "altitude_bounds": ((0.0, 38000.0), "ft"),
```

```
81         "throttle_enforcement": "path_constraint",
82         "fix_initial": False,
83         "constrain_final": True,
84         "fix_duration": False,
85         "initial_bounds": ((120.5, 361.5), "min"),
86         "duration_bounds": ((29.0, 87.0), "min"),
87     },
88 },
89 "post_mission": {
90     "include_landing": False,
91     "constrain_range": True,
92     "target_range": (1906., "nmi"),
93 },
94 }
95
96
97 def phase_info_parameterization(phase_info, post_mission_info,
98     aviary_inputs):
99     """
100     Modify the values in the phase_info dictionary to accommodate
101     different values
102     for the following mission design inputs: cruise altitude,
103     cruise Mach number,
104     cruise range, design gross mass.
105
106     Parameters
107     -----
108     phase_info : dict
109         Dictionary of phase settings for a mission profile
110     aviary_inputs : <AviaryValues>
111         Object containing values and units for all aviary inputs
112         and options
113
114     Returns
115     -----
116     dict
117         Modified phase_info that has been changed to match the new
118         mission
119         parameters
120     """
```

```
116
117     alt_cruise = aviary_inputs.get_val(Mission.Design.
CRUISE_ALTITUDE, units='ft')
118     mach_cruise = aviary_inputs.get_val(Mission.Summary.
CRUISE_MACH)
119
120     # Range
121     old_range_cruise, range_units = post_mission_info['
target_range']
122     range_cruise = aviary_inputs.get_val(Mission.Design.RANGE,
units=range_units)
123     if range_cruise != old_range_cruise:
124         new_val = post_mission_info['target_range'][0] *
range_cruise / old_range_cruise
125         post_mission_info['target_range'] = (new_val, range_units)
126
127     # Altitude
128     old_alt_cruise = 32000.
129     if alt_cruise != old_alt_cruise:
130         phase_info['climb']['user_options']['final_altitude'] = (
alt_cruise, 'ft')
131         phase_info['cruise']['user_options']['initial_altitude'] =
(alt_cruise, 'ft')
132         phase_info['cruise']['user_options']['final_altitude'] = (
alt_cruise, 'ft')
133         phase_info['descent']['user_options']['initial_altitude']
= (alt_cruise, 'ft')
134
135     # Mach
136     old_mach_cruise = 0.72
137     if mach_cruise != old_mach_cruise:
138         phase_info['climb']['user_options']['final_mach'] = (
mach_cruise, "unitless")
139         phase_info['cruise']['user_options']['initial_mach'] = (
mach_cruise, "unitless")
140         phase_info['cruise']['user_options']['final_mach'] = (
mach_cruise, "unitless")
141         phase_info['descent']['user_options']['initial_mach'] = (
mach_cruise, "unitless")
142
```

```
143     return phase_info, post_mission_info
```

B.3 Default Phase Info: GASP

```
1 from aviary.variable_info.enums import SpeedType
2 from aviary.variable_info.variables import Mission
3
4 # defaults for 2DOF based phases
5 mission_distance = 3675
6
7 phase_info = {
8     'groundroll': {
9         'user_options': {
10             'num_segments': 1,
11             'order': 3,
12             'connect_initial_mass': False,
13             'fix_initial': True,
14             'fix_initial_mass': False,
15             'duration_ref': (50.0, 's'),
16             'duration_bounds': ((1.0, 100.0), 's'),
17             'velocity_lower': (0, 'kn'),
18             'velocity_upper': (1000, 'kn'),
19             'velocity_ref': (150, 'kn'),
20             'mass_lower': (0, 'lbm'),
21             'mass_upper': (None, 'lbm'),
22             'mass_ref': (150_000, 'lbm'),
23             'mass_defect_ref': (150_000, 'lbm'),
24             'distance_lower': (0, 'ft'),
25             'distance_upper': (10.0e3, 'ft'),
26             'distance_ref': (3000, 'ft'),
27             'distance_defect_ref': (3000, 'ft'),
28         },
29         'initial_guesses': {
30             'time': ([0.0, 40.0], 's'),
31             'velocity': ([0.066, 143.1], 'kn'),
32             'distance': ([0.0, 1000.0], 'ft'),
33             'throttle': ([0.956, 0.956], 'unitless'),
34         },
35     },
36     'rotation': {
```

```
37     'user_options': {
38         'num_segments': 1,
39         'order': 3,
40         'fix_initial': False,
41         'duration_bounds': ((1, 100), 's'),
42         'duration_ref': (50.0, 's'),
43         'velocity_lower': (0, 'kn'),
44         'velocity_upper': (1000, 'kn'),
45         'velocity_ref': (100, 'kn'),
46         'velocity_ref0': (0, 'kn'),
47         'mass_lower': (0, 'lbm'),
48         'mass_upper': (None, 'lbm'),
49         'mass_ref': (150_000, 'lbm'),
50         'mass_defect_ref': (150_000, 'lbm'),
51         'distance_lower': (0, 'ft'),
52         'distance_upper': (10_000, 'ft'),
53         'distance_ref': (5000, 'ft'),
54         'distance_defect_ref': (5000, 'ft'),
55         'angle_lower': (0.0, 'rad'),
56         'angle_upper': (5.0, 'rad'),
57         'angle_ref': (5.0, 'rad'),
58         'angle_defect_ref': (5.0, 'rad'),
59         'normal_ref': (10000, 'lbf'),
60     },
61     'initial_guesses': {
62         'time': ([40.0, 5.0], 's'),
63         'angle_of_attack': ([0.0, 2.5], 'deg'),
64         'velocity': ([143, 150.0], 'kn'),
65         'distance': ([3680.37217765, 4000], 'ft'),
66         'throttle': ([0.956, 0.956], 'unitless'),
67     },
68 },
69 'ascent': {
70     'user_options': {
71         'num_segments': 4,
72         'order': 3,
73         'fix_initial': False,
74         'velocity_lower': (0, 'kn'),
75         'velocity_upper': (700, 'kn'),
76         'velocity_ref': (200, 'kn'),
```

```
77         'velocity_ref0': (0, 'kn'),
78         'mass_lower': (0, 'lbm'),
79         'mass_upper': (None, 'lbm'),
80         'mass_ref': (150_000, 'lbm'),
81         'mass_defect_ref': (150_000, 'lbm'),
82         'distance_lower': (0, 'ft'),
83         'distance_upper': (15_000, 'ft'),
84         'distance_ref': (1e4, 'ft'),
85         'distance_defect_ref': (1e4, 'ft'),
86         'alt_lower': (0, 'ft'),
87         'alt_upper': (700, 'ft'),
88         'alt_ref': (1000, 'ft'),
89         'alt_defect_ref': (1000, 'ft'),
90         'final_altitude': (500, 'ft'),
91         'alt_constraint_ref': (500, 'ft'),
92         'angle_lower': (-10, 'rad'),
93         'angle_upper': (20, 'rad'),
94         'angle_ref': (57.2958, 'deg'),
95         'angle_defect_ref': (57.2958, 'deg'),
96         'pitch_constraint_lower': (0.0, 'deg'),
97         'pitch_constraint_upper': (15.0, 'deg'),
98         'pitch_constraint_ref': (1.0, 'deg'),
99     },
100     'initial_guesses': {
101         'time': ([45.0, 25.0], 's'),
102         'flight_path_angle': ([0.0, 8.0], 'deg'),
103         'angle_of_attack': ([2.5, 1.5], 'deg'),
104         'velocity': ([150.0, 185.0], 'kn'),
105         'distance': ([4.0e3, 10.0e3], 'ft'),
106         'altitude': ([0.0, 500.0], 'ft'),
107         'tau_gear': (0.2, 'unitless'),
108         'tau_flaps': (0.9, 'unitless'),
109         'throttle': ([0.956, 0.956], 'unitless'),
110     },
111 },
112 'accel': {
113     'user_options': {
114         'num_segments': 1,
115         'order': 3,
116         'fix_initial': False,
```

```
117         'alt': (500, 'ft'),
118         'EAS_constraint_eq': (250, 'kn'),
119         'duration_bounds': ((1, 200), 's'),
120         'duration_ref': (1000, 's'),
121         'velocity_lower': (150, 'kn'),
122         'velocity_upper': (270, 'kn'),
123         'velocity_ref': (250, 'kn'),
124         'velocity_ref0': (150, 'kn'),
125         'mass_lower': (0, 'lbm'),
126         'mass_upper': (None, 'lbm'),
127         'mass_ref': (150_000, 'lbm'),
128         'mass_defect_ref': (150_000, 'lbm'),
129         'distance_lower': (0, 'NM'),
130         'distance_upper': (150, 'NM'),
131         'distance_ref': (5, 'NM'),
132         'distance_defect_ref': (5, 'NM'),
133     },
134     'initial_guesses': {
135         'time': ([70.0, 13.0], 's'),
136         'velocity': ([185.0, 250.0], 'kn'),
137         'distance': ([10.0e3, 20.0e3], 'ft'),
138         'throttle': ([0.956, 0.956], 'unitless'),
139     },
140 },
141 'climb1': {
142     'user_options': {
143         'num_segments': 1,
144         'order': 3,
145         'fix_initial': False,
146         'EAS_target': (250, 'kn'),
147         'mach_cruise': 0.8,
148         'target_mach': False,
149         'final_altitude': (10.0e3, 'ft'),
150         'duration_bounds': ((30, 300), 's'),
151         'duration_ref': (1000, 's'),
152         'alt_lower': (400, 'ft'),
153         'alt_upper': (11_000, 'ft'),
154         'alt_ref': (10.0e3, 'ft'),
155         'mass_lower': (0, 'lbm'),
156         'mass_upper': (None, 'lbm'),
```

```
157         'mass_ref': (150_000, 'lbm'),
158         'mass_defect_ref': (150_000, 'lbm'),
159         'distance_lower': (0, 'NM'),
160         'distance_upper': (500, 'NM'),
161         'distance_ref': (10, 'NM'),
162         'distance_ref0': (0, 'NM'),
163     },
164     'initial_guesses': {
165         'time': ([1.0, 2.0], 'min'),
166         'distance': ([20.0e3, 100.0e3], 'ft'),
167         'altitude': ([500.0, 10.0e3], 'ft'),
168         'throttle': ([0.956, 0.956], 'unitless'),
169     },
170 },
171 'climb2': {
172     'user_options': {
173         'num_segments': 3,
174         'order': 3,
175         'fix_initial': False,
176         'EAS_target': (270, 'kn'),
177         'mach_cruise': 0.8,
178         'target_mach': True,
179         'final_altitude': (37.5e3, 'ft'),
180         'required_available_climb_rate': (0.1, 'ft/min'),
181         'duration_bounds': ((200, 17_000), 's'),
182         'duration_ref': (5000, 's'),
183         'alt_lower': (9000, 'ft'),
184         'alt_upper': (40000, 'ft'),
185         'alt_ref': (30000, 'ft'),
186         'alt_ref0': (0, 'ft'),
187         'mass_lower': (0, 'lbm'),
188         'mass_upper': (None, 'lbm'),
189         'mass_ref': (150_000, 'lbm'),
190         'mass_defect_ref': (150_000, 'lbm'),
191         'distance_lower': (10, 'NM'),
192         'distance_upper': (1000, 'NM'),
193         'distance_ref': (500, 'NM'),
194         'distance_ref0': (0, 'NM'),
195         'distance_defect_ref': (500, 'NM'),
196     },
```

```
197         'initial_guesses': {
198             'time': ([216.0, 1300.0], 's'),
199             'distance': ([100.0e3, 200.0e3], 'ft'),
200             'altitude': ([10.0e3, 37.5e3], 'ft'),
201             'throttle': ([0.956, 0.956], 'unitless'),
202         },
203     },
204     'cruise': {
205         'user_options': {
206             'alt_cruise': (37.5e3, 'ft'),
207             'mach_cruise': 0.8,
208         },
209         'initial_guesses': {
210             # [Initial mass, delta mass] for special cruise phase.
211             'mass': ([171481.0, -35000], 'lbm'),
212             'initial_distance': (200.0e3, 'ft'),
213             'initial_time': (1516.0, 's'),
214             'altitude': (37.5e3, 'ft'),
215             'mach': (0.8, 'unitless'),
216         },
217     },
218     'desc1': {
219         'user_options': {
220             'num_segments': 3,
221             'order': 3,
222             'fix_initial': False,
223             'input_initial': False,
224             'EAS_limit': (350, 'kn'),
225             'mach_cruise': 0.8,
226             'input_speed_type': SpeedType.MACH,
227             'final_altitude': (10.0e3, 'ft'),
228             'duration_bounds': ((300.0, 900.0), 's'),
229             'duration_ref': (1000, 's'),
230             'alt_lower': (1000, 'ft'),
231             'alt_upper': (40_000, 'ft'),
232             'alt_ref': (30_000, 'ft'),
233             'alt_ref0': (0, 'ft'),
234             'alt_constraint_ref': (10000, 'ft'),
235             'mass_lower': (0, 'lbm'),
236             'mass_upper': (None, 'lbm'),
```

```
237         'mass_ref': (140_000, 'lbm'),
238         'mass_ref0': (0, 'lbm'),
239         'mass_defect_ref': (140_000, 'lbm'),
240         'distance_lower': (3000.0, 'NM'),
241         'distance_upper': (5000.0, 'NM'),
242         'distance_ref': (mission_distance, 'NM'),
243         'distance_ref0': (0, 'NM'),
244         'distance_defect_ref': (100, 'NM'),
245     },
246     'initial_guesses': {
247         'mass': (136000.0, 'lbm'),
248         'altitude': ([37.5e3, 10.0e3], 'ft'),
249         'throttle': ([0.0, 0.0], 'unitless'),
250         'distance': ([0.92 * mission_distance, 0.96 *
mission_distance], 'NM'),
251         'time': ([28000.0, 500.0], 's'),
252     },
253 },
254 'desc2': {
255     'user_options': {
256         'num_segments': 1,
257         'order': 7,
258         'fix_initial': False,
259         'input_initial': False,
260         'EAS_limit': (250, 'kn'),
261         'mach_cruise': 0.80,
262         'input_speed_type': SpeedType.EAS,
263         'final_altitude': (1000, 'ft'),
264         'duration_bounds': ((100.0, 5000), 's'),
265         'duration_ref': (500, 's'),
266         'alt_lower': (500, 'ft'),
267         'alt_upper': (11_000, 'ft'),
268         'alt_ref': (10.0e3, 'ft'),
269         'alt_ref0': (1000, 'ft'),
270         'alt_constraint_ref': (1000, 'ft'),
271         'mass_lower': (0, 'lbm'),
272         'mass_upper': (None, 'lbm'),
273         'mass_ref': (150_000, 'lbm'),
274         'mass_defect_ref': (150_000, 'lbm'),
275         'distance_lower': (0, 'NM'),
```

```
276         'distance_upper': (5000, 'NM'),
277         'distance_ref': (3500, 'NM'),
278         'distance_defect_ref': (100, 'NM'),
279     },
280     'initial_guesses': {
281         'mass': (136000.0, 'lbm'),
282         'altitude': ([10.0e3, 1.0e3], 'ft'),
283         'throttle': ([0.0, 0.0], 'unitless'),
284         'distance': ([0.96 * mission_distance,
mission_distance], 'NM'),
285         'time': ([28500.0, 500.0], 's'),
286     },
287 },
288 }
289
290
291 def phase_info_parameterization(phase_info, post_mission_info,
aviary_inputs):
292     """
293     Modify the values in the phase_info dictionary to accomodate
different values
294     for the following mission design inputs: cruise altitude,
cruise Mach number,
295     cruise range, design gross mass.
296
297     Parameters
298     -----
299     phase_info : dict
300         Dictionary of phase settings for a mission profile
301     post_mission_info : dict
302         Dictionary of phase settings for a post mission profile
303     aviary_inputs : <AviaryValues>
304         Object containing values and units for all aviary inputs
and options
305
306     Returns
307     -----
308     dict
309         Modified phase_info that has been changed to match the new
mission
```

```
310     parameters
311     """
312     range_cruise = aviary_inputs.get_val(Mission.Design.RANGE,
313     units='NM')
314     alt_cruise = aviary_inputs.get_val(Mission.Design.
315     CRUISE_ALTITUDE, units='ft')
316     gross_mass = aviary_inputs.get_val(Mission.Design.GROSS_MASS,
317     units='lbm')
318     mach_cruise = aviary_inputs.get_val(Mission.Design.MACH)
319
320     # Range
321     old_range_cruise = phase_info['desc2']['initial_guesses']['distance'][0][1]
322     range_scale = 1.0
323     if range_cruise != old_range_cruise:
324         phase_info['desc1']['initial_guesses']['distance'] = (
325             [0.92 * range_cruise, 0.96 * range_cruise],
326             'NM',
327         )
328         phase_info['desc2']['initial_guesses']['distance'] = (
329             [0.96 * range_cruise, range_cruise],
330             'NM',
331         )
332         range_scale = range_cruise / old_range_cruise
333
334     # Altitude
335     old_alt_cruise = phase_info['climb2']['user_options']['final_altitude'][0]
336     if alt_cruise != old_alt_cruise:
337         phase_info['climb2']['user_options']['final_altitude'] = (
338             alt_cruise, 'ft')
339         phase_info['climb2']['initial_guesses']['altitude'] =
340         ([10.0e3, alt_cruise], 'ft')
341         phase_info['cruise']['initial_guesses']['altitude'] = (
342             alt_cruise, 'ft')
343         phase_info['desc1']['initial_guesses']['altitude'] = (
344             alt_cruise, 10.0e3, 'ft')
345
346     # TODO - Could adjust time guesses/bounds in climb2 and
347     desc2.
```

```
340
341     # Mass
342     old_gross_mass = 175400.0
343     if gross_mass != old_gross_mass:
344         # Note, this requires that the guess for gross mass is
345         # pretty close to the
346         # compute mass.
347
348         fuel_used = 35000 * range_scale
349         phase_info['groundroll']['initial_guesses']['mass'] = ([
350         gross_mass, gross_mass], 'lbm')
351         phase_info['rotation']['initial_guesses']['mass'] = ([
352         gross_mass, gross_mass], 'lbm')
353         phase_info['accel']['initial_guesses']['mass'] = ([
354         gross_mass, gross_mass], 'lbm')
355         phase_info['ascent']['initial_guesses']['mass'] = ([
356         gross_mass, gross_mass], 'lbm')
357
358         phase_info['cruise']['initial_guesses']['mass'] = ([
359         gross_mass, -fuel_used], 'lbm')
360
361         end_mass = gross_mass - fuel_used
362         phase_info['desc1']['initial_guesses']['mass'] = (end_mass
363         , 'lbm')
364         phase_info['desc2']['initial_guesses']['mass'] = (end_mass
365         , 'lbm')
366
367     # Mach
368     old_mach_cruise = phase_info['cruise']['initial_guesses']['
369     mach'][0]
370     if mach_cruise != old_mach_cruise:
371         phase_info['cruise']['initial_guesses']['mach'] = (
372         mach_cruise, 'unitless')
373
374     return phase_info, post_mission_info
```

B.4 Outputted Phase Info

```
1 phase_info = {
```

```
2     "pre_mission": {"include_takeoff": False, "optimize_mass":
True},
3     "climb_1": {
4         "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
5         "user_options": {
6             "optimize_mach": False,
7             "optimize_altitude": False,
8             "polynomial_control_order": 1,
9             "use_polynomial_control": True,
10            "num_segments": 9,
11            "order": 3,
12            "solve_for_distance": False,
13            "initial_mach": (0.2, "unitless"),
14            "final_mach": (0.72, "unitless"),
15            "mach_bounds": ((0.18000000000000002, 0.74), "unitless
"),
16            "initial_altitude": (0.0, "ft"),
17            "final_altitude": (1500.0, "ft"),
18            "altitude_bounds": ((0.0, 2000.0), "ft"),
19            "throttle_enforcement": "path_constraint",
20            "fix_initial": True,
21            "constrain_final": False,
22            "fix_duration": False,
23            "initial_bounds": ((0.0, 0.0), "min"),
24            "duration_bounds": ((10.5, 31.5), "min"),
25        },
26        "initial_guesses": {"times": ([0, 21], "min")},
27    },
28    "climb_2": {
29        "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
30        "user_options": {
31            "optimize_mach": False,
32            "optimize_altitude": False,
33            "polynomial_control_order": 1,
34            "use_polynomial_control": True,
35            "num_segments": 9,
36            "order": 3,
37            "solve_for_distance": False,
```

```
38         "initial_mach": (0.72, "unitless"),
39         "final_mach": (0.72, "unitless"),
40         "mach_bounds": ((0.7, 0.74), "unitless"),
41         "initial_altitude": (1500.0, "ft"),
42         "final_altitude": (27000.0, "ft"),
43         "altitude_bounds": ((1000.0, 27500.0), "ft"),
44         "throttle_enforcement": "boundary_constraint",
45         "fix_initial": False,
46         "constrain_final": False,
47         "fix_duration": False,
48         "initial_bounds": ((10.5, 31.5), "min"),
49         "duration_bounds": ((15.0, 45.0), "min"),
50     },
51     "initial_guesses": {"times": ([21, 30], "min")},
52 },
53 "climb_3": {
54     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
55     "user_options": {
56         "optimize_mach": False,
57         "optimize_altitude": False,
58         "polynomial_control_order": 1,
59         "use_polynomial_control": True,
60         "num_segments": 9,
61         "order": 3,
62         "solve_for_distance": False,
63         "initial_mach": (0.72, "unitless"),
64         "final_mach": (0.72, "unitless"),
65         "mach_bounds": ((0.7, 0.74), "unitless"),
66         "initial_altitude": (27000.0, "ft"),
67         "final_altitude": (35000.0, "ft"),
68         "altitude_bounds": ((26500.0, 35500.0), "ft"),
69         "throttle_enforcement": "path_constraint",
70         "fix_initial": False,
71         "constrain_final": True,
72         "fix_duration": False,
73         "initial_bounds": ((25.5, 76.5), "min"),
74         "duration_bounds": ((6.0, 18.0), "min"),
75     },
76     "initial_guesses": {"times": ([51, 12], "min")},
```

```
77     },
78     "post_mission": {
79         "include_landing": False,
80         "constrain_range": True,
81         "target_range": (443, "nmi"),
82     },
83 }
```

B.5 Add External Subsystem

```
1 from copy import deepcopy
2
3 import aviary.api as av
4 from aviary.api import Aircraft
5 from aviary.examples.external_subsystems.simple_weight.
   simple_weight_builder import (
6     WingWeightBuilder,
7 )
8
9 # Max iterations set to 1 to reduce runtime of example
10 max_iter = 1
11 phase_info = deepcopy(av.default_height_energy_phase_info)
12 # Here we just add the simple weight system to only the pre-
   mission
13 phase_info['pre_mission']['external_subsystems'] = [
   WingWeightBuilder(name='wing_external')]
14
15 prob = av.AviaryProblem()
16
17 # Load aircraft and options data from user
18 # Allow for user overrides here
19 prob.load_inputs('models/test_aircraft/aircraft_for_bench_FwFm.csv
   ', phase_info)
20
21 # Have checks for clashing user inputs
22 # Raise warnings or errors depending on how clashing the issues
   are
23 prob.check_and_preprocess_inputs()
24
25 prob.add_pre_mission_systems()
```

```
26
27 prob.add_phases()
28
29 prob.add_post_mission_systems()
30
31 # Link phases and variables
32 prob.link_phases()
33
34 prob.add_driver('SLSQP', max_iter)
35
36 prob.add_design_variables()
37
38 prob.add_objective()
39
40 prob.setup()
41
42 prob.set_initial_guesses()
43
44 prob.run_aviary_problem(suppress_solver_print=True)
45
46 print('Engine Mass', prob.get_val(av.Aircraft.Engine.MASS))
47 print('Wing Mass', prob.get_val(av.Aircraft.Wing.MASS))
48 print('Horizontal Tail Mass', prob.get_val(av.Aircraft.
      HorizontalTail.MASS))
```

B.6 Level 3 Example: N3CC Aircraft

```
1 '''
2 NOTES:
3 Includes:
4 Takeoff, Climb, Cruise, Descent, Landing
5 Computed Aero
6 N3CC data
7 '''
8 import unittest
9
10 import dymos as dm
11 import numpy as np
12 import openmdao.api as om
13 import scipy.constants as _units
```

```
14 from openmdao.utils.assert_utils import assert_near_equal
15 from openmdao.utils.testing_utils import use_tempdirs
16 from openmdao.utils.testing_utils import require_pyoptsparse
17
18 from aviary.mission.flops_based.phases.build_landing import
    Landing
19 from aviary.mission.flops_based.phases.build_takeoff import
    Takeoff
20 from aviary.utils.functions import set_aviary_initial_values
21 from aviary.utils.test_utils.assert_utils import
    warn_timeseries_near_equal
22 from aviary.validation_cases.validation_tests import
    get_flops_inputs
23 from aviary.variable_info.functions import setup_trajectory_params
24 from aviary.utils.aviary_values import AviaryValues
25 from aviary.variable_info.variables_in import VariablesIn
26 from aviary.mission.flops_based.phases.energy_phase import
    EnergyPhase
27
28 from aviary.variable_info.variables import Aircraft, Dynamic,
    Mission
29 from aviary.subsystems.premission import CorePreMission
30 from aviary.interface.default_phase_info.height_energy import
    default_premission_subsystems, default_mission_subsystems
31 from aviary.utils.preprocessors import preprocess_crewpayload
32
33 try:
34     import pyoptsparse
35 except ImportError:
36     pyoptsparse = None
37
38
39 # benchmark for simple sizing problem on the N3CC
40 def run_trajectory(sim=True):
41     prob = om.Problem(model=om.Group())
42     if pyoptsparse:
43         driver = prob.driver = om.pyOptSparseDriver()
44         driver.options["optimizer"] = "SNOPT"
45         # driver.declare_coloring() # currently disabled pending
    resolve of issue 2507
```

```
46         if driver.options["optimizer"] == "SNOPT":
47             driver.opt_settings["Major iterations limit"] = 45
48             driver.opt_settings["Major optimality tolerance"] = 1e
-4
49             driver.opt_settings["Major feasibility tolerance"] = 1
e-6
50             driver.opt_settings["iSumm"] = 6
51         elif driver.options["optimizer"] == "IPOPT":
52             driver.opt_settings["max_iter"] = 100
53             driver.opt_settings["tol"] = 1e-3
54             driver.opt_settings['print_level'] = 4
55
56     else:
57         driver = prob.driver = om.ScipyOptimizeDriver()
58         opt_settings = prob.driver.opt_settings
59
60         driver.options['optimizer'] = 'SLSQP'
61         opt_settings['maxiter'] = 100
62         opt_settings['ftol'] = 5.0e-3
63         opt_settings['eps'] = 1e-2
64
65     #####
66     # Aircraft Input Variables and Options    #
67     #####
68
69     aviary_inputs = get_flops_inputs('N3CC')
70
71     aviary_inputs.set_val(Mission.Landing.LIFT_COEFFICIENT_MAX,
72                          2.4, units="unitless")
73     aviary_inputs.set_val(Mission.Takeoff.LIFT_COEFFICIENT_MAX,
74                          2.0, units="unitless")
75     aviary_inputs.set_val(
76         Mission.Takeoff.ROLLING_FRICTION_COEFFICIENT,
77         val=.0175, units="unitless")
78
79     takeoff_fuel_burned = 577 # lbm TODO: where should this get
connected from?
80     takeoff_thrust_per_eng = 24555.5 # lbf TODO: where should
this get connected from?
81     takeoff_L_over_D = 17.35 # TODO: should this come from aero?
```

```
82
83     aviary_inputs.set_val(Mission.Takeoff.FUEL_SIMPLE,
84                           takeoff_fuel_burned, units='lbm')
85     aviary_inputs.set_val(Mission.Takeoff.LIFT_OVER_DRAG,
86                           takeoff_L_over_D, units="unitless")
87     aviary_inputs.set_val(Mission.Design.THRUST_TAKEOFF_PER_ENG,
88                           takeoff_thrust_per_eng, units='lbf')
89
90     alt_airport = 0 # ft
91
92     alt_i_climb = 0*_units.foot # m
93     alt_f_climb = 35000.0*_units.foot # m
94     mass_i_climb = 131000*_units.lb # kg
95     mass_f_climb = 126000*_units.lb # kg
96     # initial mach set to lower value so it can intersect with
97     takeoff end mach
98     # mach_i_climb = 0.3
99     mach_i_climb = 0.2
100    mach_f_climb = 0.79
101
102    distance_i_climb = 0*_units.nautical_mile # m
103    distance_f_climb = 160.3*_units.nautical_mile # m
104    t_i_climb = 2 * _units.minute # sec
105    t_f_climb = 26.20*_units.minute # sec
106    t_duration_climb = t_f_climb - t_i_climb
107
108    alt_i_cruise = 35000*_units.foot # m
109    alt_f_cruise = 35000*_units.foot # m
110    alt_min_cruise = 35000*_units.foot # m
111    alt_max_cruise = 35000*_units.foot # m
112    mass_i_cruise = 126000*_units.lb # kg
113    mass_f_cruise = 102000*_units.lb # kg
114    cruise_mach = 0.79
115
116    distance_i_cruise = 160.3*_units.nautical_mile # m
117    distance_f_cruise = 3243.9*_units.nautical_mile # m
118    t_i_cruise = 26.20*_units.minute # sec
119    t_f_cruise = 432.38*_units.minute # sec
120    t_duration_cruise = t_f_cruise - t_i_cruise
121
122    alt_i_descent = 35000*_units.foot
123    # final altitude set to 35 to ensure landing is feasible point
```

```
121     # alt_f_descent = 0*_units.foot
122     alt_f_descent = 35*_units.foot
123     mach_i_descent = 0.79
124     mach_f_descent = 0.3
125     mass_i_descent = 102000*_units.pound
126     mass_f_descent = 101000*_units.pound
127     distance_i_descent = 3243.9*_units.nautical_mile
128     distance_f_descent = 3378.7*_units.nautical_mile
129     t_i_descent = 432.38*_units.minute
130     t_f_descent = 461.62*_units.minute
131     t_duration_descent = t_f_descent - t_i_descent
132
133     #####
134     # Design Variables      #
135     #####
136
137     # Nudge it a bit off the correct answer to verify that the
138     # optimize takes us there.
139     aviary_inputs.set_val(Mission.Design.GROSS_MASS, 135000.0,
140     units='lbm')
141
142     prob.model.add_design_var(Mission.Design.GROSS_MASS, units='
143     lbm',
144
145     lower=100000.0, upper=200000.0, ref
146     =135000)
147
148     takeoff_options = Takeoff(
149         airport_altitude=alt_airport, # ft
150         # no units
151         num_engines=aviary_inputs.get_val(Aircraft.Engine.
152     NUM_ENGINES)
153     )
154
155     #####
156     # Define Phases      #
157     #####
158     num_segments_climb = 6
159     num_segments_cruise = 1
160     num_segments_descent = 5
```

```
156     climb_seg_ends, _ = dm.utils.lgl.lgl(num_segments_climb + 1)
157     descent_seg_ends, _ = dm.utils.lgl.lgl(num_segments_descent +
158     1)
159
160     transcription_climb = dm.Radau(
161         num_segments=num_segments_climb, order=3, compressed=True,
162         segment_ends=climb_seg_ends)
163     transcription_cruise = dm.Radau(
164         num_segments=num_segments_cruise, order=3, compressed=True
165     )
166     transcription_descent = dm.Radau(
167         num_segments=num_segments_descent, order=3, compressed=
168     True,
169         segment_ends=descent_seg_ends)
170
171     climb_options = EnergyPhase(
172         'test_climb',
173         user_options=AviaryValues({
174             'initial_altitude': (alt_i_climb, 'm'),
175             'final_altitude': (alt_f_climb, 'm'),
176             'initial_mach': (mach_i_climb, 'unitless'),
177             'final_mach': (mach_f_climb, 'unitless'),
178             'fix_initial': (False, 'unitless'),
179             'input_initial': (True, 'unitless'),
180             'use_polynomial_control': (False, 'unitless'),
181         }),
182         core_subsystems=default_mission_subsystems,
183         subsystem_options={'core_aerodynamics': {'method': '
184     computed'}},
185         transcription=transcription_climb,
186     )
187
188     cruise_options = EnergyPhase(
189         'test_cruise',
190         user_options=AviaryValues({
191             'initial_altitude': (alt_min_cruise, 'm'),
192             'final_altitude': (alt_max_cruise, 'm'),
193             'initial_mach': (cruise_mach, 'unitless'),
194             'final_mach': (cruise_mach, 'unitless'),
195             'required_available_climb_rate': (300, 'ft/min'),
```

```
192         'fix_initial': (False, 'unitless'),
193     }),
194     core_subsystems=default_mission_subsystems,
195     subsystem_options={'core_aerodynamics': {'method': '
computed'}}},
196     transcription=transcription_cruise,
197 )
198
199 descent_options = EnergyPhase(
200     'test_descent',
201     user_options=AviaryValues({
202         'final_altitude': (alt_f_descent, 'm'),
203         'initial_altitude': (alt_i_descent, 'm'),
204         'initial_mach': (mach_i_descent, 'unitless'),
205         'final_mach': (mach_f_descent, 'unitless'),
206         'fix_initial': (False, 'unitless'),
207         'use_polynomial_control': (False, 'unitless'),
208     }),
209     core_subsystems=default_mission_subsystems,
210     subsystem_options={'core_aerodynamics': {'method': '
computed'}}},
211     transcription=transcription_descent,
212 )
213
214 landing_options = Landing(
215     ref_wing_area=aviary_inputs.get_val(Aircraft.Wing.AREA,
216     units='ft**2'),
217     Cl_max_ldg=aviary_inputs.get_val(
218         Mission.Landing.LIFT_COEFFICIENT_MAX) # no units
219 )
220
221 preprocess_crewpayload(aviary_inputs)
222
223 # Upstream static analysis for aero
224 prob.model.add_subsystem(
225     'pre_mission',
226     CorePreMission(aviary_options=aviary_inputs,
227         subsystems=default_premission_subsystems),
228     promotes_inputs=['aircraft:', 'mission:'],
229     promotes_outputs=['aircraft:', 'mission:'])
```

```
229
230     # directly connect phases (strong_couple = True), or use
linkage constraints (weak
231     # coupling / strong_couple=False)
232     strong_couple = False
233
234     takeoff = takeoff_options.build_phase(False)
235
236     climb = climb_options.build_phase(aviary_options=aviary_inputs
)
237
238     cruise = cruise_options.build_phase(aviary_options=
aviary_inputs)
239
240     descent = descent_options.build_phase(aviary_options=
aviary_inputs)
241
242     landing = landing_options.build_phase(False)
243
244     prob.model.add_subsystem(
245         'takeoff', takeoff, promotes_inputs=['aircraft:*', '
mission:*'],
246         promotes_outputs=['mission:*'])
247
248     traj = prob.model.add_subsystem('traj', dm.Trajectory())
249
250     # if fix_initial is false, can we always set input_initial to
be true for
251     # necessary states, and then ignore if we use a linkage?
252     climb.set_time_options(fix_initial=True, fix_duration=False,
units='s',
253                           duration_bounds=(t_duration_climb*0.5,
t_duration_climb*2),
254                           duration_ref=t_duration_climb)
255     cruise.set_time_options(fix_initial=False, fix_duration=False,
units='s',
256                           duration_bounds=(t_duration_cruise
*0.5, t_duration_cruise*2),
257                           duration_ref=t_duration_cruise,
```

```
258         initial_bounds=(t_duration_climb*0.5,
259         t_duration_climb*2))
260     descent.set_time_options(
261         fix_initial=False, fix_duration=False, units='s',
262         duration_bounds=(t_duration_descent*0.5,
263         t_duration_descent*2),
264         duration_ref=t_duration_descent,
265         initial_bounds=(
266             (t_duration_cruise + t_duration_climb)*0.5,
267             (t_duration_cruise + t_duration_climb)*2))
268
269     traj.add_phase('climb', climb)
270
271     traj.add_phase('cruise', cruise)
272
273     traj.add_phase('descent', descent)
274
275     prob.model.add_subsystem(
276         'landing', landing, promotes_inputs=['aircraft:*', '
277 mission:*'],
278         promotes_outputs=['mission:*'])
279
280     traj.link_phases(["climb", "cruise", "descent"], [
281         "time", Dynamic.Mission.MASS, Dynamic.Mission
282 .DISTANCE], connected=strong_couple)
283
284     traj = setup_trajectory_params(prob.model, traj, aviary_inputs
285 )
286
287     #####
288     # Connect in Takeoff and Landing #
289     #####
290     prob.model.connect(Mission.Takeoff.FINAL_MASS,
291         'traj.climb.initial_states:mass')
292     prob.model.connect(Mission.Takeoff.GROUND_DISTANCE,
293         'traj.climb.initial_states:distance')
294
295     prob.model.connect('traj.descent.states:mass',
296         Mission.Landing.TOUCHDOWN_MASS, src_indices
297     =[-1])
```

```
292     # TODO: approach velocity should likely be connected
293     prob.model.connect('traj.descent.control_values:altitude',
Mission.Landing.INITIAL_ALTITUDE,
294                         src_indices=[-1])
295
296     #####
297     # Constraints          #
298     #####
299
300     ecomp = om.ExecComp('fuel_burned = initial_mass -
descent_mass_final',
301                         initial_mass={'units': 'lbm', 'shape': 1},
302                         descent_mass_final={'units': 'lbm', 'shape
': 1},
303                         fuel_burned={'units': 'lbm', 'shape': 1})
304
305     prob.model.add_subsystem('fuel_burn', ecomp,
306                             promotes_inputs=[
307                                 ('initial_mass', Mission.Design.
GROSS_MASS)],
308                             promotes_outputs=['fuel_burned'])
309
310     prob.model.connect("traj.descent.states:mass",
311                        "fuel_burn.descent_mass_final", src_indices
= [-1])
312
313     # TODO: need to add some sort of check that this value is less
than the fuel capacity
314     # TODO: need to update this with actual FLOPS value, this
gives unrealistic
315     # appearance of accuracy
316     # TODO: the overall_fuel variable is the burned fuel plus the
reserve, but should
317     # also include the unused fuel, and the hierarchy variable
name should be more clear
318     ecomp = om.ExecComp('overall_fuel = fuel_burned + fuel_reserve
',
319                         fuel_burned={'units': 'lbm', 'shape': 1},
320                         fuel_reserve={'units': 'lbm', 'val':
2173.},
```

```
321         overall_fuel={'units': 'lbm'})
322     prob.model.add_subsystem('fuel_calc', ecomp,
323                             promotes_inputs=['fuel_burned'],
324                             promotes_outputs=['overall_fuel'])
325
326     ecomp = om.ExecComp(
327         'mass_resid = operating_empty_mass + overall_fuel +
payload_mass ',
328         '- initial_mass',
329         operating_empty_mass={'units': 'lbm'},
330         overall_fuel={'units': 'lbm'},
331         payload_mass={'units': 'lbm'},
332         initial_mass={'units': 'lbm'},
333         mass_resid={'units': 'lbm'})
334
335     prob.model.add_subsystem(
336         'mass_constraint', ecomp,
337         promotes_inputs=[
338             ('operating_empty_mass', Aircraft.Design.
OPERATING_MASS),
339             'overall_fuel',
340             ('payload_mass', Aircraft.CrewPayload.
TOTAL_PAYLOAD_MASS),
341             ('initial_mass', Mission.Design.GROSS_MASS)],
342         promotes_outputs=['mass_resid'])
343
344     prob.model.add_constraint('mass_resid', equals=0.0, ref=1.0)
345
346     #####
347     # Add Objective Function #
348     #####
349
350     # This is an example of a overall mission objective
351     # create a compound objective that minimizes climb time and
maximizes final mass
352     # we are maxing final mass b/c we don't have an independent
value for fuel_mass yet
353     # we are going to normalize these (making each of the sub-
objectives approx = 1 )
354     # TODO: change the scaling on climb_duration
```

```
355     prob.model.add_subsystem(
356         "regularization",
357         om.ExecComp(
358             "reg_objective = fuel_mass/1500",
359             reg_objective=0.0,
360             fuel_mass={"units": "lbm", "shape": 1},
361         ),
362         promotes_outputs=['reg_objective']
363     )
364     # connect the final mass from cruise into the objective
365     prob.model.connect(Mission.Design.FUEL_MASS, "regularization.
fuel_mass")
366
367     prob.model.add_objective('reg_objective', ref=1)
368
369     # Set initial default values for all LEAPS aircraft variables.
370     set_aviary_initial_values(prob.model, aviary_inputs)
371
372     prob.model.add_subsystem(
373         'input_sink',
374         VariablesIn(aviary_options=aviary_inputs),
375         promotes_inputs=['*'],
376         promotes_outputs=['*']
377     )
378
379     prob.setup(force_alloc_complex=True)
380
381     #####
382     # Intial Settings for States and Controls #
383     #####
384
385     prob.set_val('traj.climb.t_initial', t_i_climb, units='s')
386     prob.set_val('traj.climb.t_duration', t_duration_climb, units=
's')
387
388     prob.set_val('traj.climb.controls:altitude', climb.interp(
389         Dynamic.Mission.ALTITUDE, ys=[alt_i_climb, alt_f_climb]),
units='m')
390     prob.set_val(
391         'traj.climb.controls:mach', climb.interp(
```

```
392         Dynamic.Mission.MACH, ys=[mach_i_climb, mach_f_climb])
, units='unitless')
393     prob.set_val('traj.climb.states:mass', climb.interp(
394         Dynamic.Mission.MASS, ys=[mass_i_climb, mass_f_climb]),
units='kg')
395     prob.set_val('traj.climb.states:distance', climb.interp(
396         Dynamic.Mission.DISTANCE, ys=[distance_i_climb,
distance_f_climb]), units='m')
397
398     prob.set_val('traj.cruise.t_initial', t_i_cruise, units='s')
399     prob.set_val('traj.cruise.t_duration', t_duration_cruise,
units='s')
400
401     prob.set_val('traj.cruise.polynomial_controls:altitude',
cruise.interp(
402         Dynamic.Mission.ALTITUDE, ys=[alt_i_cruise, alt_f_cruise])
, units='m')
403     prob.set_val(
404         'traj.cruise.polynomial_controls:mach', cruise.interp(
405         Dynamic.Mission.MACH, ys=[cruise_mach, cruise_mach]),
units='unitless')
406     prob.set_val('traj.cruise.states:mass', cruise.interp(
407         Dynamic.Mission.MASS, ys=[mass_i_cruise, mass_f_cruise]),
units='kg')
408     prob.set_val('traj.cruise.states:distance', cruise.interp(
409         Dynamic.Mission.DISTANCE, ys=[distance_i_cruise,
distance_f_cruise]), units='m')
410
411     prob.set_val('traj.descent.t_initial', t_i_descent, units='s')
412     prob.set_val('traj.descent.t_duration', t_duration_descent,
units='s')
413
414     prob.set_val('traj.descent.controls:altitude', descent.interp(
415         Dynamic.Mission.ALTITUDE, ys=[alt_i_descent, alt_f_descent
]), units='m')
416     prob.set_val(
417         'traj.descent.controls:mach', descent.interp(
418         Dynamic.Mission.MACH, ys=[mach_i_descent,
mach_f_descent]), units='unitless')
419     prob.set_val('traj.descent.states:mass', descent.interp(
```

```
420     Dynamic.Mission.MASS, ys=[mass_i_descent, mass_f_descent])
    , units='kg')
421     prob.set_val('traj.descent.states:distance', descent.interp(
422         Dynamic.Mission.DISTANCE, ys=[distance_i_descent,
    distance_f_descent]), units='m')
423
424     # Turn off solver printing so that the SNOPT output is
    readable.
425     prob.set_solver_print(level=0)
426
427     dm.run_problem(prob, simulate=sim, make_plots=False,
    simulate_kwargs={
428         'times_per_seg': 100, 'atol': 1e-9, 'rtol': 1e
    -9},
429         solution_record_file='N3CC_sizing.db')
430     # prob.run_model()
431     # z=prob.check_totals(method='cs', step=2e-40, compact_print=
    False)
432     # exit()
433     prob.record("final")
434     prob.cleanup()
435
436     return prob
437
438
439 @use_tempdirs
440 class ProblemPhaseTestCase(unittest.TestCase):
441
442     @require_pyoptsparse(optimizer="SNOPT")
443     def bench_test_sizing_N3CC(self):
444
445         prob = run_trajectory(sim=False)
446
447         times_climb = prob.get_val('traj.climb.timeseries.time',
    units='s')
448         altitudes_climb = prob.get_val(
449             'traj.climb.timeseries.altitude', units='m')
450         masses_climb = prob.get_val('traj.climb.timeseries.mass',
    units='kg')
```

```
451     distances_climb = prob.get_val('traj.climb.timeseries.  
distance', units='m')  
452     velocities_climb = prob.get_val(  
453         'traj.climb.timeseries.velocity', units='m/s')  
454     thrusts_climb = prob.get_val('traj.climb.timeseries.  
thrust_net_total', units='N')  
455     times_cruise = prob.get_val('traj.cruise.timeseries.time',  
units='s')  
456     altitudes_cruise = prob.get_val(  
457         'traj.cruise.timeseries.altitude', units='m')  
458     masses_cruise = prob.get_val('traj.cruise.timeseries.mass',  
units='kg')  
459     distances_cruise = prob.get_val('traj.cruise.timeseries.  
distance', units='m')  
460     velocities_cruise = prob.get_val(  
461         'traj.cruise.timeseries.velocity', units='m/s')  
462     thrusts_cruise = prob.get_val(  
463         'traj.cruise.timeseries.thrust_net_total', units='N')  
464     times_descent = prob.get_val('traj.descent.timeseries.time',  
units='s')  
465     altitudes_descent = prob.get_val(  
466         'traj.descent.timeseries.altitude', units='m')  
467     masses_descent = prob.get_val('traj.descent.timeseries.  
mass', units='kg')  
468     distances_descent = prob.get_val('traj.descent.timeseries.  
distance', units='m')  
469     velocities_descent = prob.get_val(  
470         'traj.descent.timeseries.velocity', units='m/s')  
471     thrusts_descent = prob.get_val(  
472         'traj.descent.timeseries.thrust_net_total', units='N')  
473  
474     expected_times_s_climb = [[120.], [163.76325828],  
[224.14762249], [243.2590673],  
475                                     [243.2590673], [336.41088085],  
[464.94137099],  
476                                     [505.62083166], [505.62083166],  
[626.47618404],  
477                                     [793.2319034], [846.00951843],  
[846.00951843],
```

```
478         [966.8648708], [1133.62059016],
    [1186.39820519],
479         [1186.39820519],
    [1279.55001873], [1408.08050887],
480         [1448.75996955],
    [1448.75996955], [1492.52322782],
481         [1552.90759204],
    [1572.01903685]]
482     expected_altitudes_m_climb = [[10.668], [0.],
    [835.43072799], [1237.19027083],
483         [1237.19027083],
    [3154.43458807], [5478.53141388],
484         [6035.03506592],
    [6035.03506592], [7369.93558792],
485         [8611.93242084],
    [8931.907682], [8931.907682],
486         [9555.56028912],
    [10196.52547754], [10341.80261401],
487         [10341.80261401],
    [10526.85288051], [10653.9273369],
488         [10668.], [10668.],
    [10668.], [10664.89939949], [10668.]]
489     expected_masses_kg_climb = [[58331.64520977],
    [58289.14326023], [58210.1552262],
490         [58183.99841695],
    [58183.99841695], [58064.21371439],
491         [57928.02594919],
    [57893.85802859], [57893.85802859],
492         [57803.5753272],
    [57701.17154376], [57671.70469428],
493         [57671.70469428],
    [57609.99954455], [57532.67046087],
494         [57509.28816794],
    [57509.28816794], [57468.36184014],
495         [57411.39726843],
    [57392.97463799], [57392.97463799],
496         [57372.80054331],
    [57344.30023996], [57335.11578186]]
497     expected_distances_m_climb = [[1459.66454213],
    [6138.11750563], [15269.84014039],
```

```

498                                     [18334.78691191] ,
    [18334.78691191] , [34224.35398213] ,
499                                     [57056.15756331] ,
    [64259.82264908] , [64259.82264908] ,
500                                     [85983.44219477] ,
    [116781.82372802] , [
501                                     126787.42506431] ,
502                                     [126787.42506431] ,
    [149770.216723] , [181655.376959] ,
503                                     [191785.63505195] ,
    [191785.63505195] , [
504                                     210054.32022093] ,
505                                     [236459.08240245] ,
    [245218.76016711] , [
506                                     245218.76016711] ,
507                                     [254896.51199279] ,
    [268679.73823007] , [273140.04867091]]
508     expected_velocities_ms_climb = [[77.19291754] ,
    [132.35228283] , [162.28279625] ,
509                                     [166.11250634] ,
    [166.11250634] , [176.30796789] ,
510                                     [178.55049791] ,
    [178.67862048] , [178.67862048] ,
511                                     [181.75616771] ,
    [188.37687907] , [189.78671051] ,
512                                     [189.78671051] ,
    [190.67789763] , [191.79702196] ,
513                                     [193.51306342] ,
    [193.51306342] , [199.28763405] ,
514                                     [212.62699415] ,
    [218.00379223] , [218.00379223] ,
515                                     [224.21350812] ,
    [232.18822869] , [234.25795132]]
516     expected_thrusts_N_climb = [[82387.90445676] ,
    [105138.56964482] , [113204.81413537] ,
517                                     [110631.69881503] ,
    [110631.69881503] , [97595.73505557] ,
518                                     [74672.35033284] ,
    [68787.54639919] , [68787.54639919] ,

```

```
519         [56537.02658008] ,
        [46486.74146611] , [43988.99250831] ,
520         [43988.99250831] ,
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521         [35877.85248136] ,
        [35877.85248136] , [35222.20684522] ,
522         [34829.78305946] ,
        [34857.84665827] , [34857.84665827] ,
523         [34988.40432301] ,
        [35243.28462529] , [35286.14075168]]
524
525         expected_times_s_cruise = [[1572.01903685] ,
        [10224.85688577] ,
526         [22164.00704809] ,
        [25942.70725365]]
527         expected_altitudes_m_cruise = [[10668.] , [10668.] ,
528         [10668.] , [10668.]]
529         expected_masses_kg_cruise = [[57335.11578186] ,
        [53895.3524649] ,
530         [49306.34176818] ,
        [47887.72131688]]
531         expected_distances_m_cruise = [[273140.04867091] ,
        [2300136.11626779] ,
532         [5096976.9738027] ,
        [5982167.54261146]]
533         expected_velocities_ms_cruise = [[234.25795132] ,
        [234.25795132] ,
534         [234.25795132] ,
        [234.25795132]]
535         expected_thrusts_N_cruise = [[28998.46944214] ,
        [28027.44677784] ,
536         [26853.54343662] ,
        [26522.10071819]]
537
538         expected_times_s_descent = [[25942.70725365] ,
        [26017.49838255] , [26120.69487534] ,
539         [26153.35621248] ,
        [26153.35621248] , [26306.10095576] ,
540         [26516.85752584] ,
        [26583.56125968] , [26583.56125968] ,
```

```

541         [26765.15964678] ,
        [27015.72835621] , [27095.03249603] ,
542         [27095.03249603] ,
        [27247.77723931] , [27458.5338094] ,
543         [27525.23754324] ,
        [27525.23754324] , [27600.02867214] ,
544         [27703.22516493] ,
        [27735.88650207]]
545     expected_altitudes_m_descent = [[10668.] , [10668.] ,
        [10065.85989164] ,
546         [9813.33438203] ,
        [9813.33438203] , [8725.84180063] ,
547         [7399.4358998] ,
        [6995.36734403] , [6995.36734403] ,
548         [5880.98032937] ,
        [4300.0193441] , [3787.54388607] ,
549         [3787.54388607] ,
        [2768.24427675] , [1328.48487414] ,
550         [872.88952055] ,
        [872.88952055] , [393.61709386] ,
551         [10.668] , [10.668]]
552     expected_masses_kg_descent = [[47887.72131688] ,
        [47887.72131688] , [47887.72131688] ,
553         [47887.72131688] ,
        [47887.72131688] , [47887.72131688] ,
554         [47887.72131688] ,
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557         [47842.09391697] ,
        [47842.09391697] , [47833.150133] ,
558         [47820.60083267] ,
        [47816.69389115]]
559     expected_distances_m_descent = [[5982167.54261146] ,
        [5998182.9986382] , [6017437.15474761] ,
560         [6023441.80485498] ,
        [6023441.80485498] , [
561         6050450.80904601] ,

```

```
562         [6085202.09693457], [6095472.55993089], [  
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564         [6122427.64793619], [6158176.53029461], [  
565         6169433.26612421],  
566         [6169433.26612421], [6191073.79296936], [  
567         6220839.65410345],  
568         [6230195.89769052], [6230195.89769052], [  
569         6240573.15704622],  
570         [6253740.15118502], [6257352.4]]  
571     expected_velocities_ms_descent = [[234.25795132],  
[197.64415171], [182.5029101],  
572                                     [181.15994177],  
[181.15994177], [172.42254637],  
573                                     [156.92424445],  
[152.68023428], [152.68023428],  
574                                     [145.15327267],  
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575                                     [141.72294853],  
[141.82174008], [140.7384589],  
576                                     [139.65952688],  
[139.65952688], [136.46721905],  
577                                     [115.68627038],  
[102.07377559]]  
578     expected_thrusts_N_descent = [[0.], [8.11038373e-13],  
[4.89024663e-13],  
579                                     [-3.80747087e-14], [0.],  
[1.10831527e-12],  
580                                     [7.77983996e-13],  
[-6.64041439e-16], [0.],  
581                                     [0.], [-5.7108371e-14],  
[-8.28280737e-14],  
582                                     [0.], [1.14382967e-13],  
[5.36023712e-14],  
583                                     [-3.04972888e-14], [0.],  
[-1.0682523e-13],  
584                                     [-6.30544276e-14],  
[5.37050667e-15]]  
585     expected_times_s_climb = np.array(expected_times_s_climb)  
586     expected_altitudes_m_climb = np.array(  
expected_altitudes_m_climb)
```

```
587         expected_masses_kg_climb = np.array(  
expected_masses_kg_climb)  
588         expected_distances_m_climb = np.array(  
expected_distances_m_climb)  
589         expected_velocities_ms_climb = np.array(  
expected_velocities_ms_climb)  
590         expected_thrusts_N_climb = np.array(  
expected_thrusts_N_climb)  
591  
592         expected_times_s_cruise = np.array(expected_times_s_cruise  
)  
593         expected_altitudes_m_cruise = np.array(  
expected_altitudes_m_cruise)  
594         expected_masses_kg_cruise = np.array(  
expected_masses_kg_cruise)  
595         expected_distances_m_cruise = np.array(  
expected_distances_m_cruise)  
596         expected_velocities_ms_cruise = np.array(  
expected_velocities_ms_cruise)  
597         expected_thrusts_N_cruise = np.array(  
expected_thrusts_N_cruise)  
598  
599         expected_times_s_descent = np.array(  
expected_times_s_descent)  
600         expected_altitudes_m_descent = np.array(  
expected_altitudes_m_descent)  
601         expected_masses_kg_descent = np.array(  
expected_masses_kg_descent)  
602         expected_distances_m_descent = np.array(  
expected_distances_m_descent)  
603         expected_velocities_ms_descent = np.array(  
expected_velocities_ms_descent)  
604         expected_thrusts_N_descent = np.array(  
expected_thrusts_N_descent)  
605  
606         # Check Objective and other key variables to a reasonably  
tight tolerance.  
607  
608         # TODO: update truth values once everyone is using latest  
Dymos
```

```
609         rtol = 5e-2
610
611         # Mass at the end of Descent
612         assert_near_equal(masses_descent[-1],
613                           expected_masses_kg_descent[-1],
614                           tolerance=rtol)
615
616         # Range at the end of Descent
617         assert_near_equal(distances_descent[-1],
618                           expected_distances_m_descent[-1],
619                           tolerance=rtol)
620
621         # Flight time
622         assert_near_equal(times_descent[-1],
623                           expected_times_s_descent[-1], tolerance=
624                           rtol)
625
626         # Check mission values.
627
628         # NOTE rtol = 0.05 = 5% different from truth (first
629         # timeseries)
630         #         atol = 2 = no more than +/-2 meter/second/kg
631         # difference between values
632         #         atol_altitude = 30 ft. There is occasional time-
633         # shifting with the N3CC
634         #         model during climb and descent so
635         # we need a looser
636         #         absolute tolerance for the points
637         # near the ground.
638         rtol = .05
639         atol = 2.0
640         atol_altitude = 30.0
641
642         # FLIGHT PATH
643         # CLIMB
644         warn_timeseries_near_equal(
645             times_climb, altitudes_climb, expected_times_s_climb,
646             expected_altitudes_m_climb, abs_tolerance=
647             atol_altitude, rel_tolerance=rtol)
648         warn_timeseries_near_equal(
```

```
640         times_climb, masses_climb, expected_times_s_climb,
641         expected_masses_kg_climb, abs_tolerance=atol,
        rel_tolerance=rtol)
642     warn_timeseries_near_equal(
643         times_climb, distances_climb, expected_times_s_climb,
644         expected_distances_m_climb, abs_tolerance=atol,
        rel_tolerance=rtol)
645     warn_timeseries_near_equal(
646         times_climb, velocities_climb, expected_times_s_climb,
647         expected_velocities_ms_climb, abs_tolerance=atol,
        rel_tolerance=rtol)
648     warn_timeseries_near_equal(
649         times_climb, thrusts_climb, expected_times_s_climb,
650         expected_thrusts_N_climb, abs_tolerance=atol,
        rel_tolerance=rtol)
651
652     # CRUISE
653     warn_timeseries_near_equal(
654         times_cruise, altitudes_cruise,
        expected_times_s_cruise,
655         expected_altitudes_m_cruise, abs_tolerance=atol,
        rel_tolerance=rtol)
656     warn_timeseries_near_equal(
657         times_cruise, masses_cruise, expected_times_s_cruise,
658         expected_masses_kg_cruise, abs_tolerance=atol,
        rel_tolerance=rtol)
659     warn_timeseries_near_equal(
660         times_cruise, distances_cruise,
        expected_times_s_cruise,
661         expected_distances_m_cruise, abs_tolerance=atol,
        rel_tolerance=rtol)
662     warn_timeseries_near_equal(
663         times_cruise, velocities_cruise,
        expected_times_s_cruise,
664         expected_velocities_ms_cruise, abs_tolerance=atol,
        rel_tolerance=rtol)
665     warn_timeseries_near_equal(
666         times_cruise, thrusts_cruise, expected_times_s_cruise,
667         expected_thrusts_N_cruise, abs_tolerance=atol,
        rel_tolerance=rtol)
```

```
668
669     # DESCENT
670     warn_timeseries_near_equal(
671         times_descent, altitudes_descent,
672         expected_times_s_descent,
673         expected_altitudes_m_descent, abs_tolerance=
674         atol_altitude,
675         rel_tolerance=rtol)
676     warn_timeseries_near_equal(
677         times_descent, masses_descent,
678         expected_times_s_descent,
679         expected_masses_kg_descent, abs_tolerance=atol,
680         rel_tolerance=rtol)
681     warn_timeseries_near_equal(
682         times_descent, distances_descent,
683         expected_times_s_descent,
684         expected_distances_m_descent, abs_tolerance=atol,
685         rel_tolerance=rtol)
686     warn_timeseries_near_equal(
687         times_descent, velocities_descent,
688         expected_times_s_descent,
689         expected_velocities_ms_descent, abs_tolerance=atol,
690         rel_tolerance=rtol)
691     warn_timeseries_near_equal(
692         times_descent, thrusts_descent,
693         expected_times_s_descent,
694         expected_thrusts_N_descent, abs_tolerance=atol,
695         rel_tolerance=rtol)
696
697 if __name__ == '__main__':
698     z = ProblemPhaseTestCase()
699     z.bench_test_sizing_N3CC()
```

B.7 Engine Deck file

```
1 # FLOPS-derived engine deck converted from turbofan_28_ENGDEK
2
```

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

	Mach_Number (unitless),	Altitude (ft),	Throttle (unitless),	Gross_Thrust (lbf),	Ram_Drag (lbf),	Fuel_Flow (lb/h),	NOx_Rate (lb/h)
3							
4		0.0,	0.0,			21.0,	
	1446.4,		0.0,		842.2,		4.7876
5		0.0,	0.0,			22.0,	
	2314.3,		0.0,		976.0,		5.1926
6		0.0,	0.0,			24.0,	
	4049.9,		0.0,		1281.0,		6.6532
7		0.0,	0.0,			26.0,	
	5785.6,		0.0,		1659.9,		8.2234
8		0.0,	0.0,			30.0,	
	9642.7,		0.0,		2621.6,		12.0946
9		0.0,	0.0,			34.0,	
	13499.8,		0.0,		3673.3,		15.0321
10		0.0,	0.0,			38.0,	
	17356.9,		0.0,		4795.2,		17.5877
11		0.0,	0.0,			42.0,	
	21214.0,		0.0,		5979.1,		19.8547
12		0.0,	0.0,			46.0,	
	25071.1,		0.0,		7258.1,		33.3976
13		0.0,	0.0,			48.0,	
	26999.7,		0.0,		7932.6,		49.2185
14		0.0,	0.0,			50.0,	
	28928.1,		0.0,		8662.3,		61.9894
15		0.0,	2000.0,			21.0,	
	1446.4,		0.0,		781.8,		5.2521
16		0.0,	2000.0,			22.0,	
	2314.2,		0.0,		914.2,		5.1431
17		0.0,	2000.0,			24.0,	
	4049.9,		0.0,		1220.2,		6.7284
18		0.0,	2000.0,			26.0,	
	5785.6,		0.0,		1608.2,		8.4472
19		0.0,	2000.0,			30.0,	
	9642.7,		0.0,		2572.5,		12.5205
20		0.0,	2000.0,			34.0,	
	13499.7,		0.0,		3624.6,		15.6007
21		0.0,	2000.0,			38.0,	
	17356.8,		0.0,		4748.2,		18.2407

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

22		0.0,	2000.0,	42.0,	
	21213.8,		0.0,	5953.1,	20.6168
23		0.0,	2000.0,	46.0,	
	25070.8,		0.0,	7274.3,	46.5192
24		0.0,	2000.0,	48.0,	
	26999.7,		0.0,	8005.4,	61.6004
25		0.0,	2000.0,	50.0,	
	28928.0,		0.0,	8769.0,	72.5104
26		0.0,	5000.0,	21.0,	
	1338.1,		0.0,	706.8,	6.8008
27		0.0,	5000.0,	22.0,	
	2140.9,		0.0,	828.3,	5.03
28		0.0,	5000.0,	24.0,	
	3746.7,		0.0,	1111.0,	6.2319
29		0.0,	5000.0,	26.0,	
	5352.3,		0.0,	1469.9,	7.9885
30		0.0,	5000.0,	30.0,	
	8920.6,		0.0,	2355.4,	12.0275
31		0.0,	5000.0,	34.0,	
	12488.9,		0.0,	3323.4,	15.1312
32		0.0,	5000.0,	38.0,	
	16057.1,		0.0,	4353.1,	17.7742
33		0.0,	5000.0,	42.0,	
	19625.3,		0.0,	5473.5,	20.1814
34		0.0,	5000.0,	46.0,	
	23193.5,		0.0,	6708.4,	39.1314
35		0.0,	5000.0,	48.0,	
	24977.9,		0.0,	7391.9,	57.3145
36		0.0,	5000.0,	50.0,	
	26761.8,		0.0,	8104.6,	69.2582
37		0.1,	0.0,	21.0,	
	2503.9,	1057.5,		905.8,	4.7726
38		0.1,	0.0,	22.0,	
	3575.1,	1260.9,		1088.1,	5.7209
39		0.1,	0.0,	24.0,	
	5626.3,	1576.4,		1525.4,	7.6905
40		0.1,	0.0,	26.0,	
	7615.0,	1829.5,		2001.1,	9.4545
41		0.1,	0.0,	30.0,	
	11922.9,	2280.3,		3129.8,	13.5965

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

42		0.1 ,	0.0 ,	34.0 ,	
	16145.2 ,		2645.4 ,	4326.3 ,	16.5878
43		0.1 ,	0.0 ,	38.0 ,	
	20316.5 ,		2959.7 ,	5587.6 ,	19.1578
44		0.1 ,	0.0 ,	42.0 ,	
	24452.2 ,		3238.4 ,	6932.0 ,	26.8701
45		0.1 ,	0.0 ,	46.0 ,	
	28560.1 ,		3489.2 ,	8389.7 ,	57.6579
46		0.1 ,	0.0 ,	48.0 ,	
	30603.9 ,		3604.5 ,	9194.3 ,	69.2477
47		0.1 ,	0.0 ,	50.0 ,	
	32642.3 ,		3714.3 ,	10032.8 ,	77.4403
48		0.1 ,	2000.0 ,	21.0 ,	
	2330.3 ,		984.5 ,	824.4 ,	4.924
49		0.1 ,	2000.0 ,	22.0 ,	
	3327.1 ,		1173.8 ,	991.2 ,	5.5336
50		0.1 ,	2000.0 ,	24.0 ,	
	5235.7 ,		1467.4 ,	1391.5 ,	7.5234
51		0.1 ,	2000.0 ,	26.0 ,	
	7086.3 ,		1702.9 ,	1826.8 ,	9.2983
52		0.1 ,	2000.0 ,	30.0 ,	
	11094.9 ,		2122.6 ,	2859.5 ,	13.4284
53		0.1 ,	2000.0 ,	34.0 ,	
	15023.5 ,		2462.3 ,	3960.7 ,	16.4467
54		0.1 ,	2000.0 ,	38.0 ,	
	18904.9 ,		2754.8 ,	5117.1 ,	19.0209
55		0.1 ,	2000.0 ,	42.0 ,	
	22752.9 ,		3013.8 ,	6361.1 ,	24.7835
56		0.1 ,	2000.0 ,	46.0 ,	
	26574.2 ,		3246.4 ,	7721.3 ,	56.6411
57		0.1 ,	2000.0 ,	48.0 ,	
	28476.4 ,		3353.7 ,	8462.9 ,	68.5093
58		0.1 ,	2000.0 ,	50.0 ,	
	30372.6 ,		3455.8 ,	9235.9 ,	77.0405
59		0.1 ,	5000.0 ,	21.0 ,	
	2084.6 ,		880.6 ,	738.0 ,	6.5816
60		0.1 ,	5000.0 ,	22.0 ,	
	2976.4 ,		1050.0 ,	884.8 ,	4.9156
61		0.1 ,	5000.0 ,	24.0 ,	
	4684.1 ,		1312.8 ,	1237.6 ,	6.8861

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

62		0.1 ,	5000.0 ,		26.0 ,
	6339.8 ,		1523.6 ,	1621.7 ,	8.6447
63		0.1 ,	5000.0 ,		30.0 ,
	9926.1 ,		1899.3 ,	2532.7 ,	12.6499
64		0.1 ,	5000.0 ,		34.0 ,
	13440.9 ,		2203.3 ,	3503.2 ,	15.6314
65		0.1 ,	5000.0 ,		38.0 ,
	16913.5 ,		2465.1 ,	4524.4 ,	18.1789
66		0.1 ,	5000.0 ,		42.0 ,
	20356.6 ,		2696.9 ,	5621.1 ,	20.4797
67		0.1 ,	5000.0 ,		46.0 ,
	23775.6 ,		2905.2 ,	6820.1 ,	42.0756
68		0.1 ,	5000.0 ,		48.0 ,
	25476.8 ,		3001.2 ,	7474.2 ,	58.5348
69		0.1 ,	5000.0 ,		50.0 ,
	27173.2 ,		3092.6 ,	8156.2 ,	69.8119
70		0.1 ,	10000.0 ,		21.0 ,
	1721.9 ,		727.2 ,	612.6 ,	9.402
71		0.1 ,	10000.0 ,		22.0 ,
	2458.8 ,		867.2 ,	730.7 ,	7.2271
72		0.1 ,	10000.0 ,		24.0 ,
	3869.8 ,		1084.5 ,	1014.8 ,	5.7309
73		0.1 ,	10000.0 ,		26.0 ,
	5237.7 ,		1258.8 ,	1324.4 ,	7.4445
74		0.1 ,	10000.0 ,		30.0 ,
	8200.9 ,		1569.4 ,	2059.1 ,	10.9423
75		0.1 ,	10000.0 ,		34.0 ,
	11104.9 ,		1820.8 ,	2841.8 ,	14.0989
76		0.1 ,	10000.0 ,		38.0 ,
	13974.0 ,		2037.3 ,	3665.3 ,	16.5692
77		0.1 ,	10000.0 ,		42.0 ,
	16818.6 ,		2229.1 ,	4548.6 ,	18.7998
78		0.1 ,	10000.0 ,		46.0 ,
	19643.6 ,		2401.3 ,	5515.6 ,	21.9454
79		0.1 ,	10000.0 ,		48.0 ,
	21049.0 ,		2480.6 ,	6042.3 ,	33.2727
80		0.1 ,	10000.0 ,		50.0 ,
	22450.7 ,		2556.3 ,	6592.6 ,	50.9804
81		0.2 ,	0.0 ,		21.0 ,
	3984.0 ,		2660.5 ,	927.8 ,	4.88

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

82		0.2,	0.0,	22.0,	
	5132.8,		3015.2,	1158.3,	6.0773
83		0.2,	0.0,	24.0,	
	7290.5,		3584.8,	1655.7,	8.2264
84		0.2,	0.0,	26.0,	
	9344.4,		4050.6,	2168.2,	10.048
85		0.2,	0.0,	30.0,	
	13714.4,		4891.5,	3335.6,	14.1832
86		0.2,	0.0,	34.0,	
	17928.1,		5575.9,	4564.4,	17.1365
87		0.2,	0.0,	38.0,	
	22048.5,		6167.1,	5839.6,	19.6518
88		0.2,	0.0,	42.0,	
	26104.0,		6693.4,	7176.2,	31.254
89		0.2,	0.0,	46.0,	
	30105.5,		7165.7,	8625.1,	60.8012
90		0.2,	0.0,	48.0,	
	32088.4,		7383.6,	9408.5,	71.4541
91		0.2,	0.0,	50.0,	
	34059.1,		7590.1,	10231.7,	78.754
92		0.2,	2000.0,	21.0,	
	3705.8,		2475.9,	844.5,	4.8026
93		0.2,	2000.0,	22.0,	
	4773.5,		2805.8,	1055.1,	5.8928
94		0.2,	2000.0,	24.0,	
	6779.2,		3335.6,	1509.9,	8.0591
95		0.2,	2000.0,	26.0,	
	8688.2,		3768.8,	1978.1,	9.8731
96		0.2,	2000.0,	30.0,	
	12750.0,		4551.0,	3045.6,	14.0129
97		0.2,	2000.0,	34.0,	
	16665.9,		5187.3,	4175.2,	16.9893
98		0.2,	2000.0,	38.0,	
	20495.5,		5737.3,	5341.9,	19.5044
99		0.2,	2000.0,	42.0,	
	24264.1,		6226.1,	6575.1,	28.1727
100		0.2,	2000.0,	46.0,	
	27981.8,		6663.9,	7924.2,	59.5213
101		0.2,	2000.0,	48.0,	
	29823.9,		6866.3,	8646.0,	70.5775

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

102		0.2,	2000.0,		50.0,
	31655.3,		7058.3,	9403.9,	78.2786
103		0.2,	5000.0,		21.0,
	3315.0,		2214.7,	755.5,	6.435
104		0.2,	5000.0,		22.0,
	4270.4,		2510.0,	941.0,	5.268
105		0.2,	5000.0,		24.0,
	6064.9,		2984.3,	1342.0,	7.4149
106		0.2,	5000.0,		26.0,
	7773.0,		3372.1,	1755.4,	9.2124
107		0.2,	5000.0,		30.0,
	11407.0,		4072.2,	2696.9,	13.2256
108		0.2,	5000.0,		34.0,
	14910.5,		4641.7,	3693.1,	16.1681
109		0.2,	5000.0,		38.0,
	18336.7,		5134.0,	4722.6,	18.6548
110		0.2,	5000.0,		42.0,
	21708.3,		5571.5,	5810.0,	20.9007
111		0.2,	5000.0,		46.0,
	25034.4,		5963.4,	6999.7,	46.548
112		0.2,	5000.0,		48.0,
	26682.2,		6144.6,	7635.7,	60.7973
113		0.2,	5000.0,		50.0,
	28321.1,		6316.5,	8304.7,	71.4843
114		0.2,	10000.0,		21.0,
	2738.0,		1829.0,	626.4,	9.2804
115		0.2,	10000.0,		22.0,
	3527.6,		2073.3,	775.5,	6.4797
116		0.2,	10000.0,		24.0,
	5010.5,		2465.5,	1098.5,	6.2413
117		0.2,	10000.0,		26.0,
	6421.8,		2786.1,	1431.7,	7.9908
118		0.2,	10000.0,		30.0,
	9424.6,		3365.1,	2191.4,	11.7561
119		0.2,	10000.0,		34.0,
	12319.4,		3836.1,	2994.6,	14.6148
120		0.2,	10000.0,		38.0,
	15150.2,		4243.1,	3825.2,	17.0282
121		0.2,	10000.0,		42.0,
	17936.1,		4604.8,	4701.2,	19.1798

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

122		0.2 ,	10000.0 ,		46.0 ,
	20683.4 ,		4929.0 ,	5659.9 ,	23.6308
123		0.2 ,	10000.0 ,		48.0 ,
	22045.5 ,		5078.8 ,	6173.0 ,	36.4956
124		0.2 ,	10000.0 ,		50.0 ,
	23399.5 ,		5221.0 ,	6712.2 ,	53.4919
125		0.25 ,	0.0 ,		21.0 ,
	4982.9 ,		3711.0 ,	967.7 ,	5.1347
126		0.25 ,	0.0 ,		22.0 ,
	6155.9 ,		4120.9 ,	1221.5 ,	6.4157
127		0.25 ,	0.0 ,		24.0 ,
	8353.0 ,		4791.8 ,	1741.2 ,	8.5818
128		0.25 ,	0.0 ,		26.0 ,
	10434.6 ,		5347.2 ,	2267.6 ,	10.7481
129		0.25 ,	0.0 ,		30.0 ,
	14837.1 ,		6358.1 ,	3458.3 ,	14.5379
130		0.25 ,	0.0 ,		34.0 ,
	19055.8 ,		7185.2 ,	4700.4 ,	17.4532
131		0.25 ,	0.0 ,		38.0 ,
	23164.2 ,		7901.7 ,	5979.8 ,	19.9304
132		0.25 ,	0.0 ,		42.0 ,
	27194.4 ,		8540.4 ,	7318.7 ,	34.2788
133		0.25 ,	0.0 ,		46.0 ,
	31158.1 ,		9112.7 ,	8772.0 ,	62.9527
134		0.25 ,	0.0 ,		48.0 ,
	33119.2 ,		9377.6 ,	9547.4 ,	72.8167
135		0.25 ,	0.0 ,		50.0 ,
	35064.8 ,		9627.7 ,	10368.8 ,	79.61
136		0.25 ,	2000.0 ,		21.0 ,
	4635.4 ,		3453.6 ,	881.2 ,	4.9403
137		0.25 ,	2000.0 ,		22.0 ,
	5725.7 ,		3834.8 ,	1113.2 ,	6.2358
138		0.25 ,	2000.0 ,		24.0 ,
	7767.9 ,		4458.7 ,	1587.7 ,	8.4148
139		0.25 ,	2000.0 ,		26.0 ,
	9702.8 ,		4975.4 ,	2068.9 ,	10.3133
140		0.25 ,	2000.0 ,		30.0 ,
	13794.8 ,		5915.8 ,	3157.8 ,	14.3694
141		0.25 ,	2000.0 ,		34.0 ,
	17715.3 ,		6684.5 ,	4299.7 ,	17.3076

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

142		0.25 ,	2000.0 ,		38.0 ,
	21533.5 ,		7351.2 ,	5470.6 ,	19.7854
143		0.25 ,	2000.0 ,		42.0 ,
	25278.1 ,		7944.4 ,	6705.3 ,	30.7493
144		0.25 ,	2000.0 ,		46.0 ,
	28960.8 ,		8474.8 ,	8057.1 ,	61.504
145		0.25 ,	2000.0 ,		48.0 ,
	30782.4 ,		8720.7 ,	8773.3 ,	71.9783
146		0.25 ,	2000.0 ,		50.0 ,
	32590.3 ,		8953.2 ,	9529.4 ,	79.1712
147		0.25 ,	5000.0 ,		21.0 ,
	4146.8 ,		3089.4 ,	787.7 ,	5.8398
148		0.25 ,	5000.0 ,		22.0 ,
	5122.4 ,		3430.7 ,	992.0 ,	5.6074
149		0.25 ,	5000.0 ,		24.0 ,
	6949.9 ,		3989.3 ,	1411.0 ,	7.7697
150		0.25 ,	5000.0 ,		26.0 ,
	8681.0 ,		4451.7 ,	1835.5 ,	9.5548
151		0.25 ,	5000.0 ,		30.0 ,
	12342.2 ,		5293.4 ,	2795.6 ,	13.5758
152		0.25 ,	5000.0 ,		34.0 ,
	15850.1 ,		5981.6 ,	3803.0 ,	16.4816
153		0.25 ,	5000.0 ,		38.0 ,
	19266.4 ,		6578.4 ,	4836.6 ,	18.9321
154		0.25 ,	5000.0 ,		42.0 ,
	22617.1 ,		7109.4 ,	5925.2 ,	21.9946
155		0.25 ,	5000.0 ,		46.0 ,
	25911.5 ,		7584.2 ,	7117.3 ,	49.402
156		0.25 ,	5000.0 ,		48.0 ,
	27541.0 ,		7804.3 ,	7748.5 ,	62.5764
157		0.25 ,	5000.0 ,		50.0 ,
	29158.9 ,		8012.2 ,	8415.7 ,	72.7322
158		0.25 ,	10000.0 ,		21.0 ,
	3424.9 ,		2551.5 ,	652.1 ,	8.6939
159		0.25 ,	10000.0 ,		22.0 ,
	4231.3 ,		2833.9 ,	816.4 ,	5.6904
160		0.25 ,	10000.0 ,		24.0 ,
	5741.3 ,		3295.8 ,	1153.9 ,	6.5846
161		0.25 ,	10000.0 ,		26.0 ,
	7171.8 ,		3678.2 ,	1496.8 ,	8.3269

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

162		0.25 ,	10000.0 ,		30.0 ,
	10196.9 ,		4374.2 ,	2270.9 ,	12.0944
163		0.25 ,	10000.0 ,		34.0 ,
	13095.1 ,		4943.3 ,	3083.3 ,	14.918
164		0.25 ,	10000.0 ,		38.0 ,
	15917.5 ,		5436.7 ,	3916.9 ,	17.295
165		0.25 ,	10000.0 ,		42.0 ,
	18685.9 ,		5875.8 ,	4794.1 ,	19.4143
166		0.25 ,	10000.0 ,		46.0 ,
	21407.5 ,		6268.5 ,	5754.5 ,	25.0166
167		0.25 ,	10000.0 ,		48.0 ,
	22754.0 ,		6450.6 ,	6263.1 ,	38.8691
168		0.25 ,	10000.0 ,		50.0 ,
	24090.7 ,		6622.7 ,	6801.4 ,	55.311
169		0.3 ,	0.0 ,		21.0 ,
	6173.4 ,		4945.6 ,	1022.8 ,	5.4835
170		0.3 ,	0.0 ,		22.0 ,
	7364.1 ,		5399.7 ,	1289.1 ,	6.7761
171		0.3 ,	0.0 ,		24.0 ,
	9594.3 ,		6156.5 ,	1828.9 ,	8.945
172		0.3 ,	0.0 ,		26.0 ,
	11702.0 ,		6790.9 ,	2370.2 ,	11.3695
173		0.3 ,	0.0 ,		30.0 ,
	16141.2 ,		7956.0 ,	3586.7 ,	14.9079
174		0.3 ,	0.0 ,		34.0 ,
	20374.2 ,		8914.9 ,	4845.9 ,	17.7911
175		0.3 ,	0.0 ,		38.0 ,
	24482.0 ,		9748.6 ,	6136.4 ,	20.2415
176		0.3 ,	0.0 ,		42.0 ,
	28498.9 ,		10491.9 ,	7487.2 ,	38.1853
177		0.3 ,	0.0 ,		46.0 ,
	32440.2 ,		11158.6 ,	8946.6 ,	65.3539
178		0.3 ,	0.0 ,		48.0 ,
	34385.6 ,		11467.0 ,	9722.6 ,	74.4559
179		0.3 ,	0.0 ,		50.0 ,
	36314.3 ,		11758.7 ,	10541.1 ,	80.6075
180		0.3 ,	2000.0 ,		21.0 ,
	5743.4 ,		4602.6 ,	931.5 ,	5.2941
181		0.3 ,	2000.0 ,		22.0 ,
	6850.3 ,		5024.9 ,	1175.0 ,	6.6001

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PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

182		0.3 ,	2000.0 ,		24.0 ,	
	8923.2 ,		5728.8 ,	1668.1 ,		8.7823
183		0.3 ,	2000.0 ,		26.0 ,	
	10882.3 ,		6318.8 ,	2161.9 ,		11.0244
184		0.3 ,	2000.0 ,		30.0 ,	
	15008.5 ,		7402.8 ,	3275.4 ,		14.742
185		0.3 ,	2000.0 ,		34.0 ,	
	18942.1 ,		8294.0 ,	4433.1 ,		17.6473
186		0.3 ,	2000.0 ,		38.0 ,	
	22759.9 ,		9069.6 ,	5614.1 ,		20.0977
187		0.3 ,	2000.0 ,		42.0 ,	
	26492.4 ,		9759.9 ,	6860.5 ,		34.3047
188		0.3 ,	2000.0 ,		46.0 ,	
	30152.8 ,		10377.9 ,	8215.0 ,		63.8559
189		0.3 ,	2000.0 ,		48.0 ,	
	31959.4 ,		10663.8 ,	8934.3 ,		73.6791
190		0.3 ,	2000.0 ,		50.0 ,	
	33752.0 ,		10934.9 ,	9687.3 ,		80.2171
191		0.3 ,	5000.0 ,		21.0 ,	
	5137.9 ,		4117.3 ,	832.0 ,		5.0092
192		0.3 ,	5000.0 ,		22.0 ,	
	6128.4 ,		4495.5 ,	1046.5 ,		5.9682
193		0.3 ,	5000.0 ,		24.0 ,	
	7983.1 ,		5125.5 ,	1481.4 ,		8.1293
194		0.3 ,	5000.0 ,		26.0 ,	
	9735.9 ,		5653.8 ,	1917.6 ,		9.9046
195		0.3 ,	5000.0 ,		30.0 ,	
	13427.5 ,		6623.9 ,	2899.2 ,		13.9423
196		0.3 ,	5000.0 ,		34.0 ,	
	16946.8 ,		7421.7 ,	3920.4 ,		16.8161
197		0.3 ,	5000.0 ,		38.0 ,	
	20362.5 ,		8115.9 ,	4962.2 ,		19.2379
198		0.3 ,	5000.0 ,		42.0 ,	
	23701.7 ,		8733.8 ,	6061.4 ,		23.5209
199		0.3 ,	5000.0 ,		46.0 ,	
	26976.2 ,		9286.8 ,	7256.0 ,		52.5299
200		0.3 ,	5000.0 ,		48.0 ,	
	28592.9 ,		9543.0 ,	7890.1 ,		64.7543
201		0.3 ,	5000.0 ,		50.0 ,	
	30196.6 ,		9785.7 ,	8554.4 ,		74.2115

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

202		0.3 ,	10000.0 ,		21.0 ,	
	4243.8 ,		3400.8 ,	687.6 ,		7.8677
203		0.3 ,	10000.0 ,		22.0 ,	
	5062.5 ,		3713.6 ,	860.4 ,		4.908
204		0.3 ,	10000.0 ,		24.0 ,	
	6595.3 ,		4234.8 ,	1211.0 ,		6.9375
205		0.3 ,	10000.0 ,		26.0 ,	
	8043.8 ,		4671.6 ,	1563.1 ,		8.6667
206		0.3 ,	10000.0 ,		30.0 ,	
	11094.2 ,		5473.9 ,	2354.8 ,		12.4504
207		0.3 ,	10000.0 ,		34.0 ,	
	14002.0 ,		6133.6 ,	3177.8 ,		15.2398
208		0.3 ,	10000.0 ,		38.0 ,	
	16824.1 ,		6707.5 ,	4018.5 ,		17.5905
209		0.3 ,	10000.0 ,		42.0 ,	
	19583.3 ,		7218.6 ,	4904.6 ,		19.6927
210		0.3 ,	10000.0 ,		46.0 ,	
	22288.8 ,		7676.1 ,	5867.0 ,		26.9467
211		0.3 ,	10000.0 ,		48.0 ,	
	23624.2 ,		7887.9 ,	6378.4 ,		42.0826
212		0.3 ,	10000.0 ,		50.0 ,	
	24949.6 ,		8088.6 ,	6913.7 ,		57.381
213		0.3 ,	15000.0 ,		21.0 ,	
	3479.6 ,		2788.1 ,	567.1 ,		10.753
214		0.3 ,	15000.0 ,		22.0 ,	
	4151.5 ,		3045.2 ,	705.0 ,		7.7596
215		0.3 ,	15000.0 ,		24.0 ,	
	5409.3 ,		3473.3 ,	985.3 ,		5.6485
216		0.3 ,	15000.0 ,		26.0 ,	
	6597.7 ,		3831.9 ,	1267.2 ,		7.317
217		0.3 ,	15000.0 ,		30.0 ,	
	9100.3 ,		4490.8 ,	1900.3 ,		10.2364
218		0.3 ,	15000.0 ,		34.0 ,	
	11486.0 ,		5032.6 ,	2558.6 ,		13.4803
219		0.3 ,	15000.0 ,		38.0 ,	
	13801.0 ,		5503.8 ,	3231.5 ,		15.7326
220		0.3 ,	15000.0 ,		42.0 ,	
	16064.5 ,		5923.6 ,	3939.7 ,		17.7439
221		0.3 ,	15000.0 ,		46.0 ,	
	18284.0 ,		6299.3 ,	4708.7 ,		19.6831

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

222		0.3,	15000.0,		48.0,
	19379.7,		6473.2,	5117.8,	21.3254
223		0.3,	15000.0,		50.0,
	20466.5,		6637.9,	5546.1,	30.4095
224		0.35,	0.0,		21.0,
	7566.3,		6374.0,	1096.3,	5.9318
225		0.35,	0.0,		22.0,
	8770.7,		6863.1,	1379.4,	7.2407
226		0.35,	0.0,		24.0,
	11031.6,		7693.3,	1932.5,	9.3656
227		0.35,	0.0,		26.0,
	13168.6,		8399.6,	2472.9,	11.7648
228		0.35,	0.0,		30.0,
	17653.6,		9705.4,	3720.3,	15.2909
229		0.35,	0.0,		34.0,
	21914.4,		10786.9,	5002.2,	18.1525
230		0.35,	0.0,		38.0,
	26037.3,		11730.5,	6310.8,	20.5849
231		0.35,	0.0,		42.0,
	30057.1,		12571.0,	7691.3,	43.1208
232		0.35,	0.0,		46.0,
	33993.9,		13328.4,	9155.7,	67.9905
233		0.35,	0.0,		48.0,
	35932.2,		13677.3,	9939.7,	76.3155
234		0.35,	0.0,		50.0,
	37853.7,		14009.0,	10755.8,	81.718
235		0.35,	2000.0,		21.0,
	7039.8,		5932.0,	999.1,	5.7509
236		0.35,	2000.0,		22.0,
	8159.4,		6386.9,	1257.8,	7.0693
237		0.35,	2000.0,		24.0,
	10260.8,		7159.0,	1763.3,	9.2076
238		0.35,	2000.0,		26.0,
	12247.3,		7816.1,	2255.9,	11.5847
239		0.35,	2000.0,		30.0,
	16416.2,		9030.9,	3397.3,	15.1257
240		0.35,	2000.0,		34.0,
	20375.6,		10036.0,	4575.8,	18.0083
241		0.35,	2000.0,		38.0,
	24207.3,		10913.7,	5773.4,	20.4408

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

242		0.35,	2000.0,		42.0,
	27941.9,		11694.1,	7047.4,	39.005
243		0.35,	2000.0,		46.0,
	31598.2,		12396.5,	8403.2,	66.4441
244		0.35,	2000.0,		48.0,
	33398.3,		12719.4,	9133.8,	75.6132
245		0.35,	2000.0,		50.0,
	35183.5,		13027.6,	9884.0,	81.3882
246		0.35,	5000.0,		21.0,
	6297.7,		5306.8,	891.4,	5.1268
247		0.35,	5000.0,		22.0,
	7299.6,		5714.1,	1119.5,	6.4339
248		0.35,	5000.0,		24.0,
	9179.9,		6405.3,	1565.3,	8.5499
249		0.35,	5000.0,		26.0,
	10957.1,		6993.4,	2000.3,	10.2625
250		0.35,	5000.0,		30.0,
	14686.9,		8080.8,	3006.9,	14.3212
251		0.35,	5000.0,		34.0,
	18229.2,		8980.4,	4046.1,	17.1706
252		0.35,	5000.0,		38.0,
	21657.4,		9766.2,	5102.9,	19.5757
253		0.35,	5000.0,		42.0,
	24998.3,		10464.7,	6226.3,	25.9255
254		0.35,	5000.0,		46.0,
	28269.4,		11093.1,	7421.8,	55.8105
255		0.35,	5000.0,		48.0,
	29879.7,		11382.5,	8065.8,	67.2746
256		0.35,	5000.0,		50.0,
	31477.1,		11658.5,	8727.8,	75.9179
257		0.35,	10000.0,		21.0,
	5202.0,		4383.5,	735.2,	6.795
258		0.35,	10000.0,		22.0,
	6030.2,		4720.6,	919.0,	5.282
259		0.35,	10000.0,		24.0,
	7584.1,		5292.2,	1278.6,	7.346
260		0.35,	10000.0,		26.0,
	9052.7,		5778.6,	1629.9,	9.0072
261		0.35,	10000.0,		30.0,
	12134.6,		6677.8,	2441.6,	12.816

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

262		0.35,	10000.0,		34.0,
	15061.4,		7421.8,	3279.3,	15.5823
263		0.35,	10000.0,		38.0,
	17893.8,		8071.6,	4132.1,	17.9157
264		0.35,	10000.0,		42.0,
	20654.1,		8649.1,	5037.3,	20.0235
265		0.35,	10000.0,		46.0,
	23357.0,		9169.2,	6000.8,	29.5981
266		0.35,	10000.0,		48.0,
	24688.2,		9408.4,	6520.4,	45.9418
267		0.35,	10000.0,		50.0,
	26007.2,		9636.6,	7053.3,	59.5544
268		0.35,	15000.0,		21.0,
	4265.5,		3594.1,	604.8,	9.6899
269		0.35,	15000.0,		22.0,
	4945.3,		3871.2,	751.6,	6.6744
270		0.35,	15000.0,		24.0,
	6220.4,		4340.7,	1039.2,	6.0427
271		0.35,	15000.0,		26.0,
	7425.3,		4740.1,	1320.6,	7.6429
272		0.35,	15000.0,		30.0,
	9953.9,		5478.5,	1969.8,	10.8708
273		0.35,	15000.0,		34.0,
	12355.2,		6089.6,	2639.9,	13.8065
274		0.35,	15000.0,		38.0,
	14678.8,		6623.1,	3322.2,	16.0412
275		0.35,	15000.0,		42.0,
	16943.3,		7097.5,	4045.6,	18.0572
276		0.35,	15000.0,		46.0,
	19160.5,		7524.6,	4816.5,	19.9608
277		0.35,	15000.0,		48.0,
	20251.7,		7720.9,	5231.4,	22.6619
278		0.35,	15000.0,		50.0,
	21334.5,		7908.4,	5657.5,	33.1924
279		0.4,	2000.0,		21.0,
	8528.1,		7446.9,	1080.6,	6.2764
280		0.4,	2000.0,		22.0,
	9658.0,		7928.2,	1353.5,	7.5936
281		0.4,	2000.0,		24.0,
	11784.7,		8757.4,	1878.4,	9.7055

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

282		0.4 ,	2000.0 ,		26.0 ,
	13797.7 ,		9473.0 ,	2382.4 ,	12.1006
283		0.4 ,	2000.0 ,		30.0 ,
	18018.9 ,		10811.1 ,	3529.2 ,	15.5376
284		0.4 ,	2000.0 ,		34.0 ,
	22012.9 ,		11922.0 ,	4732.9 ,	18.4036
285		0.4 ,	2000.0 ,		38.0 ,
	25869.2 ,		12895.0 ,	5956.0 ,	20.8298
286		0.4 ,	2000.0 ,		42.0 ,
	29617.1 ,		13759.9 ,	7260.5 ,	44.5575
287		0.4 ,	2000.0 ,		46.0 ,
	33282.9 ,		14542.5 ,	8623.9 ,	69.2745
288		0.4 ,	2000.0 ,		48.0 ,
	35081.9 ,		14900.1 ,	9368.5 ,	77.6817
289		0.4 ,	2000.0 ,		50.0 ,
	36867.3 ,		15243.9 ,	10120.0 ,	82.6292
290		0.4 ,	5000.0 ,		21.0 ,
	7629.4 ,		6662.3 ,	963.1 ,	5.6477
291		0.4 ,	5000.0 ,		22.0 ,
	8640.5 ,		7093.1 ,	1203.9 ,	6.9524
292		0.4 ,	5000.0 ,		24.0 ,
	10543.4 ,		7835.5 ,	1666.8 ,	9.0427
293		0.4 ,	5000.0 ,		26.0 ,
	12344.4 ,		8476.0 ,	2111.2 ,	11.1881
294		0.4 ,	5000.0 ,		30.0 ,
	16121.1 ,		9673.7 ,	3123.3 ,	14.7282
295		0.4 ,	5000.0 ,		34.0 ,
	19694.5 ,		10668.0 ,	4184.8 ,	17.5597
296		0.4 ,	5000.0 ,		38.0 ,
	23144.4 ,		11539.2 ,	5263.3 ,	19.9572
297		0.4 ,	5000.0 ,		42.0 ,
	26497.4 ,		12313.3 ,	6414.0 ,	29.514
298		0.4 ,	5000.0 ,		46.0 ,
	29777.0 ,		13014.0 ,	7616.7 ,	59.0834
299		0.4 ,	5000.0 ,		48.0 ,
	31386.7 ,		13333.9 ,	8272.8 ,	70.033
300		0.4 ,	5000.0 ,		50.0 ,
	32983.8 ,		13641.9 ,	8936.1 ,	77.8099
301		0.4 ,	10000.0 ,		21.0 ,
	6302.4 ,		5503.6 ,	792.8 ,	5.5515

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

302		0.4,	10000.0,		22.0,
	7138.3,		5860.2,	987.2,	5.7899
303		0.4,	10000.0,		24.0,
	8710.6,		6473.9,	1360.1,	7.8236
304		0.4,	10000.0,		26.0,
	10198.9,		7003.7,	1718.7,	9.4457
305		0.4,	10000.0,		30.0,
	13319.7,		7994.3,	2535.4,	13.2086
306		0.4,	10000.0,		34.0,
	16272.3,		8816.6,	3391.4,	15.9573
307		0.4,	10000.0,		38.0,
	19122.7,		9537.0,	4262.0,	18.2845
308		0.4,	10000.0,		42.0,
	21893.2,		10177.2,	5188.5,	20.3954
309		0.4,	10000.0,		46.0,
	24602.9,		10756.8,	6158.4,	33.2437
310		0.4,	10000.0,		48.0,
	25932.9,		11021.4,	6687.2,	50.2607
311		0.4,	10000.0,		50.0,
	27252.3,		11276.0,	7221.2,	62.3136
312		0.4,	15000.0,		21.0,
	5168.0,		4512.9,	650.8,	8.4556
313		0.4,	15000.0,		22.0,
	5854.1,		4806.0,	806.0,	5.4657
314		0.4,	15000.0,		24.0,
	7144.6,		5310.3,	1104.8,	6.507
315		0.4,	15000.0,		26.0,
	8365.6,		5745.3,	1391.4,	8.064
316		0.4,	15000.0,		30.0,
	10925.8,		6558.6,	2044.8,	11.5264
317		0.4,	15000.0,		34.0,
	13348.1,		7234.0,	2729.6,	14.1632
318		0.4,	15000.0,		38.0,
	15686.6,		7825.6,	3426.3,	16.3919
319		0.4,	15000.0,		42.0,
	17959.2,		8351.4,	4166.5,	18.4104
320		0.4,	15000.0,		46.0,
	20182.2,		8827.3,	4942.1,	20.2805
321		0.4,	15000.0,		48.0,
	21272.7,		9044.6,	5364.6,	24.6069

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

322		0.4,	15000.0,	50.0,	
	22355.5,		9253.8,	5792.4,	36.8914
323		0.4,	20000.0,	21.0,	
	4204.2,		3671.1,	533.0,	11.3443
324		0.4,	20000.0,	22.0,	
	4763.2,		3910.2,	655.9,	8.3987
325		0.4,	20000.0,	24.0,	
	5814.2,		4321.4,	892.7,	5.1322
326		0.4,	20000.0,	26.0,	
	6808.5,		4676.0,	1119.9,	6.6187
327		0.4,	20000.0,	30.0,	
	8893.2,		5339.0,	1638.7,	9.2928
328		0.4,	20000.0,	34.0,	
	10865.4,		5889.5,	2181.2,	12.2577
329		0.4,	20000.0,	38.0,	
	12769.1,		6371.6,	2734.1,	14.3697
330		0.4,	20000.0,	42.0,	
	14619.4,		6800.2,	3321.2,	16.2797
331		0.4,	20000.0,	46.0,	
	16429.0,		7188.1,	3935.2,	18.0475
332		0.4,	20000.0,	48.0,	
	17317.4,		7365.4,	4270.7,	18.9554
333		0.4,	20000.0,	50.0,	
	18198.2,		7535.7,	4608.9,	19.8172
334		0.45,	5000.0,	21.0,	
	9134.3,		8186.4,	1052.9,	6.2594
335		0.45,	5000.0,	22.0,	
	10153.5,		8637.0,	1297.4,	7.5048
336		0.45,	5000.0,	24.0,	
	12077.2,		9423.1,	1777.2,	9.5637
337		0.45,	5000.0,	26.0,	
	13900.8,		10109.4,	2237.9,	11.8951
338		0.45,	5000.0,	30.0,	
	17726.1,		11407.1,	3263.8,	15.2102
339		0.45,	5000.0,	34.0,	
	21336.8,		12490.1,	4347.5,	18.0093
340		0.45,	5000.0,	38.0,	
	24813.0,		13438.6,	5462.2,	20.4201
341		0.45,	5000.0,	42.0,	
	28188.8,		14287.0,	6626.4,	34.5899

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

342		0.45 ,	5000.0 ,		46.0 ,
	31486.0 ,		15056.3 ,	7841.9 ,	62.5039
343		0.45 ,	5000.0 ,		48.0 ,
	33098.2 ,		15405.0 ,	8512.7 ,	72.9747
344		0.45 ,	5000.0 ,		50.0 ,
	34700.2 ,		15743.1 ,	9179.8 ,	79.8154
345		0.45 ,	10000.0 ,		21.0 ,
	7545.9 ,		6763.0 ,	865.0 ,	5.1128
346		0.45 ,	10000.0 ,		22.0 ,
	8388.6 ,		7135.9 ,	1062.6 ,	6.3291
347		0.45 ,	10000.0 ,		24.0 ,
	9978.2 ,		7786.1 ,	1449.5 ,	8.3334
348		0.45 ,	10000.0 ,		26.0 ,
	11485.1 ,		8353.6 ,	1820.8 ,	9.9346
349		0.45 ,	10000.0 ,		30.0 ,
	14645.9 ,		9426.7 ,	2648.1 ,	13.6721
350		0.45 ,	10000.0 ,		34.0 ,
	17629.4 ,		10322.5 ,	3522.4 ,	16.3907
351		0.45 ,	10000.0 ,		38.0 ,
	20501.5 ,		11106.9 ,	4421.5 ,	18.7295
352		0.45 ,	10000.0 ,		42.0 ,
	23290.9 ,		11808.7 ,	5360.6 ,	20.8118
353		0.45 ,	10000.0 ,		46.0 ,
	26014.7 ,		12444.7 ,	6339.6 ,	38.0177
354		0.45 ,	10000.0 ,		48.0 ,
	27346.9 ,		12733.1 ,	6880.0 ,	54.809
355		0.45 ,	10000.0 ,		50.0 ,
	28670.6 ,		13012.9 ,	7417.8 ,	65.5452
356		0.45 ,	15000.0 ,		21.0 ,
	6188.1 ,		5546.1 ,	708.2 ,	7.0161
357		0.45 ,	15000.0 ,		22.0 ,
	6879.8 ,		5852.6 ,	866.3 ,	5.0623
358		0.45 ,	15000.0 ,		24.0 ,
	8184.3 ,		6386.7 ,	1176.1 ,	6.9948
359		0.45 ,	15000.0 ,		26.0 ,
	9420.7 ,		6852.7 ,	1473.1 ,	8.533
360		0.45 ,	15000.0 ,		30.0 ,
	12014.0 ,		7734.1 ,	2135.7 ,	11.9737
361		0.45 ,	15000.0 ,		34.0 ,
	14461.5 ,		8469.7 ,	2834.4 ,	14.5758

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

362		0.45 ,	15000.0 ,		38.0 ,
	16817.6 ,		9113.8 ,	3553.9 ,	16.8157
363		0.45 ,	15000.0 ,		42.0 ,
	19105.8 ,		9690.3 ,	4304.2 ,	18.8064
364		0.45 ,	15000.0 ,		46.0 ,
	21340.5 ,		10212.6 ,	5087.2 ,	20.6468
365		0.45 ,	15000.0 ,		48.0 ,
	22433.2 ,		10449.4 ,	5519.7 ,	27.6021
366		0.45 ,	15000.0 ,		50.0 ,
	23518.8 ,		10679.1 ,	5949.6 ,	41.4721
367		0.45 ,	20000.0 ,		21.0 ,
	5034.5 ,		4512.0 ,	578.2 ,	9.9201
368		0.45 ,	20000.0 ,		22.0 ,
	5598.0 ,		4762.1 ,	703.5 ,	7.1405
369		0.45 ,	20000.0 ,		24.0 ,
	6660.5 ,		5197.7 ,	949.2 ,	5.5997
370		0.45 ,	20000.0 ,		26.0 ,
	7667.4 ,		5577.6 ,	1184.8 ,	7.0642
371		0.45 ,	20000.0 ,		30.0 ,
	9779.0 ,		6296.0 ,	1710.7 ,	9.6704
372		0.45 ,	20000.0 ,		34.0 ,
	11771.9 ,		6895.7 ,	2264.6 ,	12.6477
373		0.45 ,	20000.0 ,		38.0 ,
	13690.0 ,		7420.5 ,	2835.3 ,	14.7686
374		0.45 ,	20000.0 ,		42.0 ,
	15553.0 ,		7890.4 ,	3430.4 ,	16.6516
375		0.45 ,	20000.0 ,		46.0 ,
	17372.0 ,		8316.2 ,	4051.2 ,	18.3923
376		0.45 ,	20000.0 ,		48.0 ,
	18261.9 ,		8509.5 ,	4393.4 ,	19.298
377		0.45 ,	20000.0 ,		50.0 ,
	19145.4 ,		8696.4 ,	4733.9 ,	20.4806
378		0.45 ,	25000.0 ,		21.0 ,
	4060.5 ,		3638.9 ,	471.3 ,	12.8242
379		0.45 ,	25000.0 ,		22.0 ,
	4515.9 ,		3841.4 ,	569.7 ,	10.0682
380		0.45 ,	25000.0 ,		24.0 ,
	5374.3 ,		4193.9 ,	762.8 ,	5.6593
381		0.45 ,	25000.0 ,		26.0 ,
	6187.3 ,		4501.0 ,	947.5 ,	5.5964

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

382		0.45 ,	25000.0 ,		30.0 ,	
	7892.2 ,		5081.8 ,	1360.8 ,		8.0513
383		0.45 ,	25000.0 ,		34.0 ,	
	9501.3 ,		5566.7 ,	1795.6 ,		10.5022
384		0.45 ,	25000.0 ,		38.0 ,	
	11049.7 ,		5991.0 ,	2244.5 ,		12.7089
385		0.45 ,	25000.0 ,		42.0 ,	
	12553.9 ,		6370.9 ,	2711.4 ,		14.4744
386		0.45 ,	25000.0 ,		46.0 ,	
	14022.2 ,		6715.2 ,	3198.7 ,		16.1089
387		0.45 ,	25000.0 ,		48.0 ,	
	14740.5 ,		6871.3 ,	3466.7 ,		16.9602
388		0.45 ,	25000.0 ,		50.0 ,	
	15453.9 ,		7022.7 ,	3734.8 ,		17.7627
389		0.5 ,	10000.0 ,		21.0 ,	
	8935.3 ,		8163.6 ,	961.2 ,		5.8415
390		0.5 ,	10000.0 ,		22.0 ,	
	9784.6 ,		8549.9 ,	1163.5 ,		6.9976
391		0.5 ,	10000.0 ,		24.0 ,	
	11396.5 ,		9235.8 ,	1543.3 ,		8.8511
392		0.5 ,	10000.0 ,		26.0 ,	
	12924.7 ,		9838.0 ,	1929.2 ,		10.5792
393		0.5 ,	10000.0 ,		30.0 ,	
	16130.8 ,		10986.4 ,	2783.0 ,		14.2064
394		0.5 ,	10000.0 ,		34.0 ,	
	19153.1 ,		11950.9 ,	3679.1 ,		16.8955
395		0.5 ,	10000.0 ,		38.0 ,	
	22058.2 ,		12798.3 ,	4602.1 ,		19.2194
396		0.5 ,	10000.0 ,		42.0 ,	
	24877.3 ,		13559.7 ,	5557.3 ,		21.8787
397		0.5 ,	10000.0 ,		46.0 ,	
	27624.5 ,		14249.1 ,	6554.3 ,		44.2213
398		0.5 ,	10000.0 ,		48.0 ,	
	28965.7 ,		14561.4 ,	7104.9 ,		59.1261
399		0.5 ,	10000.0 ,		50.0 ,	
	30298.2 ,		14865.0 ,	7650.4 ,		69.0476
400		0.5 ,	15000.0 ,		21.0 ,	
	7328.1 ,		6695.3 ,	785.0 ,		5.2669
401		0.5 ,	15000.0 ,		22.0 ,	
	8025.5 ,		7012.9 ,	947.3 ,		5.7106

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

402		0.5 ,	15000.0 ,		24.0 ,	
	9348.0 ,		7576.1 ,	1250.9 ,		7.4914
403		0.5 ,	15000.0 ,		26.0 ,	
	10602.1 ,		8070.9 ,	1560.0 ,		9.017
404		0.5 ,	15000.0 ,		30.0 ,	
	13232.8 ,		9014.0 ,	2243.0 ,		12.4829
405		0.5 ,	15000.0 ,		34.0 ,	
	15712.4 ,		9806.1 ,	2959.9 ,		15.0577
406		0.5 ,	15000.0 ,		38.0 ,	
	18095.8 ,		10502.0 ,	3698.5 ,		17.2835
407		0.5 ,	15000.0 ,		42.0 ,	
	20408.6 ,		11127.3 ,	4462.3 ,		19.2512
408		0.5 ,	15000.0 ,		46.0 ,	
	22662.5 ,		11693.7 ,	5260.4 ,		22.1856
409		0.5 ,	15000.0 ,		48.0 ,	
	23762.9 ,		11950.1 ,	5699.8 ,		31.922
410		0.5 ,	15000.0 ,		50.0 ,	
	24855.4 ,		12199.1 ,	6135.5 ,		46.874
411		0.5 ,	20000.0 ,		21.0 ,	
	5962.3 ,		5447.4 ,	638.9 ,		8.1949
412		0.5 ,	20000.0 ,		22.0 ,	
	6530.4 ,		5706.6 ,	767.5 ,		5.5864
413		0.5 ,	20000.0 ,		24.0 ,	
	7607.5 ,		6165.9 ,	1008.8 ,		6.0754
414		0.5 ,	20000.0 ,		26.0 ,	
	8628.5 ,		6569.1 ,	1253.7 ,		7.5239
415		0.5 ,	20000.0 ,		30.0 ,	
	10770.3 ,		7337.8 ,	1795.3 ,		10.1237
416		0.5 ,	20000.0 ,		34.0 ,	
	12788.9 ,		7983.4 ,	2363.9 ,		13.1017
417		0.5 ,	20000.0 ,		38.0 ,	
	14729.0 ,		8550.6 ,	2949.4 ,		15.2078
418		0.5 ,	20000.0 ,		42.0 ,	
	16611.6 ,		9060.2 ,	3555.1 ,		17.0676
419		0.5 ,	20000.0 ,		46.0 ,	
	18446.0 ,		9521.6 ,	4187.2 ,		18.7919
420		0.5 ,	20000.0 ,		48.0 ,	
	19341.8 ,		9731.0 ,	4535.0 ,		19.685
421		0.5 ,	20000.0 ,		50.0 ,	
	20231.5 ,		9934.1 ,	4880.0 ,		22.2565

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

422		0.5 ,	25000.0 ,		21.0 ,
	4809.4 ,		4393.9 ,	518.7 ,	11.1067
423		0.5 ,	25000.0 ,		22.0 ,
	5268.5 ,		4603.8 ,	619.7 ,	8.5392
424		0.5 ,	25000.0 ,		24.0 ,
	6138.4 ,		4975.2 ,	809.4 ,	4.6585
425		0.5 ,	25000.0 ,		26.0 ,
	6963.0 ,		5301.2 ,	1001.5 ,	6.0297
426		0.5 ,	25000.0 ,		30.0 ,
	8692.6 ,		5923.0 ,	1426.9 ,	8.4555
427		0.5 ,	25000.0 ,		34.0 ,
	10322.4 ,		6444.9 ,	1873.7 ,	11.1348
428		0.5 ,	25000.0 ,		38.0 ,
	11888.8 ,		6903.5 ,	2334.1 ,	13.1197
429		0.5 ,	25000.0 ,		42.0 ,
	13408.7 ,		7315.6 ,	2809.6 ,	14.8632
430		0.5 ,	25000.0 ,		46.0 ,
	14889.7 ,		7688.8 ,	3305.8 ,	16.4821
431		0.5 ,	25000.0 ,		48.0 ,
	15612.7 ,		7857.9 ,	3578.7 ,	17.3225
432		0.5 ,	25000.0 ,		50.0 ,
	16331.0 ,		8022.2 ,	3850.1 ,	18.1143
433		0.55 ,	10000.0 ,		21.0 ,
	10473.2 ,		9708.0 ,	1063.1 ,	6.5663
434		0.55 ,	10000.0 ,		22.0 ,
	11331.3 ,		10107.0 ,	1273.2 ,	7.684
435		0.55 ,	10000.0 ,		24.0 ,
	12968.8 ,		10826.2 ,	1651.6 ,	9.4227
436		0.55 ,	10000.0 ,		26.0 ,
	14524.0 ,		11463.2 ,	2046.0 ,	11.6154
437		0.55 ,	10000.0 ,		30.0 ,
	17784.6 ,		12683.1 ,	2929.7 ,	14.7724
438		0.55 ,	10000.0 ,		34.0 ,
	20855.7 ,		13713.6 ,	3852.5 ,	17.4405
439		0.55 ,	10000.0 ,		38.0 ,
	23804.1 ,		14621.6 ,	4806.1 ,	19.7586
440		0.55 ,	10000.0 ,		42.0 ,
	26664.3 ,		15441.0 ,	5782.5 ,	24.8341
441		0.55 ,	10000.0 ,		46.0 ,
	29445.2 ,		16181.5 ,	6806.8 ,	51.3216

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

442		0.55,	10000.0,		48.0,
	30801.6,		16517.7,	7366.0,	63.4873
443		0.55,	10000.0,		50.0,
	32151.3,		16847.1,	7921.7,	72.7201
444		0.55,	15000.0,		21.0,
	8589.7,		7962.3,	866.4,	5.2947
445		0.55,	15000.0,		22.0,
	9294.1,		8290.2,	1034.6,	6.3704
446		0.55,	15000.0,		24.0,
	10637.7,		8880.9,	1337.3,	8.0399
447		0.55,	15000.0,		26.0,
	11913.6,		9404.0,	1653.0,	9.52
448		0.55,	15000.0,		30.0,
	14588.5,		10405.8,	2359.7,	13.0203
449		0.55,	15000.0,		34.0,
	17108.0,		11252.3,	3098.8,	15.5778
450		0.55,	15000.0,		38.0,
	19526.7,		11997.8,	3861.4,	17.7957
451		0.55,	15000.0,		42.0,
	21872.4,		12670.6,	4642.0,	19.7451
452		0.55,	15000.0,		46.0,
	24153.7,		13278.7,	5460.9,	25.1739
453		0.55,	15000.0,		48.0,
	25266.4,		13555.1,	5907.7,	37.7816
454		0.55,	15000.0,		50.0,
	26373.7,		13825.7,	6352.0,	52.6518
455		0.55,	20000.0,		21.0,
	6989.4,		6479.0,	703.3,	6.503
456		0.55,	20000.0,		22.0,
	7563.3,		6746.5,	837.0,	5.0064
457		0.55,	20000.0,		24.0,
	8657.4,		7228.1,	1077.2,	6.5972
458		0.55,	20000.0,		26.0,
	9696.4,		7654.5,	1327.5,	8.0013
459		0.55,	20000.0,		30.0,
	11874.4,		8471.2,	1888.0,	11.0514
460		0.55,	20000.0,		34.0,
	13925.6,		9161.1,	2474.4,	13.5941
461		0.55,	20000.0,		38.0,
	15894.5,		9768.8,	3078.5,	15.69

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

462		0.55 ,	20000.0 ,		42.0 ,
	17804.3 ,		10317.3 ,	3698.0 ,	17.5325
463		0.55 ,	20000.0 ,		46.0 ,
	19661.3 ,		10813.0 ,	4347.4 ,	19.2513
464		0.55 ,	20000.0 ,		48.0 ,
	20567.3 ,		11038.3 ,	4701.1 ,	20.1286
465		0.55 ,	20000.0 ,		50.0 ,
	21468.4 ,		11258.8 ,	5053.1 ,	25.1535
466		0.55 ,	25000.0 ,		21.0 ,
	5638.5 ,		5226.6 ,	569.1 ,	9.4348
467		0.55 ,	25000.0 ,		22.0 ,
	6102.2 ,		5443.2 ,	674.2 ,	6.9986
468		0.55 ,	25000.0 ,		24.0 ,
	6985.9 ,		5832.7 ,	863.0 ,	5.1538
469		0.55 ,	25000.0 ,		26.0 ,
	7825.0 ,		6177.5 ,	1059.5 ,	6.4814
470		0.55 ,	25000.0 ,		30.0 ,
	9583.8 ,		6838.0 ,	1499.7 ,	8.8813
471		0.55 ,	25000.0 ,		34.0 ,
	11240.1 ,		7395.8 ,	1960.8 ,	11.5975
472		0.55 ,	25000.0 ,		38.0 ,
	12829.7 ,		7887.1 ,	2435.5 ,	13.5701
473		0.55 ,	25000.0 ,		42.0 ,
	14371.4 ,		8330.6 ,	2922.0 ,	15.2974
474		0.55 ,	25000.0 ,		46.0 ,
	15870.7 ,		8731.4 ,	3431.6 ,	16.9093
475		0.55 ,	25000.0 ,		48.0 ,
	16601.9 ,		8913.6 ,	3708.9 ,	17.7331
476		0.55 ,	25000.0 ,		50.0 ,
	17329.5 ,		9092.0 ,	3985.6 ,	18.5183
477		0.55 ,	30000.0 ,		21.0 ,
	4506.0 ,		4176.6 ,	459.6 ,	12.3646
478		0.55 ,	30000.0 ,		22.0 ,
	4877.6 ,		4350.6 ,	541.3 ,	9.9465
479		0.55 ,	30000.0 ,		24.0 ,
	5585.4 ,		4663.2 ,	688.6 ,	6.3459
480		0.55 ,	30000.0 ,		26.0 ,
	6257.1 ,		4939.6 ,	841.1 ,	4.9951
481		0.55 ,	30000.0 ,		30.0 ,
	7665.1 ,		5469.3 ,	1183.3 ,	7.2442

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

482		0.55 ,	30000.0 ,		34.0 ,
	8990.5 ,		5916.4 ,	1541.7 ,	9.1534
483		0.55 ,	30000.0 ,		38.0 ,
	10262.7 ,		6310.2 ,	1910.9 ,	11.4896
484		0.55 ,	30000.0 ,		42.0 ,
	11496.3 ,		6665.6 ,	2289.2 ,	13.1001
485		0.55 ,	30000.0 ,		46.0 ,
	12696.1 ,		6986.9 ,	2685.7 ,	14.6049
486		0.55 ,	30000.0 ,		48.0 ,
	13281.5 ,		7133.2 ,	2900.4 ,	15.3716
487		0.55 ,	30000.0 ,		50.0 ,
	13863.3 ,		7275.8 ,	3114.4 ,	16.1055
488		0.6 ,	15000.0 ,		21.0 ,
	9973.8 ,		9348.2 ,	950.5 ,	5.9783
489		0.6 ,	15000.0 ,		22.0 ,
	10687.7 ,		9686.8 ,	1124.3 ,	7.0163
490		0.6 ,	15000.0 ,		24.0 ,
	12054.5 ,		10302.9 ,	1438.6 ,	8.6443
491		0.6 ,	15000.0 ,		26.0 ,
	13357.4 ,		10855.1 ,	1754.7 ,	10.0484
492		0.6 ,	15000.0 ,		30.0 ,
	16084.8 ,		11914.4 ,	2488.5 ,	13.592
493		0.6 ,	15000.0 ,		34.0 ,
	18652.7 ,		12814.1 ,	3252.5 ,	16.1377
494		0.6 ,	15000.0 ,		38.0 ,
	21114.4 ,		13607.6 ,	4042.6 ,	18.3508
495		0.6 ,	15000.0 ,		42.0 ,
	23501.9 ,		14327.1 ,	4845.2 ,	20.2894
496		0.6 ,	15000.0 ,		46.0 ,
	25820.8 ,		14977.7 ,	5688.9 ,	30.203
497		0.6 ,	15000.0 ,		48.0 ,
	26957.4 ,		15280.2 ,	6143.4 ,	44.8334
498		0.6 ,	15000.0 ,		50.0 ,
	28089.5 ,		15578.2 ,	6600.6 ,	58.0636
499		0.6 ,	20000.0 ,		21.0 ,
	8116.3 ,		7607.3 ,	769.9 ,	4.8739
500		0.6 ,	20000.0 ,		22.0 ,
	8697.8 ,		7883.4 ,	907.9 ,	5.6219
501		0.6 ,	20000.0 ,		24.0 ,
	9810.9 ,		8385.7 ,	1157.0 ,	7.1692

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

502		0.6 ,	20000.0 ,		26.0 ,
	10872.0 ,		8836.1 ,	1408.5 ,	8.504
503		0.6 ,	20000.0 ,		30.0 ,
	13092.7 ,		9699.5 ,	1989.8 ,	11.7084
504		0.6 ,	20000.0 ,		34.0 ,
	15183.5 ,		10432.9 ,	2596.5 ,	14.1211
505		0.6 ,	20000.0 ,		38.0 ,
	17187.7 ,		11079.9 ,	3223.0 ,	16.2145
506		0.6 ,	20000.0 ,		42.0 ,
	19131.3 ,		11666.4 ,	3858.8 ,	18.0426
507		0.6 ,	20000.0 ,		46.0 ,
	21019.2 ,		12196.8 ,	4528.3 ,	19.7561
508		0.6 ,	20000.0 ,		48.0 ,
	21944.6 ,		12443.4 ,	4888.4 ,	21.6513
509		0.6 ,	20000.0 ,		50.0 ,
	22865.7 ,		12685.9 ,	5250.5 ,	29.7394
510		0.6 ,	25000.0 ,		21.0 ,
	6548.0 ,		6137.4 ,	621.3 ,	7.8343
511		0.6 ,	25000.0 ,		22.0 ,
	7018.0 ,		6361.0 ,	730.0 ,	5.5192
512		0.6 ,	25000.0 ,		24.0 ,
	7917.0 ,		6767.3 ,	925.6 ,	5.6982
513		0.6 ,	25000.0 ,		26.0 ,
	8773.7 ,		7131.3 ,	1123.2 ,	6.9559
514		0.6 ,	25000.0 ,		30.0 ,
	10567.1 ,		7829.7 ,	1580.2 ,	9.3365
515		0.6 ,	25000.0 ,		34.0 ,
	12254.9 ,		8422.5 ,	2056.4 ,	12.09
516		0.6 ,	25000.0 ,		38.0 ,
	13872.9 ,		8945.6 ,	2548.6 ,	14.0586
517		0.6 ,	25000.0 ,		42.0 ,
	15441.9 ,		9419.5 ,	3048.5 ,	15.7736
518		0.6 ,	25000.0 ,		46.0 ,
	16965.8 ,		9848.6 ,	3573.0 ,	17.3772
519		0.6 ,	25000.0 ,		48.0 ,
	17712.8 ,		10048.1 ,	3855.9 ,	18.1848
520		0.6 ,	25000.0 ,		50.0 ,
	18456.6 ,		10244.4 ,	4140.2 ,	18.9671
521		0.6 ,	30000.0 ,		21.0 ,
	5233.4 ,		4905.1 ,	500.0 ,	10.771

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

522		0.6 ,	30000.0 ,	22.0 ,	
	5610.0 ,		5084.7 ,	584.6 ,	8.4942
523		0.6 ,	30000.0 ,	24.0 ,	
	6329.9 ,		5410.6 ,	736.4 ,	5.0619
524		0.6 ,	30000.0 ,	26.0 ,	
	7015.7 ,		5702.4 ,	890.5 ,	5.441
525		0.6 ,	30000.0 ,	30.0 ,	
	8451.2 ,		6262.4 ,	1245.5 ,	7.6673
526		0.6 ,	30000.0 ,	34.0 ,	
	9802.1 ,		6737.8 ,	1616.1 ,	9.6371
527		0.6 ,	30000.0 ,	38.0 ,	
	11096.9 ,		7157.0 ,	1998.7 ,	11.9431
528		0.6 ,	30000.0 ,	42.0 ,	
	12352.3 ,		7536.9 ,	2387.5 ,	13.542
529		0.6 ,	30000.0 ,	46.0 ,	
	13571.6 ,		7880.7 ,	2795.9 ,	15.0403
530		0.6 ,	30000.0 ,	48.0 ,	
	14169.7 ,		8041.0 ,	3014.6 ,	15.7897
531		0.6 ,	30000.0 ,	50.0 ,	
	14764.6 ,		8198.1 ,	3235.5 ,	16.5238
532		0.6 ,	35000.0 ,	21.0 ,	
	4139.6 ,		3879.7 ,	401.9 ,	13.7651
533		0.6 ,	35000.0 ,	22.0 ,	
	4438.7 ,		4022.7 ,	467.0 ,	11.4717
534		0.6 ,	35000.0 ,	24.0 ,	
	5009.8 ,		4281.9 ,	583.8 ,	8.0866
535		0.6 ,	35000.0 ,	26.0 ,	
	5553.5 ,		4513.7 ,	702.3 ,	5.2844
536		0.6 ,	35000.0 ,	30.0 ,	
	6691.7 ,		4958.7 ,	975.1 ,	6.0676
537		0.6 ,	35000.0 ,	34.0 ,	
	7762.5 ,		5336.2 ,	1259.8 ,	7.8379
538		0.6 ,	35000.0 ,	38.0 ,	
	8788.5 ,		5669.1 ,	1553.9 ,	9.6313
539		0.6 ,	35000.0 ,	42.0 ,	
	9783.3 ,		5970.6 ,	1853.8 ,	11.4063
540		0.6 ,	35000.0 ,	46.0 ,	
	10749.7 ,		6243.7 ,	2167.6 ,	12.7926
541		0.6 ,	35000.0 ,	48.0 ,	
	11223.1 ,		6370.7 ,	2335.6 ,	13.4895

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

542		0.6 ,	35000.0 ,		50.0 ,
	11695.0 ,		6496.0 ,	2504.7 ,	14.1725
543		0.6 ,	37000.0 ,		21.0 ,
	3758.1 ,		3522.0 ,	370.0 ,	14.2083
544		0.6 ,	37000.0 ,		22.0 ,
	4030.2 ,		3652.4 ,	428.7 ,	11.9308
545		0.6 ,	37000.0 ,		24.0 ,
	4549.5 ,		3888.3 ,	534.1 ,	8.6067
546		0.6 ,	37000.0 ,		26.0 ,
	5043.7 ,		4099.0 ,	640.8 ,	5.8649
547		0.6 ,	37000.0 ,		30.0 ,
	6078.5 ,		4504.0 ,	886.9 ,	5.62
548		0.6 ,	37000.0 ,		34.0 ,
	7051.8 ,		4847.5 ,	1143.9 ,	7.3337
549		0.6 ,	37000.0 ,		38.0 ,
	7984.2 ,		5150.1 ,	1409.1 ,	8.8243
550		0.6 ,	37000.0 ,		42.0 ,
	8888.2 ,		5424.2 ,	1680.1 ,	10.7527
551		0.6 ,	37000.0 ,		46.0 ,
	9766.3 ,		5672.7 ,	1963.0 ,	12.0908
552		0.6 ,	37000.0 ,		48.0 ,
	10197.0 ,		5788.4 ,	2114.5 ,	12.7641
553		0.6 ,	37000.0 ,		50.0 ,
	10625.8 ,		5902.3 ,	2266.3 ,	13.4179
554		0.6 ,	39000.0 ,		21.0 ,
	3410.5 ,		3195.9 ,	342.8 ,	13.7365
555		0.6 ,	39000.0 ,		22.0 ,
	3658.1 ,		3314.8 ,	396.0 ,	11.5252
556		0.6 ,	39000.0 ,		24.0 ,
	4130.3 ,		3529.5 ,	491.6 ,	8.3235
557		0.6 ,	39000.0 ,		26.0 ,
	4579.5 ,		3721.3 ,	588.5 ,	5.6738
558		0.6 ,	39000.0 ,		30.0 ,
	5520.0 ,		4089.6 ,	811.7 ,	5.3948
559		0.6 ,	39000.0 ,		34.0 ,
	6404.7 ,		4402.1 ,	1044.8 ,	7.0416
560		0.6 ,	39000.0 ,		38.0 ,
	7251.9 ,		4677.1 ,	1285.7 ,	8.4753
561		0.6 ,	39000.0 ,		42.0 ,
	8073.2 ,		4926.2 ,	1532.0 ,	10.3344

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

562		0.6 ,	39000.0 ,		46.0 ,
	8871.3 ,		5152.2 ,	1788.5 ,	11.6188
563		0.6 ,	39000.0 ,		48.0 ,
	9262.7 ,		5257.5 ,	1925.9 ,	12.2647
564		0.6 ,	39000.0 ,		50.0 ,
	9652.5 ,		5361.2 ,	2063.4 ,	12.8882
565		0.6 ,	41000.0 ,		21.0 ,
	3094.4 ,		2899.4 ,	318.6 ,	13.295
566		0.6 ,	41000.0 ,		22.0 ,
	3320.0 ,		3008.0 ,	366.6 ,	11.1448
567		0.6 ,	41000.0 ,		24.0 ,
	3749.4 ,		3203.6 ,	453.0 ,	8.0632
568		0.6 ,	41000.0 ,		26.0 ,
	4157.8 ,		3378.0 ,	541.0 ,	5.5011
569		0.6 ,	41000.0 ,		30.0 ,
	5012.8 ,		3713.2 ,	743.4 ,	5.178
570		0.6 ,	41000.0 ,		34.0 ,
	5816.8 ,		3997.3 ,	954.9 ,	6.7566
571		0.6 ,	41000.0 ,		38.0 ,
	6586.8 ,		4247.5 ,	1173.9 ,	8.1404
572		0.6 ,	41000.0 ,		42.0 ,
	7333.1 ,		4473.9 ,	1397.5 ,	9.9298
573		0.6 ,	41000.0 ,		46.0 ,
	8058.4 ,		4679.4 ,	1630.2 ,	11.1649
574		0.6 ,	41000.0 ,		48.0 ,
	8414.1 ,		4775.2 ,	1754.8 ,	11.7844
575		0.6 ,	41000.0 ,		50.0 ,
	8768.5 ,		4869.7 ,	1878.9 ,	12.376
576		0.65 ,	15000.0 ,		21.0 ,
	11481.3 ,		10854.1 ,	1035.9 ,	6.6394
577		0.65 ,	15000.0 ,		22.0 ,
	12207.7 ,		11204.2 ,	1215.3 ,	7.6447
578		0.65 ,	15000.0 ,		24.0 ,
	13603.0 ,		11846.9 ,	1542.7 ,	9.2444
579		0.65 ,	15000.0 ,		26.0 ,
	14935.6 ,		12427.0 ,	1867.4 ,	11.011
580		0.65 ,	15000.0 ,		30.0 ,
	17724.6 ,		13543.7 ,	2628.1 ,	14.1919
581		0.65 ,	15000.0 ,		34.0 ,
	20349.9 ,		14496.6 ,	3420.7 ,	16.7302

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

582		0.65 ,	15000.0 ,		38.0 ,
	22863.3 ,		15337.4 ,	4243.8 ,	18.9494
583		0.65 ,	15000.0 ,		42.0 ,
	25300.6 ,		16102.7 ,	5073.7 ,	20.8824
584		0.65 ,	15000.0 ,		46.0 ,
	27684.0 ,		16813.4 ,	5945.8 ,	37.6447
585		0.65 ,	15000.0 ,		48.0 ,
	28853.2 ,		17146.3 ,	6412.4 ,	52.4446
586		0.65 ,	15000.0 ,		50.0 ,
	30016.4 ,		17473.3 ,	6885.5 ,	63.165
587		0.65 ,	20000.0 ,		21.0 ,
	9343.5 ,		8833.4 ,	837.7 ,	5.2653
588		0.65 ,	20000.0 ,		22.0 ,
	9935.0 ,		9118.7 ,	979.9 ,	6.2209
589		0.65 ,	20000.0 ,		24.0 ,
	11071.1 ,		9642.6 ,	1239.6 ,	7.74
590		0.65 ,	20000.0 ,		26.0 ,
	12156.3 ,		10115.6 ,	1497.6 ,	9.0357
591		0.65 ,	20000.0 ,		30.0 ,
	14427.2 ,		11026.1 ,	2101.3 ,	12.2787
592		0.65 ,	20000.0 ,		34.0 ,
	16564.3 ,		11802.7 ,	2729.9 ,	14.6793
593		0.65 ,	20000.0 ,		38.0 ,
	18610.2 ,		12488.0 ,	3382.1 ,	16.7756
594		0.65 ,	20000.0 ,		42.0 ,
	20594.6 ,		13112.0 ,	4040.1 ,	18.6009
595		0.65 ,	20000.0 ,		46.0 ,
	22534.2 ,		13691.1 ,	4731.2 ,	20.3058
596		0.65 ,	20000.0 ,		48.0 ,
	23485.7 ,		13962.4 ,	5100.5 ,	24.9412
597		0.65 ,	20000.0 ,		50.0 ,
	24432.6 ,		14229.1 ,	5474.5 ,	36.2661
598		0.65 ,	25000.0 ,		21.0 ,
	7538.7 ,		7127.2 ,	674.5 ,	6.3118
599		0.65 ,	25000.0 ,		22.0 ,
	8016.8 ,		7358.3 ,	786.7 ,	4.8016
600		0.65 ,	25000.0 ,		24.0 ,
	8934.3 ,		7781.9 ,	990.5 ,	6.2373
601		0.65 ,	25000.0 ,		26.0 ,
	9810.5 ,		8164.3 ,	1193.3 ,	7.4577

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

602		0.65 ,	25000.0 ,		30.0 ,
	11644.1 ,		8900.5 ,	1667.2 ,	9.8122
603		0.65 ,	25000.0 ,		34.0 ,
	13369.6 ,		9528.5 ,	2161.3 ,	12.6125
604		0.65 ,	25000.0 ,		38.0 ,
	15021.2 ,		10082.6 ,	2673.6 ,	14.582
605		0.65 ,	25000.0 ,		42.0 ,
	16623.1 ,		10587.1 ,	3190.9 ,	16.2937
606		0.65 ,	25000.0 ,		46.0 ,
	18188.8 ,		11055.3 ,	3733.0 ,	17.8916
607		0.65 ,	25000.0 ,		48.0 ,
	18957.1 ,		11274.9 ,	4023.5 ,	18.6867
608		0.65 ,	25000.0 ,		50.0 ,
	19721.6 ,		11490.7 ,	4316.5 ,	19.4646
609		0.65 ,	30000.0 ,		21.0 ,
	6025.8 ,		5696.8 ,	541.2 ,	9.2686
610		0.65 ,	30000.0 ,		22.0 ,
	6408.8 ,		5882.4 ,	628.6 ,	7.1132
611		0.65 ,	30000.0 ,		24.0 ,
	7143.4 ,		6222.1 ,	786.8 ,	4.7609
612		0.65 ,	30000.0 ,		26.0 ,
	7844.8 ,		6528.7 ,	944.9 ,	5.9115
613		0.65 ,	30000.0 ,		30.0 ,
	9312.7 ,		7119.2 ,	1313.5 ,	8.114
614		0.65 ,	30000.0 ,		34.0 ,
	10693.4 ,		7622.5 ,	1697.7 ,	10.5176
615		0.65 ,	30000.0 ,		38.0 ,
	12015.1 ,		8066.7 ,	2096.0 ,	12.429
616		0.65 ,	30000.0 ,		42.0 ,
	13296.7 ,		8470.9 ,	2498.2 ,	14.0245
617		0.65 ,	30000.0 ,		46.0 ,
	14549.5 ,		8846.3 ,	2919.9 ,	15.5145
618		0.65 ,	30000.0 ,		48.0 ,
	15164.4 ,		9022.5 ,	3145.2 ,	16.2578
619		0.65 ,	30000.0 ,		50.0 ,
	15776.0 ,		9195.4 ,	3372.5 ,	16.9835
620		0.65 ,	35000.0 ,		21.0 ,
	4767.0 ,		4506.6 ,	433.5 ,	12.2477
621		0.65 ,	35000.0 ,		22.0 ,
	5071.1 ,		4654.4 ,	500.8 ,	10.0982

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

622		0.65 ,	35000.0 ,	24.0 ,	
	5653.7 ,		4924.4 ,	622.1 ,	6.8639
623		0.65 ,	35000.0 ,	26.0 ,	
	6210.0 ,		5168.0 ,	743.9 ,	4.422
624		0.65 ,	35000.0 ,	30.0 ,	
	7373.7 ,		5637.1 ,	1027.3 ,	6.4841
625		0.65 ,	35000.0 ,	34.0 ,	
	8468.2 ,		6037.1 ,	1322.7 ,	8.2441
626		0.65 ,	35000.0 ,	38.0 ,	
	9515.4 ,		6389.7 ,	1628.5 ,	10.3632
627		0.65 ,	35000.0 ,	42.0 ,	
	10530.9 ,		6710.5 ,	1938.8 ,	11.8544
628		0.65 ,	35000.0 ,	46.0 ,	
	11523.6 ,		7008.6 ,	2262.9 ,	13.2342
629		0.65 ,	35000.0 ,	48.0 ,	
	12010.7 ,		7148.5 ,	2436.1 ,	13.9247
630		0.65 ,	35000.0 ,	50.0 ,	
	12495.8 ,		7286.2 ,	2609.9 ,	14.5969
631		0.65 ,	37000.0 ,	21.0 ,	
	4328.0 ,		4091.4 ,	398.3 ,	12.7114
632		0.65 ,	37000.0 ,	22.0 ,	
	4604.7 ,		4226.1 ,	459.1 ,	10.5799
633		0.65 ,	37000.0 ,	24.0 ,	
	5134.7 ,		4472.0 ,	568.6 ,	7.4067
634		0.65 ,	37000.0 ,	26.0 ,	
	5640.3 ,		4693.6 ,	678.3 ,	4.7981
635		0.65 ,	37000.0 ,	30.0 ,	
	6698.2 ,		5120.4 ,	934.1 ,	6.0241
636		0.65 ,	37000.0 ,	34.0 ,	
	7693.1 ,		5484.2 ,	1200.6 ,	7.7263
637		0.65 ,	37000.0 ,	38.0 ,	
	8645.0 ,		5805.0 ,	1476.6 ,	9.5229
638		0.65 ,	37000.0 ,	42.0 ,	
	9567.7 ,		6096.5 ,	1757.2 ,	11.1876
639		0.65 ,	37000.0 ,	46.0 ,	
	10470.1 ,		6367.8 ,	2049.0 ,	12.5173
640		0.65 ,	37000.0 ,	48.0 ,	
	10912.6 ,		6494.8 ,	2205.3 ,	13.1845
641		0.65 ,	37000.0 ,	50.0 ,	
	11353.7 ,		6620.3 ,	2361.7 ,	13.8301

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

642		0.65,	39000.0,		21.0,
	3928.0,		3713.0,	368.4,	12.2906
643		0.65,	39000.0,		22.0,
	4179.8,		3835.7,	423.5,	10.2222
644		0.65,	39000.0,		24.0,
	4661.5,		4059.5,	522.5,	7.1754
645		0.65,	39000.0,		26.0,
	5121.2,		4261.1,	622.3,	4.6517
646		0.65,	39000.0,		30.0,
	6082.8,		4649.3,	854.5,	5.7838
647		0.65,	39000.0,		34.0,
	6987.2,		4980.3,	1096.2,	7.4195
648		0.65,	39000.0,		38.0,
	7852.3,		5272.0,	1347.0,	9.1325
649		0.65,	39000.0,		42.0,
	8690.6,		5536.9,	1601.9,	10.7517
650		0.65,	39000.0,		46.0,
	9510.4,		5783.5,	1866.9,	12.0307
651		0.65,	39000.0,		48.0,
	9912.8,		5899.1,	2008.5,	12.6712
652		0.65,	39000.0,		50.0,
	10313.9,		6013.4,	2149.9,	13.285
653		0.65,	41000.0,		21.0,
	3564.4,		3369.0,	341.4,	11.8988
654		0.65,	41000.0,		22.0,
	3793.7,		3481.1,	391.2,	9.8837
655		0.65,	41000.0,		24.0,
	4231.9,		3684.9,	480.9,	6.9499
656		0.65,	41000.0,		26.0,
	4649.7,		3868.3,	571.5,	4.5148
657		0.65,	41000.0,		30.0,
	5523.7,		4221.4,	782.2,	5.5521
658		0.65,	41000.0,		34.0,
	6345.8,		4522.5,	1001.6,	7.1247
659		0.65,	41000.0,		38.0,
	7131.8,		4787.6,	1229.2,	8.7518
660		0.65,	41000.0,		42.0,
	7893.5,		5028.4,	1460.7,	10.3306
661		0.65,	41000.0,		46.0,
	8638.7,		5252.7,	1701.3,	11.5623

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

662		0.65 ,	41000.0 ,	48.0 ,	
	9004.5 ,		5357.9 ,	1829.8 ,	12.177
663		0.65 ,	41000.0 ,	50.0 ,	
	9369.0 ,		5462.0 ,	1957.7 ,	12.7624
664		0.7 ,	15000.0 ,	21.0 ,	
	13112.0 ,		12479.9 ,	1130.1 ,	7.3244
665		0.7 ,	15000.0 ,	22.0 ,	
	13855.4 ,		12844.0 ,	1307.0 ,	8.2542
666		0.7 ,	15000.0 ,	24.0 ,	
	15285.0 ,		13515.0 ,	1648.6 ,	9.8351
667		0.7 ,	15000.0 ,	26.0 ,	
	16649.3 ,		14120.8 ,	1994.3 ,	11.9014
668		0.7 ,	15000.0 ,	30.0 ,	
	19512.9 ,		15298.6 ,	2780.9 ,	14.827
669		0.7 ,	15000.0 ,	34.0 ,	
	22204.6 ,		16304.7 ,	3606.0 ,	17.3622
670		0.7 ,	15000.0 ,	38.0 ,	
	24778.2 ,		17192.6 ,	4465.4 ,	19.5875
671		0.7 ,	15000.0 ,	42.0 ,	
	27296.1 ,		18024.8 ,	5329.0 ,	23.4826
672		0.7 ,	15000.0 ,	46.0 ,	
	29762.1 ,		18805.2 ,	6235.3 ,	46.8096
673		0.7 ,	15000.0 ,	48.0 ,	
	30970.5 ,		19170.8 ,	6719.8 ,	59.383
674		0.7 ,	15000.0 ,	50.0 ,	
	32171.1 ,		19528.5 ,	7209.9 ,	68.7032
675		0.7 ,	20000.0 ,	21.0 ,	
	10671.0 ,		10156.9 ,	912.4 ,	5.9185
676		0.7 ,	20000.0 ,	22.0 ,	
	11276.8 ,		10454.1 ,	1053.1 ,	6.8056
677		0.7 ,	20000.0 ,	24.0 ,	
	12440.5 ,		11000.8 ,	1323.8 ,	8.3011
678		0.7 ,	20000.0 ,	26.0 ,	
	13551.0 ,		11494.4 ,	1598.0 ,	9.6082
679		0.7 ,	20000.0 ,	30.0 ,	
	15882.3 ,		12454.6 ,	2221.7 ,	12.8741
680		0.7 ,	20000.0 ,	34.0 ,	
	18073.4 ,		13274.7 ,	2876.5 ,	15.2715
681		0.7 ,	20000.0 ,	38.0 ,	
	20168.3 ,		13998.5 ,	3557.9 ,	17.3754

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

682		0.7 ,	20000.0 ,		42.0 ,
	22217.1 ,		14676.3 ,	4242.1 ,	19.2013
683		0.7 ,	20000.0 ,		46.0 ,
	24224.9 ,		15312.9 ,	4960.5 ,	22.3983
684		0.7 ,	20000.0 ,		48.0 ,
	25208.3 ,		15610.7 ,	5344.4 ,	30.8596
685		0.7 ,	20000.0 ,		50.0 ,
	26185.8 ,		15902.7 ,	5731.7 ,	44.4788
686		0.7 ,	25000.0 ,		21.0 ,
	8610.5 ,		8195.8 ,	733.3 ,	4.7574
687		0.7 ,	25000.0 ,		22.0 ,
	9099.7 ,		8436.2 ,	843.9 ,	5.3542
688		0.7 ,	25000.0 ,		24.0 ,
	10039.4 ,		8878.3 ,	1056.5 ,	6.7662
689		0.7 ,	25000.0 ,		26.0 ,
	10936.2 ,		9277.4 ,	1272.2 ,	7.9972
690		0.7 ,	25000.0 ,		30.0 ,
	12818.5 ,		10053.9 ,	1762.2 ,	10.8094
691		0.7 ,	25000.0 ,		34.0 ,
	14587.3 ,		10716.9 ,	2276.5 ,	13.1665
692		0.7 ,	25000.0 ,		38.0 ,
	16278.4 ,		11302.1 ,	2811.5 ,	15.1405
693		0.7 ,	25000.0 ,		42.0 ,
	17932.2 ,		11850.1 ,	3349.2 ,	16.8532
694		0.7 ,	25000.0 ,		46.0 ,
	19552.5 ,		12364.7 ,	3912.9 ,	18.4489
695		0.7 ,	25000.0 ,		48.0 ,
	20346.0 ,		12605.2 ,	4213.9 ,	19.2419
696		0.7 ,	25000.0 ,		50.0 ,
	21135.9 ,		12842.2 ,	4516.7 ,	20.8046
697		0.7 ,	30000.0 ,		21.0 ,
	6883.1 ,		6551.6 ,	586.9 ,	7.7444
698		0.7 ,	30000.0 ,		22.0 ,
	7275.0 ,		6744.6 ,	673.2 ,	5.7924
699		0.7 ,	30000.0 ,		24.0 ,
	8027.3 ,		7099.1 ,	838.4 ,	5.2616
700		0.7 ,	30000.0 ,		26.0 ,
	8744.9 ,		7418.9 ,	1005.9 ,	6.4147
701		0.7 ,	30000.0 ,		30.0 ,
	10251.7 ,		8041.7 ,	1387.1 ,	8.5806

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

702		0.7 ,	30000.0 ,		34.0 ,
	11667.2 ,		8573.2 ,	1787.1 ,	11.0992
703		0.7 ,	30000.0 ,		38.0 ,
	13020.3 ,		9042.3 ,	2203.0 ,	12.9445
704		0.7 ,	30000.0 ,		42.0 ,
	14343.5 ,		9481.5 ,	2621.7 ,	14.5449
705		0.7 ,	30000.0 ,		46.0 ,
	15639.9 ,		9894.0 ,	3059.8 ,	16.0318
706		0.7 ,	30000.0 ,		48.0 ,
	16274.9 ,		10087.0 ,	3293.1 ,	16.7705
707		0.7 ,	30000.0 ,		50.0 ,
	16906.9 ,		10277.0 ,	3528.3 ,	17.4883
708		0.7 ,	35000.0 ,		21.0 ,
	5445.9 ,		5183.5 ,	468.4 ,	10.7259
709		0.7 ,	35000.0 ,		22.0 ,
	5757.0 ,		5337.1 ,	535.0 ,	8.7976
710		0.7 ,	35000.0 ,		24.0 ,
	6353.6 ,		5618.9 ,	661.7 ,	5.6702
711		0.7 ,	35000.0 ,		26.0 ,
	6922.8 ,		5873.2 ,	791.0 ,	4.8981
712		0.7 ,	35000.0 ,		30.0 ,
	8117.1 ,		6367.8 ,	1083.9 ,	6.9194
713		0.7 ,	35000.0 ,		34.0 ,
	9239.1 ,		6790.1 ,	1391.6 ,	8.6731
714		0.7 ,	35000.0 ,		38.0 ,
	10311.5 ,		7162.7 ,	1711.2 ,	10.8441
715		0.7 ,	35000.0 ,		42.0 ,
	11359.5 ,		7511.0 ,	2033.2 ,	12.3341
716		0.7 ,	35000.0 ,		46.0 ,
	12386.9 ,		7838.7 ,	2370.3 ,	13.7136
717		0.7 ,	35000.0 ,		48.0 ,
	12890.1 ,		7992.0 ,	2549.7 ,	14.4009
718		0.7 ,	35000.0 ,		50.0 ,
	13391.1 ,		8143.2 ,	2729.2 ,	15.0634
719		0.7 ,	37000.0 ,		21.0 ,
	4944.6 ,		4706.2 ,	429.8 ,	11.2106
720		0.7 ,	37000.0 ,		22.0 ,
	5227.7 ,		4846.2 ,	489.9 ,	9.3025
721		0.7 ,	37000.0 ,		24.0 ,
	5770.2 ,		5102.7 ,	604.1 ,	6.2444

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

722		0.7 ,	37000.0 ,		26.0 ,	
	6287.7 ,		5334.1 ,	720.9 ,		4.4868
723		0.7 ,	37000.0 ,		30.0 ,	
	7373.4 ,		5784.0 ,	985.0 ,		6.4444
724		0.7 ,	37000.0 ,		34.0 ,	
	8393.3 ,		6168.3 ,	1262.6 ,		8.1407
725		0.7 ,	37000.0 ,		38.0 ,	
	9368.0 ,		6507.2 ,	1551.0 ,		10.2088
726		0.7 ,	37000.0 ,		42.0 ,	
	10320.4 ,		6823.9 ,	1842.1 ,		11.6506
727		0.7 ,	37000.0 ,		46.0 ,	
	11254.0 ,		7121.8 ,	2146.1 ,		12.9821
728		0.7 ,	37000.0 ,		48.0 ,	
	11711.4 ,		7261.3 ,	2308.0 ,		13.645
729		0.7 ,	37000.0 ,		50.0 ,	
	12167.0 ,		7399.1 ,	2469.7 ,		14.282
730		0.7 ,	39000.0 ,		21.0 ,	
	4487.8 ,		4271.2 ,	396.9 ,		10.8462
731		0.7 ,	39000.0 ,		22.0 ,	
	4745.4 ,		4398.8 ,	451.5 ,		8.9937
732		0.7 ,	39000.0 ,		24.0 ,	
	5238.7 ,		4632.3 ,	555.0 ,		6.0497
733		0.7 ,	39000.0 ,		26.0 ,	
	5709.1 ,		4842.7 ,	660.9 ,		4.3014
734		0.7 ,	39000.0 ,		30.0 ,	
	6696.0 ,		5252.1 ,	900.8 ,		6.1896
735		0.7 ,	39000.0 ,		34.0 ,	
	7623.1 ,		5601.6 ,	1152.7 ,		7.8201
736		0.7 ,	39000.0 ,		38.0 ,	
	8508.9 ,		5909.8 ,	1414.4 ,		9.8095
737		0.7 ,	39000.0 ,		42.0 ,	
	9374.1 ,		6197.4 ,	1678.7 ,		11.196
738		0.7 ,	39000.0 ,		46.0 ,	
	10222.7 ,		6468.4 ,	1955.0 ,		12.4794
739		0.7 ,	39000.0 ,		48.0 ,	
	10638.4 ,		6595.3 ,	2101.9 ,		13.1156
740		0.7 ,	39000.0 ,		50.0 ,	
	11052.6 ,		6720.7 ,	2248.2 ,		13.7233
741		0.7 ,	41000.0 ,		21.0 ,	
	4072.9 ,		3876.1 ,	367.0 ,		10.4999

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

742		0.7 ,	41000.0 ,		22.0 ,	
	4307.3 ,		3992.4 ,	416.6 ,		8.698
743		0.7 ,	41000.0 ,		24.0 ,	
	4756.0 ,		4204.9 ,	510.3 ,		5.8669
744		0.7 ,	41000.0 ,		26.0 ,	
	5183.6 ,		4396.4 ,	606.4 ,		4.1214
745		0.7 ,	41000.0 ,		30.0 ,	
	6080.8 ,		4768.8 ,	824.2 ,		5.9412
746		0.7 ,	41000.0 ,		34.0 ,	
	6923.7 ,		5086.9 ,	1052.9 ,		7.5111
747		0.7 ,	41000.0 ,		38.0 ,	
	7728.7 ,		5367.1 ,	1290.6 ,		9.4241
748		0.7 ,	41000.0 ,		42.0 ,	
	8515.0 ,		5628.6 ,	1531.1 ,		10.7626
749		0.7 ,	41000.0 ,		46.0 ,	
	9286.2 ,		5874.9 ,	1781.7 ,		11.9963
750		0.7 ,	41000.0 ,		48.0 ,	
	9664.1 ,		5990.4 ,	1914.9 ,		12.6068
751		0.7 ,	41000.0 ,		50.0 ,	
	10040.5 ,		6104.4 ,	2047.5 ,		13.1893
752		0.7 ,	43000.0 ,		21.0 ,	
	3695.7 ,		3516.9 ,	340.2 ,		10.182
753		0.7 ,	43000.0 ,		22.0 ,	
	3909.2 ,		3623.1 ,	385.1 ,		8.4342
754		0.7 ,	43000.0 ,		24.0 ,	
	4317.5 ,		3816.8 ,	469.8 ,		5.6921
755		0.7 ,	43000.0 ,		26.0 ,	
	4706.4 ,		3991.1 ,	557.2 ,		3.9488
756		0.7 ,	43000.0 ,		30.0 ,	
	5522.1 ,		4329.9 ,	754.8 ,		5.704
757		0.7 ,	43000.0 ,		34.0 ,	
	6288.3 ,		4619.3 ,	962.3 ,		7.2124
758		0.7 ,	43000.0 ,		38.0 ,	
	7019.9 ,		4874.0 ,	1178.2 ,		9.0518
759		0.7 ,	43000.0 ,		42.0 ,	
	7734.6 ,		5111.8 ,	1396.8 ,		10.3435
760		0.7 ,	43000.0 ,		46.0 ,	
	8435.5 ,		5335.9 ,	1624.2 ,		11.5304
761		0.7 ,	43000.0 ,		48.0 ,	
	8778.7 ,		5440.7 ,	1745.0 ,		12.1165

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

762		0.7 ,	43000.0 ,		50.0 ,
	9121.2 ,		5544.6 ,	1865.4 ,	12.6763
763		0.75 ,	20000.0 ,		21.0 ,
	12099.2 ,		11578.4 ,	993.4 ,	6.5843
764		0.75 ,	20000.0 ,		22.0 ,
	12724.0 ,		11890.6 ,	1129.3 ,	7.3857
765		0.75 ,	20000.0 ,		24.0 ,
	13920.6 ,		12462.1 ,	1410.5 ,	8.8599
766		0.75 ,	20000.0 ,		26.0 ,
	15061.0 ,		12977.4 ,	1701.9 ,	10.3273
767		0.75 ,	20000.0 ,		30.0 ,
	17460.5 ,		13988.0 ,	2352.5 ,	13.4976
768		0.75 ,	20000.0 ,		34.0 ,
	19714.1 ,		14852.5 ,	3037.5 ,	15.8999
769		0.75 ,	20000.0 ,		38.0 ,
	21884.6 ,		15634.1 ,	3751.2 ,	18.0102
770		0.75 ,	20000.0 ,		42.0 ,
	24018.9 ,		16379.3 ,	4468.2 ,	19.8495
771		0.75 ,	20000.0 ,		46.0 ,
	26105.5 ,		17076.8 ,	5219.0 ,	27.2502
772		0.75 ,	20000.0 ,		48.0 ,
	27126.2 ,		17402.8 ,	5619.3 ,	39.5279
773		0.75 ,	20000.0 ,		50.0 ,
	28140.0 ,		17722.3 ,	6024.0 ,	53.0099
774		0.75 ,	25000.0 ,		21.0 ,
	9763.6 ,		9343.5 ,	797.1 ,	5.1492
775		0.75 ,	25000.0 ,		22.0 ,
	10267.9 ,		9595.8 ,	903.1 ,	5.8999
776		0.75 ,	25000.0 ,		24.0 ,
	11234.1 ,		10058.0 ,	1124.6 ,	7.2923
777		0.75 ,	25000.0 ,		26.0 ,
	12154.7 ,		10474.5 ,	1353.8 ,	8.5338
778		0.75 ,	25000.0 ,		30.0 ,
	14092.2 ,		11291.8 ,	1864.8 ,	11.4987
779		0.75 ,	25000.0 ,		34.0 ,
	15911.3 ,		11990.8 ,	2403.1 ,	13.7532
780		0.75 ,	25000.0 ,		38.0 ,
	17663.3 ,		12622.6 ,	2963.2 ,	15.732
781		0.75 ,	25000.0 ,		42.0 ,
	19385.8 ,		13225.0 ,	3526.7 ,	17.4568

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

782		0.75 ,	25000.0 ,		46.0 ,
	21070.1 ,		13789.1 ,	4116.3 ,	19.0568
783		0.75 ,	25000.0 ,		48.0 ,
	21894.0 ,		14052.8 ,	4429.6 ,	19.8471
784		0.75 ,	25000.0 ,		50.0 ,
	22712.7 ,		14311.6 ,	4746.3 ,	24.5603
785		0.75 ,	30000.0 ,		21.0 ,
	7805.4 ,		7469.7 ,	636.6 ,	6.2175
786		0.75 ,	30000.0 ,		22.0 ,
	8209.2 ,		7672.0 ,	718.6 ,	4.557
787		0.75 ,	30000.0 ,		24.0 ,
	8982.7 ,		8042.7 ,	891.3 ,	5.7565
788		0.75 ,	30000.0 ,		26.0 ,
	9719.7 ,		8376.8 ,	1069.8 ,	6.9217
789		0.75 ,	30000.0 ,		30.0 ,
	11270.2 ,		9032.1 ,	1467.1 ,	9.0687
790		0.75 ,	30000.0 ,		34.0 ,
	12725.6 ,		9592.3 ,	1885.5 ,	11.6454
791		0.75 ,	30000.0 ,		38.0 ,
	14127.3 ,		10098.7 ,	2320.9 ,	13.4935
792		0.75 ,	30000.0 ,		42.0 ,
	15505.2 ,		10581.3 ,	2759.3 ,	15.1024
793		0.75 ,	30000.0 ,		46.0 ,
	16852.7 ,		11033.5 ,	3217.1 ,	16.5918
794		0.75 ,	30000.0 ,		48.0 ,
	17511.6 ,		11244.9 ,	3461.0 ,	17.331
795		0.75 ,	30000.0 ,		50.0 ,
	18167.3 ,		11452.9 ,	3705.8 ,	18.0435
796		0.75 ,	35000.0 ,		21.0 ,
	6176.3 ,		5910.6 ,	506.6 ,	9.2124
797		0.75 ,	35000.0 ,		22.0 ,
	6496.8 ,		6071.7 ,	569.8 ,	7.5518
798		0.75 ,	35000.0 ,		24.0 ,
	7110.0 ,		6366.1 ,	702.3 ,	4.5131
799		0.75 ,	35000.0 ,		26.0 ,
	7694.4 ,		6631.6 ,	839.8 ,	5.3704
800		0.75 ,	35000.0 ,		30.0 ,
	8923.6 ,		7152.1 ,	1145.3 ,	7.3736
801		0.75 ,	35000.0 ,		34.0 ,
	10077.2 ,		7597.2 ,	1467.2 ,	9.1266

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

802		0.75 ,	35000.0 ,		38.0 ,
	11187.9 ,		7999.4 ,	1801.8 ,	11.3524
803		0.75 ,	35000.0 ,		42.0 ,
	12279.4 ,		8382.4 ,	2139.1 ,	12.8488
804		0.75 ,	35000.0 ,		46.0 ,
	13347.0 ,		8741.4 ,	2491.2 ,	14.2339
805		0.75 ,	35000.0 ,		48.0 ,
	13869.4 ,		8909.5 ,	2678.5 ,	14.9197
806		0.75 ,	35000.0 ,		50.0 ,
	14389.1 ,		9075.0 ,	2865.5 ,	15.5782
807		0.75 ,	37000.0 ,		21.0 ,
	5608.1 ,		5366.7 ,	464.3 ,	9.7221
808		0.75 ,	37000.0 ,		22.0 ,
	5899.7 ,		5513.5 ,	521.3 ,	8.0824
809		0.75 ,	37000.0 ,		24.0 ,
	6457.4 ,		5781.4 ,	640.8 ,	5.1113
810		0.75 ,	37000.0 ,		26.0 ,
	6988.6 ,		6023.0 ,	764.9 ,	4.9447
811		0.75 ,	37000.0 ,		30.0 ,
	8106.0 ,		6496.6 ,	1040.5 ,	6.8848
812		0.75 ,	37000.0 ,		34.0 ,
	9154.7 ,		6901.6 ,	1331.0 ,	8.58
813		0.75 ,	37000.0 ,		38.0 ,
	10164.2 ,		7267.4 ,	1632.9 ,	10.6998
814		0.75 ,	37000.0 ,		42.0 ,
	11156.1 ,		7615.6 ,	1937.4 ,	12.1486
815		0.75 ,	37000.0 ,		46.0 ,
	12126.5 ,		7942.2 ,	2255.5 ,	13.4852
816		0.75 ,	37000.0 ,		48.0 ,
	12601.0 ,		8094.8 ,	2424.1 ,	14.1465
817		0.75 ,	37000.0 ,		50.0 ,
	13073.6 ,		8245.6 ,	2592.2 ,	14.7777
818		0.75 ,	39000.0 ,		21.0 ,
	5090.3 ,		4871.0 ,	428.1 ,	9.413
819		0.75 ,	39000.0 ,		22.0 ,
	5355.6 ,		5004.7 ,	479.9 ,	7.8205
820		0.75 ,	39000.0 ,		24.0 ,
	5862.7 ,		5248.6 ,	588.2 ,	4.959
821		0.75 ,	39000.0 ,		26.0 ,
	6345.7 ,		5468.4 ,	700.9 ,	4.7432

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

822		0.75 ,	39000.0 ,		30.0 ,	
	7361.5 ,		5899.2 ,	951.1 ,		6.612
823		0.75 ,	39000.0 ,		34.0 ,	
	8314.7 ,		6267.5 ,	1214.7 ,		8.2426
824		0.75 ,	39000.0 ,		38.0 ,	
	9232.3 ,		6600.2 ,	1488.9 ,		10.2835
825		0.75 ,	39000.0 ,		42.0 ,	
	10133.6 ,		6916.7 ,	1765.7 ,		11.6794
826		0.75 ,	39000.0 ,		46.0 ,	
	11015.2 ,		7213.4 ,	2054.3 ,		12.9644
827		0.75 ,	39000.0 ,		48.0 ,	
	11446.7 ,		7352.4 ,	2207.5 ,		13.5999
828		0.75 ,	39000.0 ,		50.0 ,	
	11876.3 ,		7489.5 ,	2360.1 ,		14.2058
829		0.75 ,	41000.0 ,		21.0 ,	
	4620.0 ,		4420.7 ,	395.3 ,		9.1163
830		0.75 ,	41000.0 ,		22.0 ,	
	4861.4 ,		4542.5 ,	442.3 ,		7.5735
831		0.75 ,	41000.0 ,		24.0 ,	
	5322.7 ,		4764.6 ,	540.6 ,		4.8099
832		0.75 ,	41000.0 ,		26.0 ,	
	5761.8 ,		4964.6 ,	642.9 ,		4.5487
833		0.75 ,	41000.0 ,		30.0 ,	
	6685.2 ,		5356.6 ,	869.9 ,		6.3495
834		0.75 ,	41000.0 ,		34.0 ,	
	7551.8 ,		5691.7 ,	1109.2 ,		7.9189
835		0.75 ,	41000.0 ,		38.0 ,	
	8385.8 ,		5994.3 ,	1358.1 ,		9.8824
836		0.75 ,	41000.0 ,		42.0 ,	
	9204.8 ,		6281.8 ,	1609.8 ,		11.2269
837		0.75 ,	41000.0 ,		46.0 ,	
	10006.1 ,		6551.7 ,	1872.0 ,		12.4638
838		0.75 ,	41000.0 ,		48.0 ,	
	10398.3 ,		6678.1 ,	2010.9 ,		13.0741
839		0.75 ,	41000.0 ,		50.0 ,	
	10788.7 ,		6802.8 ,	2149.4 ,		13.6567
840		0.75 ,	43000.0 ,		21.0 ,	
	4192.7 ,		4011.6 ,	365.5 ,		8.8388
841		0.75 ,	43000.0 ,		22.0 ,	
	4412.3 ,		4122.6 ,	408.2 ,		7.3458

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

842		0.75 ,	43000.0 ,		24.0 ,
	4832.0 ,		4324.9 ,	497.1 ,	4.6778
843		0.75 ,	43000.0 ,		26.0 ,
	5231.3 ,		4506.9 ,	590.1 ,	4.3594
844		0.75 ,	43000.0 ,		30.0 ,
	6071.0 ,		4863.7 ,	796.3 ,	6.0969
845		0.75 ,	43000.0 ,		34.0 ,
	6858.8 ,		5168.6 ,	1013.4 ,	7.606
846		0.75 ,	43000.0 ,		38.0 ,
	7616.8 ,		5443.7 ,	1239.5 ,	9.4944
847		0.75 ,	43000.0 ,		42.0 ,
	8361.0 ,		5705.0 ,	1468.3 ,	10.7912
848		0.75 ,	43000.0 ,		46.0 ,
	9089.4 ,		5950.4 ,	1706.1 ,	11.9799
849		0.75 ,	43000.0 ,		48.0 ,
	9445.7 ,		6065.4 ,	1832.3 ,	12.5674
850		0.75 ,	43000.0 ,		50.0 ,
	9800.8 ,		6179.0 ,	1958.1 ,	13.1272
851		0.79 ,	20000.0 ,		21.0 ,
	13316.7 ,		12788.5 ,	1056.2 ,	7.085
852		0.79 ,	20000.0 ,		22.0 ,
	13958.5 ,		13113.3 ,	1191.3 ,	7.8437
853		0.79 ,	20000.0 ,		24.0 ,
	15183.9 ,		13704.9 ,	1486.2 ,	9.3251
854		0.79 ,	20000.0 ,		26.0 ,
	16353.4 ,		14240.4 ,	1788.3 ,	11.2602
855		0.79 ,	20000.0 ,		30.0 ,
	18814.0 ,		15292.3 ,	2465.9 ,	14.0199
856		0.79 ,	20000.0 ,		34.0 ,
	21136.0 ,		16205.7 ,	3176.5 ,	16.4247
857		0.79 ,	20000.0 ,		38.0 ,
	23387.7 ,		17048.6 ,	3921.0 ,	18.5484
858		0.79 ,	20000.0 ,		42.0 ,
	25599.2 ,		17851.6 ,	4668.4 ,	20.4014
859		0.79 ,	20000.0 ,		46.0 ,
	27757.9 ,		18601.6 ,	5449.7 ,	33.7104
860		0.79 ,	20000.0 ,		48.0 ,
	28812.4 ,		18951.7 ,	5865.5 ,	47.6231
861		0.79 ,	20000.0 ,		50.0 ,
	29859.3 ,		19294.4 ,	6286.5 ,	58.7708

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

862		0.79 ,	25000.0 ,	21.0 ,	
	10746.2 ,		10320.3 ,	846.3 ,	5.6217
863		0.79 ,	25000.0 ,	22.0 ,	
	11264.8 ,		10583.2 ,	952.1 ,	6.3348
864		0.79 ,	25000.0 ,	24.0 ,	
	12254.3 ,		11061.5 ,	1184.1 ,	7.73
865		0.79 ,	25000.0 ,	26.0 ,	
	13198.3 ,		11494.4 ,	1421.7 ,	8.9669
866		0.79 ,	25000.0 ,	30.0 ,	
	15184.9 ,		12345.0 ,	1954.0 ,	11.9882
867		0.79 ,	25000.0 ,	34.0 ,	
	17059.4 ,		13083.5 ,	2512.5 ,	14.2443
868		0.79 ,	25000.0 ,	38.0 ,	
	18877.2 ,		13765.2 ,	3097.0 ,	16.2353
869		0.79 ,	25000.0 ,	42.0 ,	
	20662.0 ,		14414.1 ,	3683.6 ,	17.9702
870		0.79 ,	25000.0 ,	46.0 ,	
	22404.6 ,		15020.7 ,	4297.5 ,	19.5778
871		0.79 ,	25000.0 ,	48.0 ,	
	23255.8 ,		15303.8 ,	4623.5 ,	21.9802
872		0.79 ,	25000.0 ,	50.0 ,	
	24101.0 ,		15581.1 ,	4952.6 ,	29.7794
873		0.79 ,	30000.0 ,	21.0 ,	
	8591.6 ,		8251.2 ,	675.0 ,	5.0944
874		0.79 ,	30000.0 ,	22.0 ,	
	9006.5 ,		8461.9 ,	756.7 ,	4.8532
875		0.79 ,	30000.0 ,	24.0 ,	
	9798.6 ,		8845.4 ,	937.1 ,	6.1642
876		0.79 ,	30000.0 ,	26.0 ,	
	10554.1 ,		9192.5 ,	1122.5 ,	7.3259
877		0.79 ,	30000.0 ,	30.0 ,	
	12143.7 ,		9874.3 ,	1536.0 ,	9.4741
878		0.79 ,	30000.0 ,	34.0 ,	
	13643.5 ,		10466.3 ,	1970.6 ,	12.1021
879		0.79 ,	30000.0 ,	38.0 ,	
	15097.6 ,		11012.7 ,	2424.8 ,	13.9599
880		0.79 ,	30000.0 ,	42.0 ,	
	16525.2 ,		11532.5 ,	2881.4 ,	15.5783
881		0.79 ,	30000.0 ,	46.0 ,	
	17919.4 ,		12018.9 ,	3357.8 ,	17.0748

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

882		0.79 ,	30000.0 ,		48.0 ,
	18600.1 ,		12245.8 ,	3611.2 ,	17.8146
883		0.79 ,	30000.0 ,		50.0 ,
	19277.1 ,		12468.8 ,	3865.8 ,	18.5261
884		0.79 ,	35000.0 ,		21.0 ,
	6798.9 ,		6529.5 ,	536.1 ,	8.112
885		0.79 ,	35000.0 ,		22.0 ,
	7128.1 ,		6697.1 ,	598.7 ,	6.5792
886		0.79 ,	35000.0 ,		24.0 ,
	7756.4 ,		7002.1 ,	737.5 ,	4.6585
887		0.79 ,	35000.0 ,		26.0 ,
	8355.2 ,		7277.7 ,	880.4 ,	5.7496
888		0.79 ,	35000.0 ,		30.0 ,
	9615.4 ,		7819.4 ,	1198.4 ,	7.7528
889		0.79 ,	35000.0 ,		34.0 ,
	10803.8 ,		8289.5 ,	1532.7 ,	9.805
890		0.79 ,	35000.0 ,		38.0 ,
	11956.1 ,		8723.4 ,	1881.7 ,	11.7838
891		0.79 ,	35000.0 ,		42.0 ,
	13087.1 ,		9135.9 ,	2232.9 ,	13.2881
892		0.79 ,	35000.0 ,		46.0 ,
	14191.7 ,		9522.2 ,	2599.6 ,	14.681
893		0.79 ,	35000.0 ,		48.0 ,
	14731.2 ,		9702.5 ,	2793.6 ,	15.3669
894		0.79 ,	35000.0 ,		50.0 ,
	15267.9 ,		9880.0 ,	2987.8 ,	16.0243
895		0.79 ,	37000.0 ,		21.0 ,
	6173.6 ,		5928.9 ,	490.9 ,	8.6418
896		0.79 ,	37000.0 ,		22.0 ,
	6473.1 ,		6081.5 ,	547.1 ,	7.1362
897		0.79 ,	37000.0 ,		24.0 ,
	7044.4 ,		6359.1 ,	672.3 ,	4.2757
898		0.79 ,	37000.0 ,		26.0 ,
	7588.8 ,		6609.9 ,	801.5 ,	5.3123
899		0.79 ,	37000.0 ,		30.0 ,
	8734.3 ,		7102.7 ,	1088.2 ,	7.2492
900		0.79 ,	37000.0 ,		34.0 ,
	9814.5 ,		7530.3 ,	1389.7 ,	8.9444
901		0.79 ,	37000.0 ,		38.0 ,
	10862.0 ,		7925.1 ,	1704.9 ,	11.1167

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

902		0.79 ,	37000.0 ,		42.0 ,
	11889.7 ,		8300.2 ,	2022.2 ,	12.5731
903		0.79 ,	37000.0 ,		46.0 ,
	12893.6 ,		8651.4 ,	2352.9 ,	13.9174
904		0.79 ,	37000.0 ,		48.0 ,
	13383.9 ,		8815.5 ,	2528.3 ,	14.5794
905		0.79 ,	37000.0 ,		50.0 ,
	13871.8 ,		8977.0 ,	2703.4 ,	15.2136
906		0.79 ,	39000.0 ,		21.0 ,
	5603.8 ,		5381.5 ,	452.2 ,	8.3724
907		0.79 ,	39000.0 ,		22.0 ,
	5876.3 ,		5520.5 ,	503.1 ,	6.9121
908		0.79 ,	39000.0 ,		24.0 ,
	6395.9 ,		5773.3 ,	616.7 ,	4.1333
909		0.79 ,	39000.0 ,		26.0 ,
	6890.8 ,		6001.3 ,	734.2 ,	5.0969
910		0.79 ,	39000.0 ,		30.0 ,
	7932.0 ,		6449.6 ,	994.3 ,	6.962
911		0.79 ,	39000.0 ,		34.0 ,
	8914.2 ,		6838.7 ,	1268.4 ,	8.5965
912		0.79 ,	39000.0 ,		38.0 ,
	9866.0 ,		7197.6 ,	1554.3 ,	10.685
913		0.79 ,	39000.0 ,		42.0 ,
	10799.9 ,		7538.5 ,	1842.4 ,	12.0879
914		0.79 ,	39000.0 ,		46.0 ,
	11712.2 ,		7857.8 ,	2143.1 ,	13.3818
915		0.79 ,	39000.0 ,		48.0 ,
	12157.8 ,		8007.0 ,	2302.2 ,	14.0174
916		0.79 ,	39000.0 ,		50.0 ,
	12601.3 ,		8153.9 ,	2461.0 ,	14.6254
917		0.79 ,	41000.0 ,		21.0 ,
	5086.2 ,		4884.2 ,	417.1 ,	8.114
918		0.79 ,	41000.0 ,		22.0 ,
	5334.1 ,		5010.8 ,	463.4 ,	6.7051
919		0.79 ,	41000.0 ,		24.0 ,
	5806.8 ,		5241.1 ,	566.2 ,	3.9985
920		0.79 ,	41000.0 ,		26.0 ,
	6256.7 ,		5448.5 ,	672.9 ,	4.8879
921		0.79 ,	41000.0 ,		30.0 ,
	7203.5 ,		5856.5 ,	909.4 ,	6.6888

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

922		0.79 ,	41000.0 ,		34.0 ,
	8096.2 ,		6210.4 ,	1158.0 ,	8.2594
923		0.79 ,	41000.0 ,		38.0 ,
	8961.4 ,		6536.8 ,	1417.5 ,	10.2694
924		0.79 ,	41000.0 ,		42.0 ,
	9810.0 ,		6846.6 ,	1679.3 ,	11.621
925		0.79 ,	41000.0 ,		46.0 ,
	10639.2 ,		7136.9 ,	1952.5 ,	12.8649
926		0.79 ,	41000.0 ,		48.0 ,
	11044.2 ,		7272.6 ,	2096.9 ,	13.4762
927		0.79 ,	41000.0 ,		50.0 ,
	11447.3 ,		7406.3 ,	2241.1 ,	14.0615
928		0.8 ,	20000.0 ,		21.0 ,
	13631.6 ,		13101.2 ,	1071.7 ,	7.2066
929		0.8 ,	20000.0 ,		22.0 ,
	14277.9 ,		13429.2 ,	1206.9 ,	7.9564
930		0.8 ,	20000.0 ,		24.0 ,
	15511.1 ,		14025.9 ,	1505.6 ,	9.4413
931		0.8 ,	20000.0 ,		26.0 ,
	16688.8 ,		14567.1 ,	1810.3 ,	11.3981
932		0.8 ,	20000.0 ,		30.0 ,
	19165.5 ,		15629.4 ,	2495.5 ,	14.1535
933		0.8 ,	20000.0 ,		34.0 ,
	21509.9 ,		16559.4 ,	3213.1 ,	16.5599
934		0.8 ,	20000.0 ,		38.0 ,
	23783.7 ,		17418.7 ,	3966.3 ,	18.6886
935		0.8 ,	20000.0 ,		42.0 ,
	26016.0 ,		18236.5 ,	4721.8 ,	20.5452
936		0.8 ,	20000.0 ,		46.0 ,
	28194.2 ,		19000.4 ,	5512.1 ,	35.7201
937		0.8 ,	20000.0 ,		48.0 ,
	29257.3 ,		19356.5 ,	5932.0 ,	49.6781
938		0.8 ,	20000.0 ,		50.0 ,
	30313.1 ,		19704.9 ,	6356.8 ,	59.9573
939		0.8 ,	25000.0 ,		21.0 ,
	11000.5 ,		10572.8 ,	858.4 ,	5.7369
940		0.8 ,	25000.0 ,		22.0 ,
	11522.8 ,		10838.4 ,	964.5 ,	6.4424
941		0.8 ,	25000.0 ,		24.0 ,
	12518.5 ,		11320.9 ,	1199.4 ,	7.8407

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

942		0.8 ,	25000.0 ,		26.0 ,
	13468.9 ,		11757.9 ,	1438.7 ,	9.0737
943		0.8 ,	25000.0 ,		30.0 ,
	15468.6 ,		12617.0 ,	1976.9 ,	12.1112
944		0.8 ,	25000.0 ,		34.0 ,
	17361.2 ,		13369.0 ,	2541.0 ,	14.3696
945		0.8 ,	25000.0 ,		38.0 ,
	19196.7 ,		14063.9 ,	3132.5 ,	16.3657
946		0.8 ,	25000.0 ,		42.0 ,
	20998.4 ,		14725.0 ,	3725.7 ,	18.1043
947		0.8 ,	25000.0 ,		46.0 ,
	22756.7 ,		15342.6 ,	4346.4 ,	19.7156
948		0.8 ,	25000.0 ,		48.0 ,
	23614.9 ,		15630.5 ,	4675.4 ,	22.8123
949		0.8 ,	25000.0 ,		50.0 ,
	24467.2 ,		15912.5 ,	5007.9 ,	31.4463
950		0.8 ,	30000.0 ,		21.0 ,
	8794.9 ,		8453.1 ,	684.4 ,	4.8251
951		0.8 ,	30000.0 ,		22.0 ,
	9212.8 ,		8666.0 ,	766.2 ,	4.9546
952		0.8 ,	30000.0 ,		24.0 ,
	10009.9 ,		9052.9 ,	949.1 ,	6.2683
953		0.8 ,	30000.0 ,		26.0 ,
	10770.5 ,		9403.4 ,	1135.9 ,	7.4268
954		0.8 ,	30000.0 ,		30.0 ,
	12370.4 ,		10092.0 ,	1554.2 ,	9.6026
955		0.8 ,	30000.0 ,		34.0 ,
	13884.6 ,		10694.7 ,	1993.0 ,	12.2194
956		0.8 ,	30000.0 ,		38.0 ,
	15352.8 ,		11251.5 ,	2452.3 ,	14.0807
957		0.8 ,	30000.0 ,		42.0 ,
	16793.7 ,		11781.1 ,	2913.8 ,	15.7013
958		0.8 ,	30000.0 ,		46.0 ,
	18200.3 ,		12276.3 ,	3395.6 ,	17.2013
959		0.8 ,	30000.0 ,		48.0 ,
	18886.8 ,		12507.0 ,	3651.1 ,	17.9402
960		0.8 ,	30000.0 ,		50.0 ,
	19569.5 ,		12734.0 ,	3908.4 ,	18.6521
961		0.8 ,	35000.0 ,		21.0 ,
	6959.9 ,		6689.4 ,	543.4 ,	7.8502

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

962		0.8,	35000.0,		22.0,	
	7291.5,		6858.8,	606.0,		6.339
963		0.8,	35000.0,		24.0,	
	7923.7,		7166.4,	746.6,		4.7559
964		0.8,	35000.0,		26.0,	
	8526.5,		7444.7,	890.7,		5.8442
965		0.8,	35000.0,		30.0,	
	9794.9,		7991.8,	1212.3,		7.8493
966		0.8,	35000.0,		34.0,	
	10994.6,		8470.3,	1549.7,		9.9967
967		0.8,	35000.0,		38.0,	
	12158.1,		8912.6,	1902.7,		11.8951
968		0.8,	35000.0,		42.0,	
	13299.6,		9332.9,	2257.9,		13.4031
969		0.8,	35000.0,		46.0,	
	14413.9,		9725.9,	2628.2,		14.7963
970		0.8,	35000.0,		48.0,	
	14958.1,		9909.5,	2824.3,		15.483
971		0.8,	35000.0,		50.0,	
	15499.3,		10090.1,	3020.9,		16.1418
972		0.8,	37000.0,		21.0,	
	6319.9,		6074.2,	497.4,		8.3849
973		0.8,	37000.0,		22.0,	
	6621.5,		6228.4,	553.7,		6.9012
974		0.8,	37000.0,		24.0,	
	7196.4,		6508.4,	680.6,		4.3469
975		0.8,	37000.0,		26.0,	
	7744.3,		6761.5,	810.7,		5.4024
976		0.8,	37000.0,		30.0,	
	8897.5,		7259.4,	1100.8,		7.3437
977		0.8,	37000.0,		34.0,	
	9988.0,		7694.8,	1405.5,		9.0829
978		0.8,	37000.0,		38.0,	
	11045.4,		8096.9,	1723.9,		11.2241
979		0.8,	37000.0,		42.0,	
	12082.7,		8479.1,	2044.4,		12.6821
980		0.8,	37000.0,		46.0,	
	13095.6,		8836.7,	2378.8,		14.0299
981		0.8,	37000.0,		48.0,	
	13590.1,		9003.6,	2555.9,		14.6924

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

982		0.8 ,	37000.0 ,		50.0 ,
	14082.1 ,		9167.9 ,	2733.1 ,	15.3273
983		0.8 ,	39000.0 ,		21.0 ,
	5736.6 ,		5513.4 ,	458.1 ,	8.1251
984		0.8 ,	39000.0 ,		22.0 ,
	6011.0 ,		5653.8 ,	509.0 ,	6.6908
985		0.8 ,	39000.0 ,		24.0 ,
	6533.9 ,		5908.8 ,	624.2 ,	4.1644
986		0.8 ,	39000.0 ,		26.0 ,
	7032.1 ,		6139.1 ,	742.6 ,	5.1849
987		0.8 ,	39000.0 ,		30.0 ,
	8080.3 ,		6592.0 ,	1005.9 ,	7.0545
988		0.8 ,	39000.0 ,		34.0 ,
	9071.6 ,		6988.0 ,	1282.5 ,	8.7133
989		0.8 ,	39000.0 ,		38.0 ,
	10032.7 ,		7353.7 ,	1571.6 ,	10.789
990		0.8 ,	39000.0 ,		42.0 ,
	10975.1 ,		7701.0 ,	1862.9 ,	12.1943
991		0.8 ,	39000.0 ,		46.0 ,
	11895.7 ,		8026.0 ,	2166.6 ,	13.4902
992		0.8 ,	39000.0 ,		48.0 ,
	12345.1 ,		8177.9 ,	2327.3 ,	14.1257
993		0.8 ,	39000.0 ,		50.0 ,
	12792.3 ,		8327.3 ,	2488.0 ,	14.7358
994		0.8 ,	41000.0 ,		21.0 ,
	5206.8 ,		5004.0 ,	422.5 ,	7.8759
995		0.8 ,	41000.0 ,		22.0 ,
	5456.4 ,		5131.9 ,	468.7 ,	6.4921
996		0.8 ,	41000.0 ,		24.0 ,
	5932.1 ,		5364.1 ,	573.0 ,	3.9876
997		0.8 ,	41000.0 ,		26.0 ,
	6385.0 ,		5573.6 ,	680.6 ,	4.9727
998		0.8 ,	41000.0 ,		30.0 ,
	7338.1 ,		5985.7 ,	919.7 ,	6.7752
999		0.8 ,	41000.0 ,		34.0 ,
	8239.2 ,		6346.0 ,	1170.8 ,	8.3569
1000		0.8 ,	41000.0 ,		38.0 ,
	9112.8 ,		6678.6 ,	1433.3 ,	10.3696
1001		0.8 ,	41000.0 ,		42.0 ,
	9969.4 ,		6994.3 ,	1697.9 ,	11.7243

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

1002		0.8,	41000.0,		46.0,
	10805.8,		7289.8,	1973.9,	12.9692
1003		0.8,	41000.0,		48.0,
	11214.3,		7427.8,	2119.8,	13.581
1004		0.8,	41000.0,		50.0,
	11620.8,		7563.8,	2265.5,	14.1666
1005		0.8,	43000.0,		21.0,
	4725.6,		4541.3,	390.2,	7.6384
1006		0.8,	43000.0,		22.0,
	4952.6,		4657.7,	432.1,	6.3043
1007		0.8,	43000.0,		24.0,
	5385.5,		4869.4,	526.6,	3.8166
1008		0.8,	43000.0,		26.0,
	5797.4,		5060.1,	624.5,	4.7702
1009		0.8,	43000.0,		30.0,
	6664.0,		5435.0,	841.4,	6.5063
1010		0.8,	43000.0,		34.0,
	7483.3,		5762.9,	1069.3,	8.0181
1011		0.8,	43000.0,		38.0,
	8277.5,		6065.4,	1307.7,	9.9658
1012		0.8,	43000.0,		42.0,
	9055.9,		6352.3,	1548.6,	11.2718
1013		0.8,	43000.0,		46.0,
	9816.3,		6621.1,	1799.0,	12.4684
1014		0.8,	43000.0,		48.0,
	10187.6,		6746.6,	1931.5,	13.0575
1015		0.8,	43000.0,		50.0,
	10556.9,		6870.2,	2063.5,	13.6188
1016		0.85,	20000.0,		21.0,
	15269.7,		14726.9,	1148.4,	7.7963
1017		0.85,	20000.0,		22.0,
	15940.5,		15071.8,	1286.4,	8.5229
1018		0.85,	20000.0,		24.0,
	17216.3,		15696.2,	1605.0,	10.037
1019		0.85,	20000.0,		26.0,
	18437.2,		16265.7,	1923.0,	12.0458
1020		0.85,	20000.0,		30.0,
	21018.2,		17399.0,	2650.6,	14.837
1021		0.85,	20000.0,		34.0,
	23493.4,		18426.4,	3408.9,	17.2645

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

1022		0.85 ,	20000.0 ,		38.0 ,
	25884.8 ,		19370.2 ,	4206.9 ,	19.4142
1023		0.85 ,	20000.0 ,		42.0 ,
	28229.3 ,		20267.0 ,	5007.6 ,	23.7977
1024		0.85 ,	20000.0 ,		46.0 ,
	30511.4 ,		21101.3 ,	5843.9 ,	46.826
1025		0.85 ,	20000.0 ,		48.0 ,
	31623.3 ,		21489.2 ,	6287.4 ,	58.5793
1026		0.85 ,	20000.0 ,		50.0 ,
	32726.4 ,		21868.7 ,	6737.1 ,	67.2902
1027		0.85 ,	25000.0 ,		21.0 ,
	12322.9 ,		11885.2 ,	918.3 ,	6.2921
1028		0.85 ,	25000.0 ,		22.0 ,
	12864.9 ,		12164.6 ,	1027.0 ,	6.9769
1029		0.85 ,	25000.0 ,		24.0 ,
	13894.8 ,		12669.2 ,	1277.4 ,	8.3905
1030		0.85 ,	25000.0 ,		26.0 ,
	14880.2 ,		13129.4 ,	1527.5 ,	9.6187
1031		0.85 ,	25000.0 ,		30.0 ,
	16963.6 ,		14045.5 ,	2098.8 ,	12.7509
1032		0.85 ,	25000.0 ,		34.0 ,
	18961.6 ,		14876.3 ,	2695.0 ,	15.0269
1033		0.85 ,	25000.0 ,		38.0 ,
	20891.7 ,		15639.3 ,	3321.4 ,	17.0425
1034		0.85 ,	25000.0 ,		42.0 ,
	22783.5 ,		16363.9 ,	3949.4 ,	18.7996
1035		0.85 ,	25000.0 ,		46.0 ,
	24625.9 ,		17039.0 ,	4606.3 ,	21.7264
1036		0.85 ,	25000.0 ,		48.0 ,
	25523.3 ,		17352.8 ,	4953.5 ,	29.2527
1037		0.85 ,	25000.0 ,		50.0 ,
	26413.9 ,		17659.8 ,	5304.8 ,	41.448
1038		0.85 ,	30000.0 ,		21.0 ,
	9852.7 ,		9503.0 ,	730.5 ,	4.817
1039		0.85 ,	30000.0 ,		22.0 ,
	10286.3 ,		9726.8 ,	814.8 ,	5.4569
1040		0.85 ,	30000.0 ,		24.0 ,
	11110.8 ,		10131.7 ,	1009.8 ,	6.7844
1041		0.85 ,	30000.0 ,		26.0 ,
	11899.3 ,		10500.5 ,	1204.7 ,	7.9341

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

1042		0.85 ,	30000.0 ,		30.0 ,
	13566.3 ,		11234.9 ,	1649.0 ,	10.6836
1043		0.85 ,	30000.0 ,		34.0 ,
	15164.4 ,		11900.5 ,	2112.4 ,	12.8292
1044		0.85 ,	30000.0 ,		38.0 ,
	16708.5 ,		12512.1 ,	2599.3 ,	14.7084
1045		0.85 ,	30000.0 ,		42.0 ,
	18221.3 ,		13092.4 ,	3087.7 ,	16.346
1046		0.85 ,	30000.0 ,		46.0 ,
	19695.1 ,		13633.6 ,	3597.6 ,	17.8596
1047		0.85 ,	30000.0 ,		48.0 ,
	20413.3 ,		13885.5 ,	3867.4 ,	18.6028
1048		0.85 ,	30000.0 ,		50.0 ,
	21126.4 ,		14132.3 ,	4139.7 ,	19.3169
1049		0.85 ,	35000.0 ,		21.0 ,
	7797.5 ,		7520.8 ,	578.7 ,	6.6087
1050		0.85 ,	35000.0 ,		22.0 ,
	8141.8 ,		7699.1 ,	643.4 ,	5.1541
1051		0.85 ,	35000.0 ,		24.0 ,
	8795.7 ,		8020.9 ,	793.4 ,	5.2408
1052		0.85 ,	35000.0 ,		26.0 ,
	9420.6 ,		8313.7 ,	943.8 ,	6.3186
1053		0.85 ,	35000.0 ,		30.0 ,
	10741.8 ,		8897.0 ,	1284.8 ,	8.3419
1054		0.85 ,	35000.0 ,		34.0 ,
	12008.4 ,		9425.6 ,	1641.7 ,	10.725
1055		0.85 ,	35000.0 ,		38.0 ,
	13232.1 ,		9911.4 ,	2016.1 ,	12.4766
1056		0.85 ,	35000.0 ,		42.0 ,
	14430.9 ,		10372.2 ,	2391.9 ,	13.999
1057		0.85 ,	35000.0 ,		46.0 ,
	15598.6 ,		10802.0 ,	2783.9 ,	15.4058
1058		0.85 ,	35000.0 ,		48.0 ,
	16167.5 ,		11002.0 ,	2990.7 ,	16.095
1059		0.85 ,	35000.0 ,		50.0 ,
	16732.6 ,		11198.0 ,	3199.2 ,	16.7582
1060		0.85 ,	37000.0 ,		21.0 ,
	7080.7 ,		6829.3 ,	529.2 ,	7.1696
1061		0.85 ,	37000.0 ,		22.0 ,
	7393.9 ,		6991.7 ,	587.4 ,	5.7449

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

1062		0.85 ,	37000.0 ,		24.0 ,	
	7988.5 ,		7284.6 ,	722.8 ,		4.8169
1063		0.85 ,	37000.0 ,		26.0 ,	
	8556.5 ,		7551.0 ,	858.6 ,		5.8624
1064		0.85 ,	37000.0 ,		30.0 ,	
	9757.7 ,		8081.8 ,	1166.5 ,		7.8217
1065		0.85 ,	37000.0 ,		34.0 ,	
	10908.7 ,		8562.5 ,	1488.5 ,		10.0732
1066		0.85 ,	37000.0 ,		38.0 ,	
	12020.9 ,		9004.3 ,	1826.1 ,		11.7857
1067		0.85 ,	37000.0 ,		42.0 ,	
	13110.2 ,		9423.3 ,	2165.5 ,		13.2592
1068		0.85 ,	37000.0 ,		46.0 ,	
	14171.0 ,		9813.8 ,	2518.9 ,		14.6171
1069		0.85 ,	37000.0 ,		48.0 ,	
	14688.6 ,		9996.1 ,	2705.6 ,		15.2834
1070		0.85 ,	37000.0 ,		50.0 ,	
	15202.3 ,		10174.6 ,	2893.4 ,		15.9241
1071		0.85 ,	39000.0 ,		21.0 ,	
	6427.5 ,		6199.1 ,	487.0 ,		6.9546
1072		0.85 ,	39000.0 ,		22.0 ,	
	6712.2 ,		6346.7 ,	539.4 ,		5.589
1073		0.85 ,	39000.0 ,		24.0 ,	
	7253.1 ,		6613.6 ,	662.4 ,		4.6165
1074		0.85 ,	39000.0 ,		26.0 ,	
	7769.4 ,		6855.8 ,	785.8 ,		5.6258
1075		0.85 ,	39000.0 ,		30.0 ,	
	8861.3 ,		7338.7 ,	1065.5 ,		7.514
1076		0.85 ,	39000.0 ,		34.0 ,	
	9907.4 ,		7775.8 ,	1357.5 ,		9.6651
1077		0.85 ,	39000.0 ,		38.0 ,	
	10918.3 ,		8177.7 ,	1664.3 ,		11.3296
1078		0.85 ,	39000.0 ,		42.0 ,	
	11908.0 ,		8558.4 ,	1972.4 ,		12.7479
1079		0.85 ,	39000.0 ,		46.0 ,	
	12872.3 ,		8913.7 ,	2293.5 ,		14.056
1080		0.85 ,	39000.0 ,		48.0 ,	
	13342.3 ,		9079.2 ,	2463.0 ,		14.6952
1081		0.85 ,	39000.0 ,		50.0 ,	
	13809.4 ,		9241.8 ,	2633.5 ,		15.3107

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

1082		0.9 ,	35000.0 ,		21.0 ,	
	8689.9 ,		8405.4 ,	612.6 ,		5.4642
1083		0.9 ,	35000.0 ,		22.0 ,	
	9048.1 ,		8592.9 ,	681.7 ,		4.4604
1084		0.9 ,	35000.0 ,		24.0 ,	
	9727.3 ,		8930.8 ,	841.5 ,		5.7208
1085		0.9 ,	35000.0 ,		26.0 ,	
	10383.2 ,		9245.3 ,	999.3 ,		6.7969
1086		0.9 ,	35000.0 ,		30.0 ,	
	11785.1 ,		9888.5 ,	1365.6 ,		8.8636
1087		0.9 ,	35000.0 ,		34.0 ,	
	13126.8 ,		10471.6 ,	1745.1 ,		11.3302
1088		0.9 ,	35000.0 ,		38.0 ,	
	14418.8 ,		11005.1 ,	2142.8 ,		13.0965
1089		0.9 ,	35000.0 ,		42.0 ,	
	15682.3 ,		11509.9 ,	2543.0 ,		14.6396
1090		0.9 ,	35000.0 ,		46.0 ,	
	16909.5 ,		11978.5 ,	2959.3 ,		16.0593
1091		0.9 ,	35000.0 ,		48.0 ,	
	17506.0 ,		12195.7 ,	3179.8 ,		16.7568
1092		0.9 ,	35000.0 ,		50.0 ,	
	18098.7 ,		12409.1 ,	3401.9 ,		17.4262
1093		0.9 ,	37000.0 ,		21.0 ,	
	7891.3 ,		7632.9 ,	559.6 ,		6.0554
1094		0.9 ,	37000.0 ,		22.0 ,	
	8217.1 ,		7803.6 ,	621.9 ,		4.6273
1095		0.9 ,	37000.0 ,		24.0 ,	
	8834.9 ,		8111.3 ,	766.2 ,		5.2826
1096		0.9 ,	37000.0 ,		26.0 ,	
	9431.0 ,		8397.2 ,	908.7 ,		6.3254
1097		0.9 ,	37000.0 ,		30.0 ,	
	10705.5 ,		8982.6 ,	1239.4 ,		8.326
1098		0.9 ,	37000.0 ,		34.0 ,	
	11924.9 ,		9512.8 ,	1581.3 ,		10.6732
1099		0.9 ,	37000.0 ,		38.0 ,	
	13099.4 ,		9998.1 ,	1940.8 ,		12.3857
1100		0.9 ,	37000.0 ,		42.0 ,	
	14247.6 ,		10457.1 ,	2302.0 ,		13.878
1101		0.9 ,	37000.0 ,		46.0 ,	
	15363.1 ,		10883.5 ,	2678.2 ,		15.2518

PRELIMINARY SIZING OF HOMELAND DEFENSE INTERCEPTOR AIRCRAFT USING AVIARY

1102		0.9,	37000.0,	48.0,	
	15905.5,		11081.3,	2876.5,	15.9229
1103		0.9,	37000.0,	50.0,	
	16443.8,		11275.0,	3076.2,	16.5691
1104		0.9,	39000.0,	21.0,	
	7163.6,		6928.7,	514.4,	5.8837
1105		0.9,	39000.0,	22.0,	
	7459.9,		7084.2,	570.9,	4.5067
1106		0.9,	39000.0,	24.0,	
	8021.6,		7364.1,	701.6,	5.0624
1107		0.9,	39000.0,	26.0,	
	8563.7,		7624.5,	831.4,	6.0727
1108		0.9,	39000.0,	30.0,	
	9722.3,		8156.9,	1131.6,	7.9996
1109		0.9,	39000.0,	34.0,	
	10830.8,		8639.2,	1442.2,	10.2576
1110		0.9,	39000.0,	38.0,	
	11898.0,		9080.3,	1768.2,	11.9058
1111		0.9,	39000.0,	42.0,	
	12941.4,		9497.6,	2096.6,	13.3448
1112		0.9,	39000.0,	46.0,	
	13955.2,		9885.2,	2438.2,	14.6669
1113		0.9,	39000.0,	48.0,	
	14447.9,		10064.9,	2618.2,	15.3126
1114		0.9,	39000.0,	50.0,	
	14937.5,		10241.3,	2799.5,	15.9332

B.8 Aviary: DCA Patrol Mission

```

1 import aviary.api as av
2 from aviary.api import Aircraft, Mission
3
4
5
6 aircraft_filename = "models/test_aircraft/
   Intercepto1_Aircraft_FwFm.csv"
7 optimizer = "IPOPT"
8 analysis_scheme = av.AnalysisScheme.COLLOCATION
9 objective_type = None
10 record_filename = 'aviary_history.db'

```

```
11 restart_filename = None
12 max_iter = 5
13
14 phase_info = {
15     "pre_mission": {"include_takeoff": True, "optimize_mass": True
16 },
17     "climb": {
18         "subsystem_options": {"core_aerodynamics": {"method": "
19 computed"}},
20         "user_options": {
21             "optimize_mach": False,
22             "optimize_altitude": True,
23             "num_segments": 3,
24             "order": 3,
25             "solve_for_distance": True,
26             "initial_mach": (0.15, "unitless"),
27             "final_mach": (0.5, "unitless"),
28             "mach_bounds": ((0.0, 0.6), "unitless"),
29             "initial_altitude": (0.0, "ft"),
30             "final_altitude": (35000.0, "ft"),
31             "altitude_bounds": ((0.0, 40000.0), "ft"),
32             "throttle_enforcement": "path_constraint",
33             "fix_initial": True,
34             "constrain_final": False,
35             "fix_duration": False,
36             "initial_bounds": ((5.0, 15.0), "min"),
37             "duration_bounds": ((10.0, 30.0), "min"),
38             "add_initial_mass_constraint": False,
39         },
40     },
41     "cruise": {
42         "subsystem_options": {"core_aerodynamics": {"method": "
43 computed"}},
44         "user_options": {
45             "optimize_mach": False,
46             "optimize_altitude": True,
47             "num_segments": 10,
48             "order": 5,
49             "solve_for_distance": True,
50             "initial_mach": (0.5, "unitless"),
```

```
48         "final_mach": (0.78, "unitless"),
49         "mach_bounds": ((0.6, 0.8), "unitless"),
50         "initial_altitude": (35000.0, "ft"),
51         "final_altitude": (38000.0, "ft"),
52         "altitude_bounds": ((34000.0, 40000.0), "ft"),
53         "throttle_enforcement": "path_constraint",
54         "fix_initial": False,
55         "constrain_final": False,
56         "fix_duration": False,
57         "initial_bounds": ((15.0, 30.0), "min"),
58         "duration_bounds": ((40.0, 80.0), "min"),
59     },
60 },
61 # Combat Air-Patrol
62     "cruise_1": {
63         "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
64         "user_options": {
65             "optimize_mach": True,
66             "optimize_altitude": False,
67             "num_segments": 5,
68             "order": 5,
69             "solve_for_distance": False,
70             "initial_mach": (0.78, "unitless"),
71             "final_mach": (0.5, "unitless"),
72             "mach_bounds": ((0.4, 0.8), "unitless"),
73             "initial_altitude": (38000.0, "ft"),
74             "final_altitude": (35000.0, "ft"),
75             "altitude_bounds": ((34000.0, 38000.0), "ft"),
76             "throttle_enforcement": "path_constraint",
77             "fix_initial": True,
78             "constrain_final": True,
79             "fix_duration": True,
80             "initial_bounds": ((60.0, 200.0), "min"),
81             "duration_bounds": ((240.0, 240.0), "min"),
82         },
83     },
84 #Dash
85     "cruise_2": {
```

```
86     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}}},
87     "user_options": {
88         "optimize_mach": True,
89         "optimize_altitude": True,
90         "num_segments": 5,
91         "order": 3,
92         "solve_for_distance": False,
93         "initial_mach": (0.5, "unitless"),
94         "final_mach": (0.9, "unitless"),
95         "mach_bounds": ((0.4, 0.9), "unitless"),
96         "initial_altitude": (35000.0, "ft"),
97         "final_altitude": (35000.0, "ft"),
98         "altitude_bounds": ((35000.0, 35000.0), "ft"),
99         "throttle_enforcement": "path_constraint",
100        "fix_initial": False,
101        "constrain_final": False,
102        "fix_duration": False,
103        "initial_bounds": ((200, 260.0), "min"),
104        "duration_bounds": ((2.0, 5.0), "min"),
105    },
106 },
107
108 #Combat
109 "cruise_3": {
110     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}}},
111     "user_options": {
112         "optimize_mach": False,
113         "optimize_altitude": False,
114         "num_segments": 2,
115         "order": 3,
116         "solve_for_distance": False,
117         "initial_mach": (0.9, "unitless"),
118         "final_mach": (0.9, "unitless"),
119         "mach_bounds": ((0.9, 0.9), "unitless"),
120         "initial_altitude": (35000.0, "ft"),
121         "final_altitude": (35000.0, "ft"),
122         "altitude_bounds": ((35000.0, 35000.0), "ft"),
123         "throttle_enforcement": "path_constraint",
```

```
124         "fix_initial": False,
125         "constrain_final": False,
126         "fix_duration": False,
127         "initial_bounds": ((200.0, 250.0), "min"),
128         "duration_bounds": ((2.0, 2.0), "min"),
129     },
130 },
131
132 #Climb/accel
133 "climb_2": {
134     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
135     "user_options": {
136         "optimize_mach": True,
137         "optimize_altitude": False,
138         "num_segments": 5,
139         "order": 3,
140         "solve_for_distance": False,
141         "initial_mach": (0.9, "unitless"),
142         "final_mach": (0.78, "unitless"),
143         "mach_bounds": ((0.7, 0.9), "unitless"),
144         "initial_altitude": (35000.0, "ft"),
145         "final_altitude": (38000.0, "ft"),
146         "altitude_bounds": ((35000.0, 40000.0), "ft"),
147         "throttle_enforcement": "path_constraint",
148         "fix_initial": False,
149         "constrain_final": True,
150         "fix_duration": False,
151         "initial_bounds": ((180, 220.0), "min"),
152         "duration_bounds": ((5.0, 20.0), "min"),
153     },
154
155 },
156 "cruise_4": {
157     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
158     "user_options": {
159         "optimize_mach": True,
160         "optimize_altitude": True,
161         "num_segments": 10,
```

```
162         "order": 3,
163         "solve_for_distance": False,
164         "initial_mach": (0.78, "unitless"),
165         "final_mach": (0.8, "unitless"),
166         "mach_bounds": ((0.7, 0.9), "unitless"),
167         "initial_altitude": (38000.0, "ft"),
168         "final_altitude": (40000.0, "ft"),
169         "altitude_bounds": ((35000.0, 40000.0), "ft"),
170         "throttle_enforcement": "path_constraint",
171         "fix_initial": False,
172         "constrain_final": True,
173         "fix_duration": False,
174         "initial_bounds": ((250.0, 300.0), "min"),
175         "duration_bounds": ((40.0, 80.0), "min"),
176     },
177 },
178 "descent": {
179     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
180     "user_options": {
181         "optimize_mach": False,
182         "optimize_altitude": False,
183         "num_segments": 5,
184         "order": 3,
185         "solve_for_distance": False,
186         "initial_mach": (0.8, "unitless"),
187         "final_mach": (0.25, "unitless"),
188         "mach_bounds": ((0.1, 0.8), "unitless"),
189         "initial_altitude": (40000.0, "ft"),
190         "final_altitude": (500.0, "ft"),
191         "altitude_bounds": ((0.0, 45000.0), "ft"),
192         "throttle_enforcement": "path_constraint",
193         "fix_initial": False,
194         "constrain_final": True,
195         "fix_duration": False,
196         "initial_bounds": ((300.0, 320.0), "min"),
197         "duration_bounds": ((10.0, 20.0), "min"),
198     },
199
200 }
```

```
201     "post_mission": {
202         "include_landing": False,
203         "constrain_range": True,
204         "target_range": (800, "nmi"),
205     },
206 }
207
208 prob = av.AviaryProblem(analysis_scheme)
209
210 # Load aircraft and options data from user
211 # Allow for user overrides here
212 prob.load_inputs(aircraft_filename, phase_info)
213
214 prob.check_and_preprocess_inputs()
215
216 prob.add_pre_mission_systems()
217
218 prob.add_phases()
219
220 prob.add_post_mission_systems()
221
222 # Link phases and variables
223 prob.link_phases()
224
225 prob.add_driver(optimizer, max_iter=max_iter)
226
227
228 prob.model.add_design_var(av.Mission.Design.GROSS_MASS, units='lbm
229     ',
230                           lower=32000, upper=37000.0, ref=36733)
231 prob.model.add_design_var(av.Aircraft.Wing.AREA, units='ft**2',
232                           lower=400, upper=500, ref=445.03)
233 prob.model.add_design_var(av.Aircraft.Wing.SPAN, units='ft',
234                           lower=42, upper=50, ref=42.08)
235 prob.model.add_design_var(av.Mission.Design.RANGE, units='NM',
236                           lower=500, upper=800, ref=1000)
237 prob.model.add_design_var(av.Aircraft.Wing.ASPECT_RATIO,
238                           lower=3, upper=5, ref=3.98)
239 prob.model.add_design_var(av.Aircraft.HorizontalTail.AREA, units="
240     ft**2",
```

```
239         lower=150, upper=160, ref=153.46)
240 prob.model.add_design_var(av.Aircraft.VerticalTail.AREA, units="ft
    **2",
241         lower=50, upper=55, ref=53.9)
242 prob.model.add_design_var(av.Mission.Takeoff.LIFT_OVER_DRAG,
243         lower=3, upper=5, ref=3.5)
244 prob.model.add_design_var(av.Mission.Takeoff.LIFT_COEFFICIENT_MAX,
245         lower=1.6, upper=2, ref=1.8)
246 prob.model.add_design_var(av.Mission.Landing.LIFT_COEFFICIENT_MAX,
247         lower=1.8, upper=2.5, ref=2.2)
248 prob.add_objective(objective_type=objective_type)
249
250 prob.setup()
251
252 prob.set_initial_guesses()
253
254 prob.run_aviary_problem(record_filename, restart_filename=
    restart_filename)
255
256 print('-----')
257 print('Sizing Results')
258 print('-----')
259 print(f'Design Range = {prob.get_val(av.Mission.Design.RANGE,
    units="NM")}')
260 print(f'Summary Range = {prob.get_val(av.Mission.Summary.RANGE,
    units="NM")}')
261 print(f'Total fuel capacity = {prob.get_val(av.Aircraft.Fuel.
    TOTAL_CAPACITY, units="lbm")}')
262 print(f'Empty mass = {prob.get_val(av.Aircraft.Design.
    OPERATING_MASS, units="lbm")}')
263 print(f'Total Payload mass = {prob.get_val(av.Aircraft.CrewPayload.
    TOTAL_PAYLOAD_MASS, units="lbm")}')
264 print(f'Design Gross mass = {prob.get_val(av.Mission.Design.
    GROSS_MASS, units="lbm")}')
265 print(f'Summary Gross mass = {prob.get_val(av.Mission.Summary.
    GROSS_MASS, units="lbm")}')
266 print(f'Wing Area = {prob.get_val(av.Aircraft.Wing.AREA, units="ft
    **2")}')
267 print(f'Wing Span = {prob.get_val(av.Aircraft.Wing.SPAN, units="ft
    ")}')
```

```
268 print(f'Aspect Ratio = {prob.get_val(av.Aircraft.Wing.ASPECT_RATIO
    )}')
269 print(f'HT Area = {prob.get_val(av.Aircraft.HorizontalTail.AREA,
    units="ft**2")}')
270 print(f'VT Area = {prob.get_val(av.Aircraft.VerticalTail.AREA,
    units="ft**2")}')
271 print(f'Takeoff L/D = {prob.get_val(av.Mission.Takeoff.
    LIFT_OVER_DRAG)}')
272 print(f'Takeoff Clmax = {prob.get_val(av.Mission.Takeoff.
    LIFT_COEFFICIENT_MAX)}')
273 print(f'Landing Clmax = {prob.get_val(av.Mission.Landing.
    LIFT_COEFFICIENT_MAX)}')
```

B.9 Aviary: PDI Mission

```
1 import aviary.api as av
2 from aviary.api import Aircraft, Mission
3
4
5
6 aircraft_filename = "models/test_aircraft/
    Interceptor1_Aircraft_FwFm.csv"
7 optimizer = "IPOPT"
8 analysis_scheme = av.AnalysisScheme.COLLOCATION
9 objective_type = None
10 record_filename = 'aviary_history.db'
11 restart_filename = None
12 max_iter = 5
13
14 phase_info = {
15     "pre_mission": {"include_takeoff": True, "optimize_mass": True
16 },
17     "climb": {
18         "subsystem_options": {"core_aerodynamics": {"method": "
19         computed"}},
20         "user_options": {
21             "optimize_mach": False,
22             "optimize_altitude": False,
23             "num_segments": 5,
24             "order": 3,
```

```
23         "solve_for_distance": False,
24         "initial_mach": (0.2, "unitless"),
25         "final_mach": (0.8, "unitless"),
26         "mach_bounds": ((0.1, 0.9), "unitless"),
27         "initial_altitude": (0.0, "ft"),
28         "final_altitude": (35000.0, "ft"),
29         "altitude_bounds": ((0.0, 35000.0), "ft"),
30         "throttle_enforcement": "path_constraint",
31         "fix_initial": True,
32         "constrain_final": False,
33         "fix_duration": False,
34         "initial_bounds": ((4.0, 20.0), "min"),
35         "duration_bounds": ((15.0, 35.0), "min"),
36         "add_initial_mass_constraint": False,
37     },
38 },
39 #dash
40 "cruise": {
41     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
42     "user_options": {
43         "optimize_mach": False,
44         "optimize_altitude": False,
45         "num_segments": 5,
46         "order": 3,
47         "solve_for_distance": False,
48         "initial_mach": (0.8, "unitless"),
49         "final_mach": (0.9, "unitless"),
50         "mach_bounds": ((0.8, 0.9), "unitless"),
51         "initial_altitude": (35000.0, "ft"),
52         "final_altitude": (35000.0, "ft"),
53         "altitude_bounds": ((35000.0, 35000.0), "ft"),
54         "throttle_enforcement": "boundary_constraint",
55         "fix_initial": False,
56         "constrain_final": False,
57         "fix_duration": False,
58         "initial_bounds": ((10.0, 20.0), "min"),
59         "duration_bounds": ((15.0, 25.0), "min"),
60     },
61 },
```

```
62     #combat
63     "cruise_1": {
64         "subsystem_options": {"core_aerodynamics": {"method": "
65         computed"}},
66         "user_options": {
67             "optimize_mach": False,
68             "optimize_altitude": False,
69             "num_segments": 5,
70             "order": 3,
71             "solve_for_distance": False,
72             "initial_mach": (0.9, "unitless"),
73             "final_mach": (0.9, "unitless"),
74             "mach_bounds": ((0.85, 0.95), "unitless"),
75             "initial_altitude": (35000.0, "ft"),
76             "final_altitude": (35000.0, "ft"),
77             "altitude_bounds": ((34000.0, 36000.0), "ft"),
78             "throttle_enforcement": "boundary_constraint",
79             "fix_initial": False,
80             "constrain_final": False,
81             "fix_duration": False,
82             "initial_bounds": ((5.0, 15.0), "min"),
83             "duration_bounds": ((5.0, 10.0), "min")
84         },
85     },
86     # climb/Accel
87     "cruise_2": {
88         "subsystem_options": {"core_aerodynamics": {"method": "
89         computed"}},
90         "user_options": {
91             "optimize_mach": True,
92             "optimize_altitude": True,
93             "num_segments": 10,
94             "order": 3,
95             "solve_for_distance": False,
96             "initial_mach": (0.9, "unitless"),
97             "final_mach": (0.78, "unitless"),
98             "mach_bounds": ((0.7, 0.9), "unitless"),
99             "initial_altitude": (35000.0, "ft"),
100            "final_altitude": (40000.0, "ft"),
101            "altitude_bounds": ((34000.0, 42000.0), "ft"),
```

```
100         "throttle_enforcement": "path_constraint",
101         "fix_initial": False,
102         "constrain_final": False,
103         "fix_duration": False,
104         "initial_bounds": ((5.0, 10.0), "min"),
105         "duration_bounds": ((5.0, 15.0), "min")
106     },
107 },
108     "cruise_3": {
109         "subsystem_options": {"core_aerodynamics": {"method": "
110 computed"}},
111         "user_options": {
112             "optimize_mach": True,
113             "optimize_altitude": True,
114             "num_segments": 10,
115             "order": 3,
116             "solve_for_distance": False,
117             "initial_mach": (0.6, "unitless"),
118             "final_mach": (0.6, "unitless"),
119             "mach_bounds": ((0.5, 0.7), "unitless"),
120             "initial_altitude": (40000.0, "ft"),
121             "final_altitude": (34000.0, "ft"),
122             "altitude_bounds": ((33000.0, 40000.0), "ft"),
123             "throttle_enforcement": "boundary_constraint",
124             "fix_initial": False,
125             "constrain_final": False,
126             "fix_duration": False,
127             "initial_bounds": ((60.0, 100.0), "min"),
128             "duration_bounds": ((100.0, 200.0), "min")
129         },
130     },
131     "descent": {
132         "subsystem_options": {"core_aerodynamics": {"method": "
133 computed"}},
134         "user_options": {
135             "optimize_mach": False,
136             "optimize_altitude": False,
137             "num_segments": 5,
138             "order": 3,
139             "solve_for_distance": False,
```

```
138         "initial_mach": (0.7, "unitless"),
139         "final_mach": (0.5, "unitless"),
140         "mach_bounds": ((0.4, 0.8), "unitless"),
141         "initial_altitude": (34000.0, "ft"),
142         "final_altitude": (500.0, "ft"),
143         "altitude_bounds": ((0.0, 35000.0), "ft"),
144         "throttle_enforcement": "path_constraint",
145         "fix_initial": False,
146         "constrain_final": True,
147         "fix_duration": False,
148         "initial_bounds": ((5.0, 15.0), "min"),
149         "duration_bounds": ((15.0, 30.0), "min")
150     },
151 },
152 "post_mission": {
153     "include_landing": False,
154     "constrain_range": True,
155     "target_range": (500, "nmi"),
156 },
157 }
158
159 prob = av.AviaryProblem(analysis_scheme)
160
161 # Load aircraft and options data from user
162 # Allow to overrides here
163 prob.load_inputs(aircraft_filename, phase_info)
164
165 prob.check_and_preprocess_inputs()
166
167 prob.add_pre_mission_systems()
168
169 prob.add_phases()
170
171 prob.add_post_mission_systems()
172
173 # Link phases and variables
174 prob.link_phases()
175
176 prob.add_driver(optimizer, max_iter=max_iter)
177
```

```
178
179 prob.model.add_design_var(av.Mission.Design.GROSS_MASS, units='lbm
    ',
180                               lower=32000, upper=37000.0, ref=36733)
181 prob.model.add_design_var(av.Aircraft.Wing.AREA, units='ft**2',
182                               lower=400, upper=500, ref=445.03)
183 prob.model.add_design_var(av.Aircraft.Wing.SPAN, units='ft',
184                               lower=42, upper=50, ref=42.08)
185 prob.model.add_design_var(av.Mission.Design.RANGE, units='NM',
186                               lower=500, upper=800, ref=1000)
187 prob.model.add_design_var(av.Aircraft.Wing.ASPECT_RATIO,
188                               lower=3, upper=5, ref=3.98)
189 prob.model.add_design_var(av.Aircraft.HorizontalTail.AREA, units="
    ft**2",
190                               lower=150, upper=160, ref=153.46)
191 prob.model.add_design_var(av.Aircraft.VerticalTail.AREA, units="ft
    **2",
192                               lower=50, upper=55, ref=53.9)
193 prob.model.add_design_var(av.Mission.Takeoff.LIFT_OVER_DRAG,
194                               lower=3, upper=5, ref=3.5)
195 prob.model.add_design_var(av.Mission.Takeoff.LIFT_COEFFICIENT_MAX,
196                               lower=1.6, upper=2, ref=1.8)
197 prob.model.add_design_var(av.Mission.Landing.LIFT_COEFFICIENT_MAX,
198                               lower=1.8, upper=2.5, ref=2.2)
199 prob.add_objective(objective_type=objective_type)
200
201 prob.setup()
202
203 prob.set_initial_guesses()
204
205 prob.run_aviary_problem(record_filename, restart_filename=
    restart_filename)
206
207 print('-----')
208 print('Sizing Results')
209 print('-----')
210 print(f'Design Range = {prob.get_val(av.Mission.Design.RANGE,
    units="NM")}')
211 print(f'Summary Range = {prob.get_val(av.Mission.Summary.RANGE,
    units="NM")}')
```

```
212 print(f'Total fuel capacity = {prob.get_val(av.Aircraft.Fuel.  
    TOTAL_CAPACITY, units="lbm")}')  
213 print(f'Empty mass = {prob.get_val(av.Aircraft.Design.  
    OPERATING_MASS, units="lbm")}')  
214 print(f'Total Payload mass = {prob.get_val(av.Aircraft.CrewPayload.  
    TOTAL_PAYLOAD_MASS, units="lbm")}')  
215 print(f'Design Gross mass = {prob.get_val(av.Mission.Design.  
    GROSS_MASS, units="lbm")}')  
216 print(f'Summary Gross mass = {prob.get_val(av.Mission.Summary.  
    GROSS_MASS, units="lbm")}')  
217 print(f'Wing Area = {prob.get_val(av.Aircraft.Wing.AREA, units="ft  
    **2")}')  
218 print(f'Wing Span = {prob.get_val(av.Aircraft.Wing.SPAN, units="ft  
    ")}')  
219 print(f'Aspect Ratio = {prob.get_val(av.Aircraft.Wing.ASPECT_RATIO  
    )}')  
220 print(f'HT Area = {prob.get_val(av.Aircraft.HorizontalTail.AREA,  
    units="ft**2")}')  
221 print(f'VT Area = {prob.get_val(av.Aircraft.VerticalTail.AREA,  
    units="ft**2")}')  
222 print(f'Takeoff L/D = {prob.get_val(av.Mission.Takeoff.  
    LIFT_OVER_DRAG)}')  
223 print(f'Takeoff Clmax = {prob.get_val(av.Mission.Takeoff.  
    LIFT_COEFFICIENT_MAX)}')  
224 print(f'Landing Clmax = {prob.get_val(av.Mission.Landing.  
    LIFT_COEFFICIENT_MAX)}')
```

B.10 Aviary: Escort Mission

```
1 import aviary.api as av  
2 from aviary.api import Aircraft, Mission  
3  
4  
5  
6 aircraft_filename = "models/test_aircraft/  
    Interceptor_Aircraft_FwFm.csv"  
7 optimizer = "IPOPT"  
8 analysis_scheme = av.AnalysisScheme.COLLOCATION  
9 objective_type = None  
10 record_filename = 'aviary_history.db'
```

```
11 restart_filename = None
12 max_iter = 5
13
14 phase_info = {
15     "pre_mission": {"include_takeoff": True, "optimize_mass": True
16 },
17     "climb": {
18         "subsystem_options": {"core_aerodynamics": {"method": "
19 computed"}},
20         "user_options": {
21             "optimize_mach": False,
22             "optimize_altitude": False,
23             "num_segments": 10,
24             "order": 3,
25             "solve_for_distance": False,
26             "initial_mach": (0.2, "unitless"),
27             "final_mach": (0.8, "unitless"),
28             "mach_bounds": ((0.1, 0.9), "unitless"),
29             "initial_altitude": (0.0, "ft"),
30             "final_altitude": (35000.0, "ft"),
31             "altitude_bounds": ((0.0, 40000.0), "ft"),
32             "throttle_enforcement": "path_constraint",
33             "fix_initial": True,
34             "constrain_final": False,
35             "fix_duration": False,
36             "initial_bounds": ((4.0, 20.0), "min"),
37             "duration_bounds": ((15.0, 35.0), "min"),
38             "add_initial_mass_constraint": False,
39         },
40     },
41     #dash
42     "cruise": {
43         "subsystem_options": {"core_aerodynamics": {"method": "
44 computed"}},
45         "user_options": {
46             "optimize_mach": False,
47             "optimize_altitude": False,
48             "num_segments": 10,
49             "order": 3,
50             "solve_for_distance": False,
```

```
48         "initial_mach": (0.8, "unitless"),
49         "final_mach": (0.9, "unitless"),
50         "mach_bounds": ((0.8, 0.9), "unitless"),
51         "initial_altitude": (35000.0, "ft"),
52         "final_altitude": (35000.0, "ft"),
53         "altitude_bounds": ((30000.0, 40000.0), "ft")
initial_bounds": ((60.0, 100.0), "min"),
54         "duration_bounds": ((100.0, 200.0), "min"),
55         "throttle_enforcement": "boundary_constraint",
56         "fix_initial": False,
57         "constrain_final": False,
58         "fix_duration": False,
59         "initial_bounds": ((10.0, 20.0), "min"),
60         "duration_bounds": ((15.0, 25.0), "min"),
61     },
62 },
63 #escort
64 "cruise_1": {
65     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
66     "user_options": {
67         "optimize_mach": False,
68         "optimize_altitude": False,
69         "num_segments": 10,
70         "order": 3,
71         "solve_for_distance": False,
72         "initial_mach": (0.9, "unitless"),
73         "final_mach": (0.5, "unitless"),
74         "mach_bounds": ((0.4, 0.9), "unitless"),
75         "initial_altitude": (35000.0, "ft"),
76         "final_altitude": (38000.0, "ft"),
77         "altitude_bounds": ((34000.0, 40000.0), "ft"),
78         "throttle_enforcement": "boundary_constraint",
79         "fix_initial": False,
80         "constrain_final": False,
81         "fix_duration": False,
82         "initial_bounds": ((200.0, 280.0), "min"),
83         "duration_bounds": ((150.0, 360.0), "min"),
84     },
85 },
```

```
86 # climb/Accel
87 "cruise_2": {
88     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
89     "user_options": {
90         "optimize_mach": True,
91         "optimize_altitude": True,
92         "num_segments": 10,
93         "order": 3,
94         "solve_for_distance": False,
95         "initial_mach": (0.5, "unitless"),
96         "final_mach": (0.78, "unitless"),
97         "mach_bounds": ((0.4, 0.8), "unitless"),
98         "initial_altitude": (38000.0, "ft"),
99         "final_altitude": (40000.0, "ft"),
100        "altitude_bounds": ((35000.0, 40000.0), "ft"),
101        "throttle_enforcement": "path_constraint",
102        "fix_initial": False,
103        "constrain_final": False,
104        "fix_duration": False,
105        "initial_bounds": ((5.0, 10.0), "min"),
106        "duration_bounds": ((5.0, 15.0), "min"),
107    },
108 },
109 "cruise_3": {
110     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
111     "user_options": {
112         "optimize_mach": True,
113         "optimize_altitude": True,
114         "num_segments": 10,
115         "order": 3,
116         "solve_for_distance": False,
117         "initial_mach": (0.78, "unitless"),
118         "final_mach": (0.6, "unitless"),
119         "mach_bounds": ((0.5, 0.8), "unitless"),
120         "initial_altitude": (40000.0, "ft"),
121         "final_altitude": (35000.0, "ft"),
122         "altitude_bounds": ((34000.0, 40000.0), "ft"),
123         "throttle_enforcement": "boundary_constraint",
```

```
124         "fix_initial": False,
125         "constrain_final": False,
126         "fix_duration": False,
127         "initial_bounds": ((60.0, 100.0), "min"),
128         "duration_bounds": ((100.0, 200.0), "min")
129     },
130 },
131 "descent": {
132     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
133     "user_options": {
134         "optimize_mach": False,
135         "optimize_altitude": False,
136         "num_segments": 10,
137         "order": 3,
138         "solve_for_distance": False,
139         "initial_mach": (0.6, "unitless"),
140         "final_mach": (0.3, "unitless"),
141         "mach_bounds": ((0.3, 0.6), "unitless"),
142         "initial_altitude": (35000.0, "ft"),
143         "final_altitude": (500.0, "ft"),
144         "altitude_bounds": ((0.0, 30000.0), "ft"),
145         "throttle_enforcement": "path_constraint",
146         "fix_initial": False,
147         "constrain_final": True,
148         "fix_duration": False,
149         "initial_bounds": ((5.0, 25.0), "min"),
150         "duration_bounds": ((15.0, 30.0), "min"),
151     },
152 },
153 "post_mission": {
154     "include_landing": False,
155     "constrain_range": True,
156     "target_range": (500, "nmi"),
157 },
158 }
159
160 prob = av.AviaryProblem(analysis_scheme)
161
162 # Load aircraft and options data from user
```

```
163 # Allow for user overrides here
164 prob.load_inputs(aircraft_filename, phase_info)
165
166 prob.check_and_preprocess_inputs()
167
168 prob.add_pre_mission_systems()
169
170 prob.add_phases()
171
172 prob.add_post_mission_systems()
173
174 # Link phases and variables
175 prob.link_phases()
176
177 prob.add_driver(optimizer, max_iter=max_iter)
178
179
180 prob.model.add_design_var(av.Mission.Design.GROSS_MASS, units='lbm
    ',
181
182                             lower=32000, upper=37000.0, ref=36733)
183 prob.model.add_design_var(av.Aircraft.Wing.AREA, units='ft**2',
184                             lower=400, upper=500, ref=445.03)
185 prob.model.add_design_var(av.Aircraft.Wing.SPAN, units='ft',
186                             lower=42, upper=50, ref=42.08)
187 prob.model.add_design_var(av.Mission.Design.RANGE, units='NM',
188                             lower=500, upper=800, ref=1000)
189 prob.model.add_design_var(av.Aircraft.Wing.ASPECT_RATIO,
190                             lower=3, upper=5, ref=3.98)
191 prob.model.add_design_var(av.Aircraft.HorizontalTail.AREA, units="
    ft**2",
192                             lower=150, upper=160, ref=153.46)
193 prob.model.add_design_var(av.Aircraft.VerticalTail.AREA, units="ft
    **2",
194                             lower=50, upper=55, ref=53.9)
195 prob.model.add_design_var(av.Mission.Takeoff.LIFT_OVER_DRAG,
196                             lower=3, upper=5, ref=3.5)
197 prob.model.add_design_var(av.Mission.Takeoff.LIFT_COEFFICIENT_MAX,
198                             lower=1.6, upper=2, ref=1.8)
199 prob.model.add_design_var(av.Mission.Landing.LIFT_COEFFICIENT_MAX,
200                             lower=1.8, upper=2.5, ref=2.2)
```

```
200 prob.add_objective(objective_type=objective_type)
201
202 prob.setup()
203
204 prob.set_initial_guesses()
205
206 prob.run_aviary_problem(record_filename, restart_filename=
    restart_filename)
207
208 print('-----')
209 print('Sizing Results')
210 print('-----')
211 print(f'Design Range = {prob.get_val(av.Mission.Design.RANGE,
    units="NM")}')
212 print(f'Summary Range = {prob.get_val(av.Mission.Summary.RANGE,
    units="NM")}')
213 print(f'Total fuel capacity = {prob.get_val(av.Aircraft.Fuel.
    TOTAL_CAPACITY, units="lbm")}')
214 print(f'Empty mass = {prob.get_val(av.Aircraft.Design.
    OPERATING_MASS, units="lbm")}')
215 print(f'Total Payload mass = {prob.get_val(av.Aircraft.CrewPayload.
    TOTAL_PAYLOAD_MASS, units="lbm")}')
216 print(f'Design Gross mass = {prob.get_val(av.Mission.Design.
    GROSS_MASS, units="lbm")}')
217 print(f'Summary Gross mass = {prob.get_val(av.Mission.Summary.
    GROSS_MASS, units="lbm")}')
218 print(f'Wing Area = {prob.get_val(av.Aircraft.Wing.AREA, units="ft
    **2")}')
219 print(f'Wing Span = {prob.get_val(av.Aircraft.Wing.SPAN, units="ft
    ")}')
220 print(f'Aspect Ratio = {prob.get_val(av.Aircraft.Wing.ASPECT_RATIO
    )}')
221 print(f'HT Area = {prob.get_val(av.Aircraft.HorizontalTail.AREA,
    units="ft**2")}')
222 print(f'VT Area = {prob.get_val(av.Aircraft.VerticalTail.AREA,
    units="ft**2")}')
223 print(f'Takeoff L/D = {prob.get_val(av.Mission.Takeoff.
    LIFT_OVER_DRAG)')
224 print(f'Takeoff Clmax = {prob.get_val(av.Mission.Takeoff.
    LIFT_COEFFICIENT_MAX)')
```

```
225 print(f'Landing Clmax = {prob.get_val(av.Mission.Landing.  
      LIFT_COEFFICIENT_MAX)}')
```

B.11 Aviary: DCA Patrol Phase Info

```
1 phase_info = {  
2     "pre_mission": {"include_takeoff": True, "optimize_mass": True  
3 },  
4     "climb": {  
5         "subsystem_options": {"core_aerodynamics": {"method": "  
6 computed"}},  
7         "user_options": {  
8             "optimize_mach": False,  
9             "optimize_altitude": True,  
10            "num_segments": 5,  
11            "order": 3,  
12            "solve_for_distance": True,  
13            "initial_mach": (0.2, "unitless"),  
14            "final_mach": (0.8, "unitless"),  
15            "mach_bounds": ((0.0, 0.8), "unitless"),  
16            "initial_altitude": (0.0, "ft"),  
17            "final_altitude": (40000.0, "ft"),  
18            "altitude_bounds": ((0.0, 45000.0), "ft"),  
19            "throttle_enforcement": "path_constraint",  
20            "fix_initial": False,  
21            "constrain_final": False,  
22            "fix_duration": False,  
23            "initial_bounds": ((5.0, 15.0), "min"),  
24            "duration_bounds": ((10.0, 30.0), "min"),  
25            "add_initial_mass_constraint": False,  
26        },  
27    },  
28    "cruise": {  
29        "subsystem_options": {"core_aerodynamics": {"method": "  
30 computed"}},  
31        "user_options": {  
32            "optimize_mach": True,  
33            "optimize_altitude": True,  
34            "num_segments": 5,  
35            "order": 3,
```

```
33         "solve_for_distance": False,
34         "initial_mach": (0.8, "unitless"),
35         "final_mach": (0.8, "unitless"),
36         "mach_bounds": ((0.75, 0.9), "unitless"),
37         "initial_altitude": (40000.0, "ft"),
38         "final_altitude": (40000.0, "ft"),
39         "altitude_bounds": ((40000.0, 40000.0), "ft"),
40         "throttle_enforcement": "path_constraint",
41         "fix_initial": False,
42         "constrain_final": True,
43         "fix_duration": False,
44         "initial_bounds": ((60.0, 120.0), "min"),
45         "duration_bounds": ((100.0, 300.0), "min"),
46     },
47 },
48 # Combat Air-Patrol
49     "cruise_1": {
50         "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
51         "user_options": {
52             "optimize_mach": True,
53             "optimize_altitude": False,
54             "num_segments": 1,
55             "order": 3,
56             "solve_for_distance": False,
57             "initial_mach": (0.8, "unitless"),
58             "final_mach": (0.6, "unitless"),
59             "mach_bounds": ((0.55, 0.9), "unitless"),
60             "initial_altitude": (40000.0, "ft"),
61             "final_altitude": (35000.0, "ft"),
62             "altitude_bounds": ((35000.0, 45000.0), "ft"),
63             "throttle_enforcement": "path_constraint",
64             "fix_initial": False,
65             "constrain_final": False,
66             "fix_duration": False,
67             "initial_bounds": ((200.0, 280.0), "min"),
68             "duration_bounds": ((240.0, 240.0), "min"),
69         },
70     },
71 #Dash
```

```
72     "cruise_2": {
73         "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
74         "user_options": {
75             "optimize_mach": True,
76             "optimize_altitude": True,
77             "num_segments": 5,
78             "order": 3,
79             "solve_for_distance": False,
80             "initial_mach": (0.6, "unitless"),
81             "final_mach": (0.9, "unitless"),
82             "mach_bounds": ((0.4, 0.9), "unitless"),
83             "initial_altitude": (35000.0, "ft"),
84             "final_altitude": (35000.0, "ft"),
85             "altitude_bounds": ((35000.0, 35000.0), "ft"),
86             "throttle_enforcement": "path_constraint",
87             "fix_initial": False,
88             "constrain_final": False,
89             "fix_duration": False,
90             "initial_bounds": ((1.0, 2.5), "min"),
91             "duration_bounds": ((1.5, 3.0), "min"),
92         },
93     },
94     #Accel
95     "cruise_3": {
96         "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
97         "user_options": {
98             "optimize_mach": True,
99             "optimize_altitude": True,
100             "num_segments": 5,
101             "order": 3,
102             "solve_for_distance": False,
103             "initial_mach": (0.9, "unitless"),
104             "final_mach": (0.9, "unitless"),
105             "mach_bounds": ((0.9, 0.9), "unitless"),
106             "initial_altitude": (35000.0, "ft"),
107             "final_altitude": (25000.0, "ft"),
108             "altitude_bounds": ((20000.0, 35000.0), "ft"),
109             "throttle_enforcement": "boundary_constraint",
```

```
110         "fix_initial": False,
111         "constrain_final": False,
112         "fix_duration": False,
113         "initial_bounds": ((5.0, 15.0), "min"),
114         "duration_bounds": ((10.0, 30.0), "min"),
115     },
116
117 },
118 "cruise_4": {
119     "subsystem_options": {"core_aerodynamics": {"method": "
120 computed"}},
121     "user_options": {
122         "optimize_mach": True,
123         "optimize_altitude": True,
124         "num_segments": 5,
125         "order": 3,
126         "solve_for_distance": False,
127         "initial_mach": (0.9, "unitless"),
128         "final_mach": (0.7, "unitless"),
129         "mach_bounds": ((0.6, 0.9), "unitless"),
130         "initial_altitude": (35000.0, "ft"),
131         "final_altitude": (40000.0, "ft"),
132         "altitude_bounds": ((30000.0, 45000.0), "ft"),
133         "throttle_enforcement": "path_constraint",
134         "fix_initial": False,
135         "constrain_final": True,
136         "fix_duration": False,
137         "initial_bounds": ((10.0, 30.0), "min"),
138         "duration_bounds": ((20.0, 60.0), "min"),
139     },
140 },
141 "descent": {
142     "subsystem_options": {"core_aerodynamics": {"method": "
143 computed"}},
144     "user_options": {
145         "optimize_mach": False,
146         "optimize_altitude": False,
147         "num_segments": 5,
148         "order": 3,
149         "solve_for_distance": False,
```

```
148         "initial_mach": (0.6, "unitless"),
149         "final_mach": (0.4, "unitless"),
150         "mach_bounds": ((0.4, 0.6), "unitless"),
151         "initial_altitude": (45000.0, "ft"),
152         "final_altitude": (0.0, "ft"),
153         "altitude_bounds": ((0.0, 30000.0), "ft"),
154         "throttle_enforcement": "path_constraint",
155         "fix_initial": False,
156         "constrain_final": True,
157         "fix_duration": False,
158         "initial_bounds": ((5.0, 15.0), "min"),
159         "duration_bounds": ((10.0, 25.0), "min"),
160     },
161
162 },
163 "post_mission": {
164     "include_landing": True,
165     "constrain_range": True,
166     "target_range": (800, "nmi"),
167 },
168 }
```

B.12 Aviary: PDI Phase Info

```
1 aircraft_filename = "models/test_aircraft/
   Interceptor1_Aircraft_FwFm.csv"
2 optimizer = "IPOPT"
3 analysis_scheme = av.AnalysisScheme.COLLOCATION
4 objective_type = None
5 record_filename = 'aviary_history.db'
6 restart_filename = None
7 max_iter = 5
8
9 phase_info = {
10     "pre_mission": {"include_takeoff": True, "optimize_mass": True
11 },
12     "climb": {
13         "subsystem_options": {"core_aerodynamics": {"method": "
   computed"}},
14         "user_options": {
```

```
14         "optimize_mach": False,
15         "optimize_altitude": False,
16         "num_segments": 5,
17         "order": 3,
18         "solve_for_distance": False,
19         "initial_mach": (0.2, "unitless"),
20         "final_mach": (0.8, "unitless"),
21         "mach_bounds": ((0.1, 0.9), "unitless"),
22         "initial_altitude": (0.0, "ft"),
23         "final_altitude": (35000.0, "ft"),
24         "altitude_bounds": ((0.0, 35000.0), "ft"),
25         "throttle_enforcement": "path_constraint",
26         "fix_initial": True,
27         "constrain_final": False,
28         "fix_duration": False,
29         "initial_bounds": ((4.0, 20.0), "min"),
30         "duration_bounds": ((15.0, 35.0), "min"),
31         "add_initial_mass_constraint": False,
32     },
33 },
34 #dash
35 "cruise": {
36     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
37     "user_options": {
38         "optimize_mach": False,
39         "optimize_altitude": False,
40         "num_segments": 5,
41         "order": 3,
42         "solve_for_distance": False,
43         "initial_mach": (0.8, "unitless"),
44         "final_mach": (0.9, "unitless"),
45         "mach_bounds": ((0.8, 0.9), "unitless"),
46         "initial_altitude": (35000.0, "ft"),
47         "final_altitude": (35000.0, "ft"),
48         "altitude_bounds": ((35000.0, 35000.0), "ft"),
49         "throttle_enforcement": "boundary_constraint",
50         "fix_initial": False,
51         "constrain_final": False,
52         "fix_duration": False,
```

```
53         "initial_bounds": ((10.0, 20.0), "min"),
54         "duration_bounds": ((15.0, 25.0), "min"),
55     },
56 },
57 #combat
58 "cruise_1": {
59     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
60     "user_options": {
61         "optimize_mach": False,
62         "optimize_altitude": False,
63         "num_segments": 5,
64         "order": 3,
65         "solve_for_distance": False,
66         "initial_mach": (0.9, "unitless"),
67         "final_mach": (0.9, "unitless"),
68         "mach_bounds": ((0.85, 0.95), "unitless"),
69         "initial_altitude": (35000.0, "ft"),
70         "final_altitude": (35000.0, "ft"),
71         "altitude_bounds": ((34000.0, 36000.0), "ft"),
72         "throttle_enforcement": "boundary_constraint",
73         "fix_initial": False,
74         "constrain_final": False,
75         "fix_duration": False,
76         "initial_bounds": ((5.0, 15.0), "min"),
77         "duration_bounds": ((5.0, 10.0), "min")
78     },
79 },
80 # climb/Accel
81 "cruise_2": {
82     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
83     "user_options": {
84         "optimize_mach": True,
85         "optimize_altitude": True,
86         "num_segments": 10,
87         "order": 3,
88         "solve_for_distance": False,
89         "initial_mach": (0.9, "unitless"),
90         "final_mach": (0.78, "unitless"),
```

```
91         "mach_bounds": ((0.7, 0.9), "unitless"),
92         "initial_altitude": (35000.0, "ft"),
93         "final_altitude": (40000.0, "ft"),
94         "altitude_bounds": ((34000.0, 42000.0), "ft"),
95         "throttle_enforcement": "path_constraint",
96         "fix_initial": False,
97         "constrain_final": False,
98         "fix_duration": False,
99         "initial_bounds": ((5.0, 10.0), "min"),
100        "duration_bounds": ((5.0, 15.0), "min")
101    },
102},
103    "cruise_3": {
104        "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
105        "user_options": {
106            "optimize_mach": True,
107            "optimize_altitude": True,
108            "num_segments": 10,
109            "order": 3,
110            "solve_for_distance": False,
111            "initial_mach": (0.6, "unitless"),
112            "final_mach": (0.6, "unitless"),
113            "mach_bounds": ((0.5, 0.7), "unitless"),
114            "initial_altitude": (40000.0, "ft"),
115            "final_altitude": (34000.0, "ft"),
116            "altitude_bounds": ((33000.0, 40000.0), "ft"),
117            "throttle_enforcement": "boundary_constraint",
118            "fix_initial": False,
119            "constrain_final": False,
120            "fix_duration": False,
121            "initial_bounds": ((60.0, 100.0), "min"),
122            "duration_bounds": ((100.0, 200.0), "min")
123        },
124    },
125    "descent": {
126        "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
127        "user_options": {
128            "optimize_mach": False,
```

```
129         "optimize_altitude": False,
130         "num_segments": 5,
131         "order": 3,
132         "solve_for_distance": False,
133         "initial_mach": (0.7, "unitless"),
134         "final_mach": (0.5, "unitless"),
135         "mach_bounds": ((0.4, 0.8), "unitless"),
136         "initial_altitude": (34000.0, "ft"),
137         "final_altitude": (500.0, "ft"),
138         "altitude_bounds": ((0.0, 35000.0), "ft"),
139         "throttle_enforcement": "path_constraint",
140         "fix_initial": False,
141         "constrain_final": True,
142         "fix_duration": False,
143         "initial_bounds": ((5.0, 15.0), "min"),
144         "duration_bounds": ((15.0, 30.0), "min")
145     },
146 },
147     "post_mission": {
148         "include_landing": False,
149         "constrain_range": True,
150         "target_range": (500, "nmi"),
151     },
152 }
```

B.13 Aviary: Escort Phase Info

```
1 phase_info = {
2     "pre_mission": {"include_takeoff": True, "optimize_mass": True
3 },
4     "climb": {
5         "subsystem_options": {"core_aerodynamics": {"method": "
6         computed"}},
7         "user_options": {
8             "optimize_mach": False,
9             "optimize_altitude": False,
10            "num_segments": 10,
11            "order": 3,
12            "solve_for_distance": False,
13            "initial_mach": (0.2, "unitless"),
```

```
12         "final_mach": (0.8, "unitless"),
13         "mach_bounds": ((0.1, 0.9), "unitless"),
14         "initial_altitude": (0.0, "ft"),
15         "final_altitude": (35000.0, "ft"),
16         "altitude_bounds": ((0.0, 40000.0), "ft"),
17         "throttle_enforcement": "path_constraint",
18         "fix_initial": True,
19         "constrain_final": False,
20         "fix_duration": False,
21         "initial_bounds": ((4.0, 20.0), "min"),
22         "duration_bounds": ((15.0, 35.0), "min"),
23         "add_initial_mass_constraint": False,
24     },
25 },
26 #dash
27 "cruise": {
28     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
29     "user_options": {
30         "optimize_mach": False,
31         "optimize_altitude": False,
32         "num_segments": 10,
33         "order": 3,
34         "solve_for_distance": False,
35         "initial_mach": (0.8, "unitless"),
36         "final_mach": (0.9, "unitless"),
37         "mach_bounds": ((0.8, 0.9), "unitless"),
38         "initial_altitude": (35000.0, "ft"),
39         "final_altitude": (35000.0, "ft"),
40         "altitude_bounds": ((30000.0, 40000.0), "ft")"
initial_bounds": ((60.0, 100.0), "min"),
41         "duration_bounds": ((100.0, 200.0), "min"),
42         "throttle_enforcement": "boundary_constraint",
43         "fix_initial": False,
44         "constrain_final": False,
45         "fix_duration": False,
46         "initial_bounds": ((10.0, 20.0), "min"),
47         "duration_bounds": ((15.0, 25.0), "min"),
48     },
49 }
```

```
50     #escort
51     "cruise_1": {
52         "subsystem_options": {"core_aerodynamics": {"method": "
53         computed"}},
54         "user_options": {
55             "optimize_mach": False,
56             "optimize_altitude": False,
57             "num_segments": 10,
58             "order": 3,
59             "solve_for_distance": False,
60             "initial_mach": (0.9, "unitless"),
61             "final_mach": (0.5, "unitless"),
62             "mach_bounds": ((0.4, 0.9), "unitless"),
63             "initial_altitude": (35000.0, "ft"),
64             "final_altitude": (38000.0, "ft"),
65             "altitude_bounds": ((34000.0, 40000.0), "ft"),
66             "throttle_enforcement": "boundary_constraint",
67             "fix_initial": False,
68             "constrain_final": False,
69             "fix_duration": False,
70             "initial_bounds": ((200.0, 280.0), "min"),
71             "duration_bounds": ((150.0, 360.0), "min"),
72         },
73     },
74     # climb/Accel
75     "cruise_2": {
76         "subsystem_options": {"core_aerodynamics": {"method": "
77         computed"}},
78         "user_options": {
79             "optimize_mach": True,
80             "optimize_altitude": True,
81             "num_segments": 10,
82             "order": 3,
83             "solve_for_distance": False,
84             "initial_mach": (0.5, "unitless"),
85             "final_mach": (0.78, "unitless"),
86             "mach_bounds": ((0.4, 0.8), "unitless"),
87             "initial_altitude": (38000.0, "ft"),
88             "final_altitude": (40000.0, "ft"),
89             "altitude_bounds": ((35000.0, 40000.0), "ft"),
```

```
88         "throttle_enforcement": "path_constraint",
89         "fix_initial": False,
90         "constrain_final": False,
91         "fix_duration": False,
92         "initial_bounds": ((5.0, 10.0), "min"),
93         "duration_bounds": ((5.0, 15.0), "min"),
94     },
95 },
96 "cruise_3": {
97     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
98     "user_options": {
99         "optimize_mach": True,
100         "optimize_altitude": True,
101         "num_segments": 10,
102         "order": 3,
103         "solve_for_distance": False,
104         "initial_mach": (0.78, "unitless"),
105         "final_mach": (0.6, "unitless"),
106         "mach_bounds": ((0.5, 0.8), "unitless"),
107         "initial_altitude": (40000.0, "ft"),
108         "final_altitude": (35000.0, "ft"),
109         "altitude_bounds": ((34000.0, 40000.0), "ft"),
110         "throttle_enforcement": "boundary_constraint",
111         "fix_initial": False,
112         "constrain_final": False,
113         "fix_duration": False,
114         "initial_bounds": ((60.0, 100.0), "min"),
115         "duration_bounds": ((100.0, 200.0), "min")
116     },
117 },
118 "descent": {
119     "subsystem_options": {"core_aerodynamics": {"method": "
computed"}},
120     "user_options": {
121         "optimize_mach": False,
122         "optimize_altitude": False,
123         "num_segments": 10,
124         "order": 3,
125         "solve_for_distance": False,
```

```
126         "initial_mach": (0.6, "unitless"),
127         "final_mach": (0.3, "unitless"),
128         "mach_bounds": ((0.3, 0.6), "unitless"),
129         "initial_altitude": (35000.0, "ft"),
130         "final_altitude": (500.0, "ft"),
131         "altitude_bounds": ((0.0, 30000.0), "ft"),
132         "throttle_enforcement": "path_constraint",
133         "fix_initial": False,
134         "constrain_final": True,
135         "fix_duration": False,
136         "initial_bounds": ((5.0, 25.0), "min"),
137         "duration_bounds": ((15.0, 30.0), "min"),
138     },
139 },
140     "post_mission": {
141         "include_landing": False,
142         "constrain_range": True,
143         "target_range": (500, "nmi"),
144     },
145 }
```

B.14 Aviary: Aviary Run Mission Command

```
1 aircraft_filename = "models/test_aircraft/
   Interceptor1_Aircraft_FwFm.csv"
2 optimizer = "IPOPT"
3 analysis_scheme = av.AnalysisScheme.COLLOCATION
4 objective_type = None
5 record_filename = 'DCAP-sizing.db'
6 restart_filename = None
7 max_iter = 5
```

B.15 Aviary: Aviary Analysis Problem

```
1 prob = av.AviaryProblem(analysis_scheme)
2
3 # Load aircraft and options data from user
4 # Allow for user overrides here
5 prob.load_inputs(aircraft_filename, phase_info)
6
```

```
7 prob.check_and_preprocess_inputs()
8
9 prob.add_pre_mission_systems()
10
11 prob.add_phases()
12
13 prob.add_post_mission_systems()
14
15 # Link phases and variables
16 prob.link_phases()
17
18 prob.add_driver(optimizer, max_iter=max_iter)
19
20
21 prob.model.add_design_var(av.Mission.Design.GROSS_MASS, units='lbm
    ',
22                           lower=32000, upper=37000.0, ref=36733)
23 prob.model.add_design_var(av.Aircraft.Wing.AREA, units='ft**2',
24                           lower=400, upper=500, ref=486.26)
25 prob.model.add_design_var(av.Aircraft.Wing.SPAN, units='ft',
26                           lower=43, upper=50, ref=44)
27 prob.model.add_design_var(av.Mission.Design.RANGE, units='NM',
28                           lower=500, upper=800, ref=700)
29 prob.model.add_design_var(av.Aircraft.Wing.ASPECT_RATIO,
30                           lower=3, upper=5, ref=3.98)
31 prob.model.add_design_var(av.Aircraft.HorizontalTail.AREA, units="
    ft**2",
32                           lower=85, upper=100, ref=86)
33 prob.model.add_design_var(av.Aircraft.VerticalTail.AREA, units="ft
    **2",
34                           lower=58, upper=65, ref=58.6)
35 prob.model.add_design_var(av.Mission.Takeoff.LIFT_OVER_DRAG,
36                           lower=10, upper=12, ref=10)
37 prob.model.add_design_var(av.Mission.Takeoff.LIFT_COEFFICIENT_MAX,
38                           lower=1.6, upper=2, ref=1.8)
39 prob.model.add_design_var(av.Mission.Landing.LIFT_COEFFICIENT_MAX,
40                           lower=1.8, upper=2.5, ref=2.2)
41 prob.add_objective(objective_type=objective_type)
42
43 prob.setup()
```

```
44
45 prob.set_initial_guesses()
46
47 prob.run_aviary_problem(record_filename, restart_filename=
    restart_filename)
```

B.16 Aviary: Design Variables

```
1 prob.model.add_design_var(av.Mission.Design.GROSS_MASS, units='lbm
    ',
2
3                               lower=32000, upper=37000.0, ref=36733)
4 prob.model.add_design_var(av.Aircraft.Wing.AREA, units='ft**2',
5                               lower=400, upper=500, ref=486.26)
6 prob.model.add_design_var(av.Aircraft.Wing.SPAN, units='ft',
7                               lower=43, upper=50, ref=44)
8 prob.model.add_design_var(av.Mission.Design.RANGE, units='NM',
9                               lower=500, upper=800, ref=700)
10 prob.model.add_design_var(av.Aircraft.Wing.ASPECT_RATIO,
11                               lower=3, upper=5, ref=3.98)
12 prob.model.add_design_var(av.Aircraft.HorizontalTail.AREA, units="
13     ft**2",
14                               lower=85, upper=100, ref=86)
15 prob.model.add_design_var(av.Aircraft.VerticalTail.AREA, units="ft
16     **2",
17                               lower=58, upper=65, ref=58.6)
18 prob.model.add_design_var(av.Mission.Takeoff.LIFT_OVER_DRAG,
19                               lower=10, upper=12, ref=10)
20 prob.model.add_design_var(av.Mission.Takeoff.LIFT_COEFFICIENT_MAX,
21                               lower=1.6, upper=2, ref=1.8)
22 prob.model.add_design_var(av.Mission.Landing.LIFT_COEFFICIENT_MAX,
23                               lower=1.8, upper=2.5, ref=2.2)
```

B.17 Aviary: Print Desired Sizing Variables

```
1 print('-----')
2 print('Sizing Results')
3 print('-----')
4 print(f'Design Range = {prob.get_val(av.Mission.Design.RANGE,
5     units="NM")}')')
```

```
5 print(f'Summary Range = {prob.get_val(av.Mission.Summary.RANGE,
    units="NM")}')
6 print(f'Total fuel capacity = {prob.get_val(av.Aircraft.Fuel.
    TOTAL_CAPACITY, units="lbm")}')
7 print(f'Empty mass = {prob.get_val(av.Aircraft.Design.
    OPERATING_MASS, units="lbm")}')
8 print(f'Total Payload mass = {prob.get_val(av.Aircraft.CrewPayload.
    TOTAL_PAYLOAD_MASS, units="lbm")}')
9 print(f'Design Gross mass = {prob.get_val(av.Mission.Design.
    GROSS_MASS, units="lbm")}')
10 print(f'Summary Gross mass = {prob.get_val(av.Mission.Summary.
    GROSS_MASS, units="lbm")}')
11 print(f'Wing Area = {prob.get_val(av.Aircraft.Wing.AREA, units="ft
    **2")}')
12 print(f'Wing Span = {prob.get_val(av.Aircraft.Wing.SPAN, units="ft
    ")}')
13 print(f'Aspect Ratio = {prob.get_val(av.Aircraft.Wing.ASPECT_RATIO
    )}')
14 print(f'HT Area = {prob.get_val(av.Aircraft.HorizontalTail.AREA,
    units="ft**2")}')
15 print(f'VT Area = {prob.get_val(av.Aircraft.VerticalTail.AREA,
    units="ft**2")}')
16 print(f'Takeoff L/D = {prob.get_val(av.Mission.Takeoff.
    LIFT_OVER_DRAG)}')
17 print(f'Takeoff Clmax = {prob.get_val(av.Mission.Takeoff.
    LIFT_COEFFICIENT_MAX)}')
18 print(f'Landing Clmax = {prob.get_val(av.Mission.Landing.
    LIFT_COEFFICIENT_MAX)}')
```

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2023	Aircraft Maintenance Training General Aircraft Maintenance - Sheet metal fabrication, composite lamination - Engine ground runs, landing gear inspection
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